# Transportation Impact Study

# Golden State Natural Resources Forest Resiliency Demonstration Project Tuolumne County, CA

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Prepared for:

#### **GOLDEN STATE FINANCE AUTHORITY**

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# Table of Contents

SEC	CTION		PAGE NO.
1	Intro	duction	4
	1.1	Purpose and Scope of the TIS	4
	1.2	Project Location	5
	1.3	Project Description	5
2	Study	y Area	11
	2.1	Existing Street Network	11
	2.2	Transit Facilities	13
	2.3	Pedestrian and Bicycle Facilities	13
3	Proje	ct Traffic	18
	3.1	Trip Generation	18
	3.2	Trip Distribution and Assignment	19
4	Level	of Service (LOS) Analysis	26
	4.1	Study Intersections and Roadway Segments	
	4.2	Analysis Scenarios	26
	4.3	Traffic Volumes	27
	4.4	Operational Analysis Methodology	27
	4.5	Tuolumne County General Plan Consistency Requirements	28
	4.6	California Public Utilities Commission	32
	4.7	Caltrans Transportation Impact Study Guide	33
5	Existi	ing (2023) Conditions Analysis	34
	5.1	Intersection Operations	34
	5.2	Roadway Segment Operations	34
6	Open	ing Year (2025) Analysis	45
	6.1	Cumulative Projects	45
	6.2	Intersection Operations	45
	6.3	Roadway Segment Operations	46
7	Proje	ct Site Access	55
	7.1	Vehicular Site Access and Circulation	55
		7.1.1 Project Site Access	55
		7.1.2 Off-site Queuing Analysis	66
8	Vehic	cle Miles Traveled Analysis	70
	8.1	Methodology	70

8	3.2 VMT Analysis	72
9 9	Summary	74
10 I	References	75
TABLE	(S)	
Table 1.	Tuolumne Daily Employees	6
Table 2.	Trip Generation Summary	18
Table 3.	_evels of Service for Intersections using HCM Methodology	27
Table 4.	_evels of Service for Roadway Segments	28
Table 3.	Existing plus Project Weekday Peak Hour Intersection LOS	34
Table 4.	Existing ADT Roadway Segment Level of Service	35
Table 5.	Representative Haul Routes and Levels of Service – Existing	36
Table 6.	Opening Year (2025) Weekday Peak Hour Intersection LOS	45
Table 7.	Opening Year (2025) ADT Roadway Segment Level of Service	46
Table 8.	Representative Haul Routes and Levels of Service – Opening Year (2025)	48
Table 9.	Peak-Hour Queuing Summary for Existing Plus Project Conditions	67
Table 10	. Peak-Hour Queuing Summary for Opening Year (2025) Plus Project Conditions	68
Table 11	. VMT Threshold Summary	72
Table 12	. Summary of Project Area VMT	72
FIGUR		
Figure 1	Project Location and Study Area	7
Figure 2	Site Layout: Tuolumne Facility	9
Figure 3	Tuolumne County General Plan Roadway Network	14
Figure 4	Feed Stock and Haul Routes	16
Figure 5	Project Passenger Vehicle Trip Distribution and Assignment	20
Figure 6	Project Truck Trip Distribution and Assignment	22
Figure 7	Project Total Trip Assignment	24
Figure 8	Existing Intersection Controls and Geometrics	37
Figure 9	Existing Peak Hour Traffic Volumes	39
Figure 10	Existing plus Project Peak Hour Traffic Volumes	41
Figure 1	Existing Conditions Haul Route ADT and LOS Analysis (Lassen Facility)	43
Figure 1	Opening Year (2025) Peak Hour Traffic Volumes	49
Figure 1	Opening Year (2025) plus Project Peak Hour Traffic Volumes	51
Figure 1	Opening Year (2025) Conditions Haul Route ADT and Los Analysis (Lassen Facility)	53



# GOLDEN STATE NATURAL RESOURCES FOREST RESILIENCY DEMONSTRATION PROJECT, TUOLUMNE COUNTY TRANSPORTATION IMPACT ANALYSIS

Figure 16	AutoTurn Analysis - WB 62	58
Figure 14	AutoTurn Analysis - WB 62 with 30-foot KPRA & 65' Max Length	
Figure 18	AutoTurn Analysis - Fixed Axle 45' Pulp Log Truck	62
Figure 19	AutoTurn Analysis - Standard Log Truck with Rear Axle Steering	64

#### **APPENDICES**

- A Census Data and Raw Traffic Counts
- B LOS Worksheets
- C Haul Routes and Levels of Service
- D Cumulative Project Trip Generation
- E SimTraffic Queuing Worksheet



# 1 Introduction

#### 1.1 Purpose and Scope of the TIS

The purpose of this Transportation Impact Study (TIS) is to identify potential traffic impacts associated with the wood pellet manufacturing facility proposed to be constructed and operated in Tuolumne County as part of the Golden State Natural Resources Forest Resiliency Demonstration Project. This TIS has been prepared per the County's General Plan Transportation Element (Tuolumne County 2018), and applicable CEQA guidelines, including adherence to Senate Bill (SB) 743 and guidelines from the Governor's Office of Planning and Research (OPR 2018).

In 2019, the Golden State Finance Authority (GSFA) and the U.S. Forest Service signed a master Stewardship Agreement (MSA) for the general purpose of achieving resilient forests within U.S. Forest Service Region 5, which includes all of the 18 national forests located in California. Feedstock for manufacturing of wood pellets will be wood byproducts sourced from Sustainable Forest Management Projects such as hazardous fuel reduction projects, construction of shaded fuel breaks, and salvage harvests (see Chapter 2, Project Description, of the DEIR for a full description). While the MSA applies to the entirety of Region 5, only Sustainable Forest Management Projects within the "Working Area" described in Section 2.4 of the DEIR are contemplated under the proposed project. Feedstock will be taken to two sites for the manufacturing of the wood pellet byproducts, located in Northern California (Lassen Facility) and the Central Sierra Nevada foothills (Tuolumne Facility). This TIS focuses on traffic operations in and around the Tuolumne Facility (proposed project or project) and analyzes the impacts of the project on the local transportation system.

#### The objectives of this TIS are to:

- Document existing roadway, pedestrian, bicycle, transit and traffic conditions, including intersection levels
  of service in the study area;
- Estimate trip generation and trip characteristics for construction-related activities of the wood pellet manufacturing site;
- Document Existing (Year 2023) intersection levels of service in the study area;
- Document Opening Year (2025) intersection levels of service in the study area per traffic volumes derived from adding growth to existing traffic volumes and accounting for cumulative project traffic;
- Analyze the project related traffic impacts that would occur under the Existing (2023) and Opening Year (2025) conditions and describe the significance of the potential impacts;
- Provide a Vehicle Miles Traveled (VMT) analysis per Senate Bill 743 and the updated California CEQA Guidelines;
- Identify CEQA-required mitigation measures for significant transportation impacts and/or other improvements needed to meet level of service standards (if any); and,
- Provide findings and recommendations based on the traffic analysis of the proposed project.

Figure 1, Project Location and Study Area, shows the project location and study area. As illustrated in Figure 1, the study area is comprised of five (5) intersections near the project site. Additionally, two (2) roadway segments

adjacent to the site, along with representative haul routes throughout the Working Area, are included in this analysis.

#### 1.2 Project Location

The proposed Tuolumne wood pellet processing site is located at 12001 La Grange Road approximately 9 miles southwest of the community of Jamestown, in Tuolumne County, California, and in the western foothills of the Sierra Nevada Mountain Range (see Figure 1, Project Location and Study Area). The Tuolumne site is located immediately southeast of the junction of State Route 108 and La Grange Road. The site is situated in Township 1 South, Range 13 East, and Sections 14 and 23 of the U.S. Geological Survey Tuolumne, California 7.5-minute quadrangle.

The Tuolumne location is a previously developed site that was formerly a wood processing mill, used by the former owner, Sierra Pacific Industries (SPI), for finished bark and colored mulch processing. A wood shaving plant owned by American Wood Fibers is located adjacent to the west side of the site, and two residences are located adjacent to the northwest corner of the site. Agricultural land is located to the north, east, and south.

The project site is located southeast of State Route 108/120 (SR-108/120), with primary access to the site provided from La Grange Road – CR-J59, which connects to SR-108/120 northwest of the site. The site is bordered by Sierra Northern Railroad to the west that travels along La Grange Road and intersects near the southwestern project site boundary.

As shown in Figure 2, passenger vehicular (personnel/employee) access to the site would be provided via a currently unused and gated driveway (to be improved as part of the proposed project) along the northern boundary of the site, and truck access to the site would be provided via the existing site access driveway south of the train tracks.

#### 1.3 Project Description

The Golden State Natural Resources Forest Resiliency Demonstration Project is a response to the growing rate of wildfires in California, which has been exacerbated by hazardous excess fuel loads in forests, and the need to promote economic activity with California's rural counties. The project serves as an opportunity to begin restoring California forests and watersheds to a natural and resilient status and provide overall benefit to the state by sustainably procuring and processing excess biomass into a pelletized fuel source for renewable energy generation.

The Golden State Natural Resources Forest Resiliency Demonstration Project includes vegetation treatment and restoration activities (feedstock source); transportation and processing of the feedstock at two pellet processing facilities, one in the Central Sierra Nevada foothills and one in Northern California; and transportation of the finished product to a storage facility to be constructed at the Port of Stockton, California, for export to international markets. As noted above, this TIS specifically focuses on traffic operations in and around the Tuolumne Facility (identified as the proposed project or project in this study) and analyzes the impacts of the project on the local transportation system. The Tuolumne Facility would employ up to 51 people, with 38 overlapping on site between Shifts A and B during the workday, as shown in Table 1 below.



#### **Table 1. Tuolumne Daily Employees**

Shift	Employees
A (8:00 a.m 8:00 p.m.)	25
B (4:00 p.m 12:00 a.m.)	13
C (12:00 a.m 8:00 a.m.)	13
Total	51





SOURCE: Bing Maps (Accessed 2023), Nexus PMG 2021





SOURCE: Nexus PMG 2021



FIGURE 2



# 2 Study Area

This section provides a summary of the existing street network, including the major roadways serving the site, the existing transit service, and bicycle and pedestrian facilities in the study area (if applicable).

#### 2.1 Existing Street Network

Figure 3 provides the Tuolumne County Master Plan of Streets and Highways. Regional access to the site would be provided from SR-108/120, with local access from La Grange Road – CR-J59. Characteristics of the primary existing road network within the study area are described below.

#### Site Access Roadways

The Tuolumne Facility Site is located south of State Route 120 (SR-120) and north of the unincorporated community of Keystone in Tuolumne County. Employee access to the site is provided via La Grange Road and the northern site access driveway and truck access the site is provide via the southern site access driveway.

State Route 120 (SR-120) – SR-120 is an east-west, two-lane undivided highway located north of the project site. SR-120 is a Caltrans designated truck route; in Tuolumne County, SR-120 has terminal access, and allows the use of both STAA and California legal trucks. In Mariposa County, SR-120 allows only trucks that are no longer than 65 feet as per the kingpin-to-rear-axle (KRPA) advisory. The posted speed limit is generally 55-65 MPH.

La Grange Road – County Road J59 (CR-J59) – La Grange Road is a north-south, two-lane, undivided roadway located along the western edge of the project site. La Grange Road will provide primary personnel access to the project site. The posted speed limit is 55 MPH.

Yosemite Boulevard – State Route 132 (SR-132) – SR-132 is an east-west, two-lane, undivided highway located south of the project site. SR-132 is a Caltrans designated truck route; west of the City of Modesto, SR-132 has terminal access, and allows the use of both STAA and California legal trucks. East of the City of Modesto, SR-132 allows only trucks that are no longer than 65 feet as per the California Legal Route. The posted speed limit is 45 MPH.

**Red Hill Road** – Red Hill Road is a north-south, two-lane, undivided, and unstriped roadway located northeast of the project site. There are no present sidewalks, or curbs, and the use of trucks heavier than 25 tons is prohibited. The posted speed limit is 25 MPH.

Montezuma Road – State Route 49 (SR-49) – Montezuma Road is a north-south, two-lane, undivided highway located northeast of the project site. Montezuma Road provides regional access to the project site, and is a Caltrans designated truck route, wavering between allowing STAA and KPRA advisory sized trucks. It allows STAA trucks from Amador City to Angels Camp, Sonora to Postmile Marker 23.9, and Postmile 30.7 to the terminus in Mariposa County; in between these sections, SR-49 allows only KPRA advisory sized trucks. The posted speed limit is 65 MPH.



**Site Access Driveways** – The site access driveways provide direct access to project site. The northern driveway, which is currently overgrown and not operational, will be improved as part of the proposed project and serve as the primary employee access to the site. The southern driveway, which is currently paved and operational, will provide primary truck access to the project site.

#### **Haul Routes**

Although the exact haul routes to be used at any given time would vary widely depending on the feedstock areas, the following local and state highways would constitute the majority of expected haul routes throughout the Working Area. A brief description of each route is provided below, and all routes for the Tuolumne feedstock area are shown in Figure 4.

**US Route 50 (US-50)** – US-50 is an east-west, two- to four-lane highway located north of the project site. US-50 is a Caltrans designated truck route; west of Postmile Marker 31.3 it is part of the National Network, and allows the use of both STAA and California legal trucks. East of Postmile Marker 31.3, US-50 allows only 65 feet California Legal trucks. The posted speed limit is generally 55-65 MPH.

State Route 88 (SR-88) – SR-88 is an east-west highway located north of the project site. SR-88 is a Caltrans designated truck route that varies between allowing trucks with terminal access and trucks that are 65 feet maximum in length. SR-88 allows STAA trucks from Stockton to Amador City, and from Postmile Marker 2.2 to its eastern terminus, and it allows only 65 feet California Legal trucks between Amador City and Postmile Marker 2.2. The posted speed limit is generally 55 MPH.

State Route 4 (SR-4) – SR-4 is an east-west highway located north of the project site. SR-4 is a Caltrans designated truck route that varies between allowing trucks with terminal access and trucks that are KPRA advisory sized. SR-4 allows STAA trucks from Stockton to Postmile Marker 8.1, and from its junction with SR-49 to Postmile Marker 3.0, and it allows only KPRA advisory sized trucks between Postmile Marker 8.1 to its junction with SR-49, and from Postmile Marker 3.0 to its eastern terminus. The posted speed limit is generally 55 MPH.

State Route 108 (SR-108) – SR-108 is an east-west highway located north of the project site, and overlaps with SR-120 from Oakdale to Yosemite Junction. SR-108 is a Caltrans designated truck route with terminal access, and allows the use of both STAA and California legal trucks. From Postmile Marker 31.3 to its eastern terminus, SR-108 allows only KPRA advisory sized trucks. The posted speed limit is generally 55 MPH.

**State Route 140 (SR-140)** – SR-140 is an east-west highway located south of the project site. SR-140 is a Caltrans designated truck route with terminal access, and allows the use of both STAA and California legal trucks. The posted speed limit is generally 55-65 MPH.

**State Route 41 (SR-41)** – SR-41 is a north-south highway located south of the project site. SR-41 is a Caltrans designated truck route with terminal access, and allows the use of both STAA and California legal trucks, except for a small portion from Postmile Marker 45.7 to its northern terminus in Fresno County. The posted speed limit is generally 55 MPH.

State Route 168 (SR-168) – SR-168 is an east-west highway located south of the project site. SR-168 is a Caltrans designated truck route that varies between allowing trucks with terminal access, 65 feet California Legal trucks, and trucks that are KPRA advisory sized. SR-168 allows STAA trucks from Fresno to Postmile Marker 18.6, allows



only KPRA advisory sized trucks between Postmile Marker 36.6 to Postmile Marker 49.7, and allows only 65 feet California Legal trucks from Postmile Marker 18.6 to Postmile Marker 36.3, and from Postmile Parker 49.7 to its eastern terminus. The posted speed limit is generally 55-65 MPH.

#### 2.2 Transit Facilities

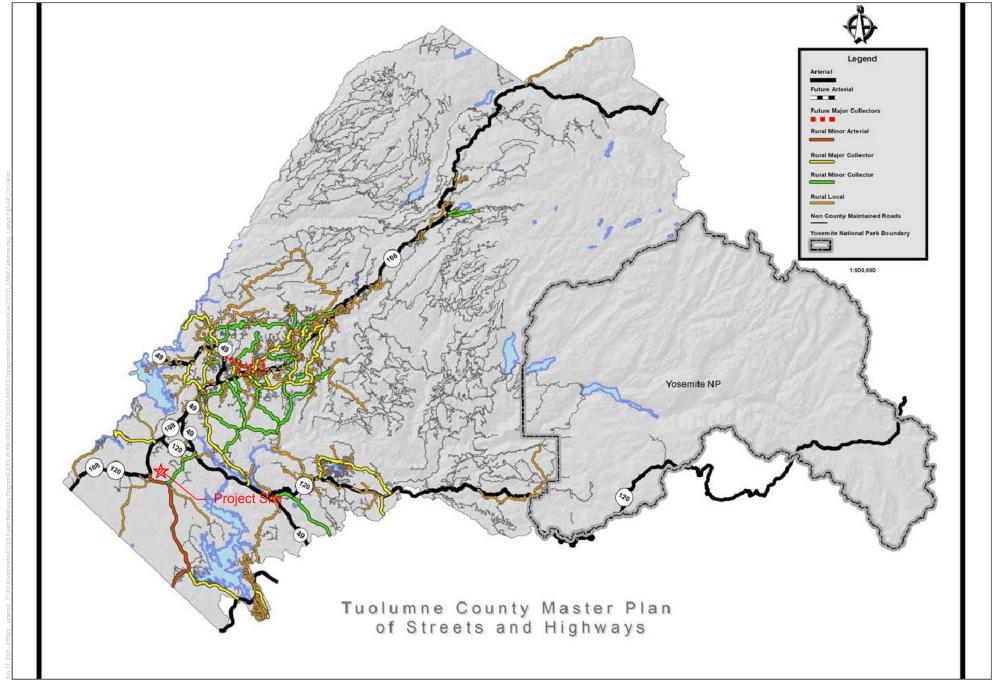
Transit in Tuolumne County is provided by Tuolumne County Transit (TCT) which currently operates two routes and a Dial-A-Ride service. There are no existing bus or transit routes that operate within a 1-mile radius of the project site, or near the community of Keystone. However, for additional reference, the Tuolumne County Transit routes are described below.

The two TCT routes operate only on weekdays whereas the Dial-A-Ride service is available on Mondays through Saturdays. Route 1 provides service mainly within the Sonora and East Sonora communities, and operates from 7:30am to 7:30pm, with 60-minute headways. Route 2 provides service between the Columbia, Shaws Flat, Sonora, Crystal Falls, Sugar Pine, and Sierra Village communities, and operates five trains at 6:25am, 9:30am, 11:00am, 1:30pm, and 4:40pm. The Dial-A-Ride service is reservation based and has an expansive service area throughout Tuolumne County; however, it does not service the project site area.

## 2.3 Pedestrian and Bicycle Facilities

There are currently little to no pedestrian or bicycle facilities provided near the project site. The 2020 Tuolumne County Active Transportation Plan (ATP) (TCTC 2020) has identified the need for improvements in the area under Project Numbers ATP-County06 and ATP-County07 for SR-108 and SR-120, respectively, which both include installation of bikeways with 4- to 8-foot shoulders and buffers throughout Tuolumne County along these roadways, including the extent adjacent to the project site. These facilities are identified as "Tier 2" improvements as prioritized by the Tuolumne County Transportation Commission (TCTC), indicating improved facilities have received either community and/or local agency support, but would likely require more community outreach and project information prior to implementation.



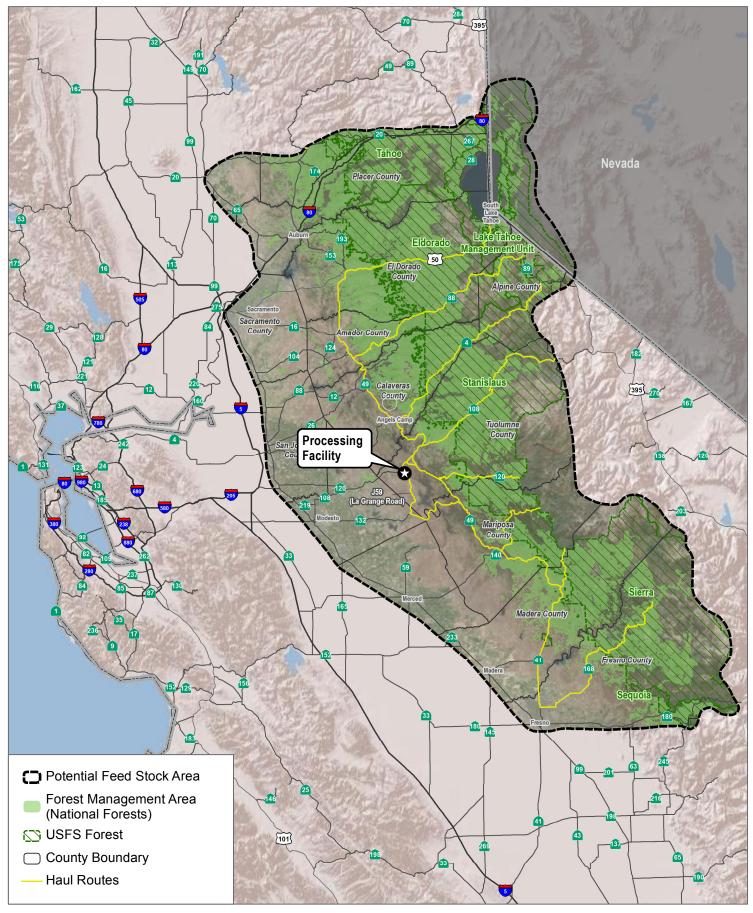


SOURCE: Tuolumne County 2018



FIGURE 3





SOURCE: Bing Maps 2022

**DUDEK** 

FIGURE 4



# 3 Project Traffic

This section documents the trip generation, distribution, and assignment of project traffic in the study area. As noted in Chapter 1, for the purposes of this analysis, "project" refers to traffic generated from transportation and processing of the feedstock at the Central Sierra Nevada pellet processing facility in Tuolumne County.

#### 3.1 Trip Generation

Trip generation estimates for the operation of the Tuolumne Facility are based on the number of workers and trucks that would be required for the proposed pellet production operations. Feedstock would be received at the woodyard 24 hours per day, 5 days per week<sup>1</sup>. This would produce and store enough woodchips for fuel to enable pellet production to operate consistently. Pellet production operations would be active 24 hours per day, 7 days per week, with up to 4 weeks total downtime allotted for planned and unplanned outages once at capacity. Operational traffic includes the number of employees, as well as and the amount of truck traffic that would be generated to and from the site daily and during the AM and PM peak commuting hours.

To provide a conservative analysis while also accounting for trips beginning or ending prior to peak period and/or multiple shifts throughout the workday, it is assumed that 100% of the Shift A employees would arrive inbound to the site during the AM peak period (7:00 a.m. to 9:00 a.m.) for their 8:00 a.m. to 8:00 p.m. shift, all Shift C employees would depart during the AM peak period at the end of their 12:-00 a.m. to 8:00 a.m. shift, and all Shift B employees would arrive at the site during the PM peak period (4:00 p.m. to 6:00 p.m.) for their 4:00 p.m. to 12:00 a.m. shift. No outbound PM peak period employee trips would occur.

Truck deliveries are typically sporadic throughout the day; therefore, in order to provide a conservative analysis, truck arrivals and departures were assumed to be distributed over the 24 hours, with daytime truck operations comprising 70% of delivery trips. The remaining 30% of feedstock deliveries are expected to occur overnight (7:00 a.m. to 7:00 p.m.).

The trip generation estimates for the operation of Tuolumne Facility are summarized in Table 2 below. To account for the impact trucks may have compared to passenger vehicles, passenger car equivalence (PCE) factors were applied to the trip generation estimates to account for truck traffic associated with the proposed facility. A 1.0 PCE factor was applied to passenger vehicles and 3.0 for ash removal and logging/haul trucks.

**Table 2. Trip Generation Summary** 

			Daily	AM Peak Hour			PM Peak Hour			
Vehicle Type	Daily	Quantity	Trips	In	Out	Total	In	Out	Total	
Non-PCE Adjusted Trip Generation										
Employees (Passenger Vehicles) <sup>1</sup> 51 workers		102	25	13	38	13	0	13		
Logging/Haul Trucks (day) <sup>2</sup>	165	7	7	14	7	7	14			
Logging/Haul Trucks (night) <sup>2</sup>	36	trucks	71	0	0	0	0	0	0	

<sup>&</sup>lt;sup>1</sup> In-forest operations are generally limited to Monday through Friday; however, the facility will also be open on Saturdays to receive occasional deliveries.

Ash Removal <sup>3</sup>	1	trucks	2	1	0	1	0	1	1
Peak T	340	33	20	53	20	8	28		
PCE Adjusted Trip Generation <sup>4</sup>									
Employees (Passenger Vehicles)1	51	workers	102	25	13	38	13	0	13
Logging/Haul Trucks <sup>2</sup>	82	trucks	495	21	21	42	21	21	42
Logging/Haul Trucks (night) <sup>2</sup>	36	trucks	213	0	0	0	0	0	0
Ash Removal <sup>3</sup>	1	trucks	6	3	0	3	0	3	3
Peak Trip Total (PCE)				49	34	83	34	24	58

- <sup>1</sup> Assumes employee arrivals and departures coincide with shift times.
- Trucks are assumed to arrive and depart the site throughout the day. Feedstock would be received 24 hours per day, with 70% of total daily feedstock expected to be received across 12 hours from 7am to 7pm, and 30% of total daily feedstock to be received overnight from 7pm to 7am.
- Ash removal may occur at any time of the day; 1 truck trip is assumed to arrive during the AM peak hour and depart during the PM peak hour for the purposes of this analysis. Ash removal would occur once every four days at Tuolumne.
- 4 Truck trips included the combined total of both ash removal and haul trucks across all sites within one day. All trucks use a PCE rate of 3.0 for the purposes of this analysis.

As shown in Table 2, the project would generate approximately 340 daily trips, 53 AM peak hour trips and 28 PM peak hour trips. After trip generation estimates were adjusted utilizing PCE factors, the project would generate approximately 816 daily trips, 83 AM peak hour trips, and 58 PM peak hour trips.

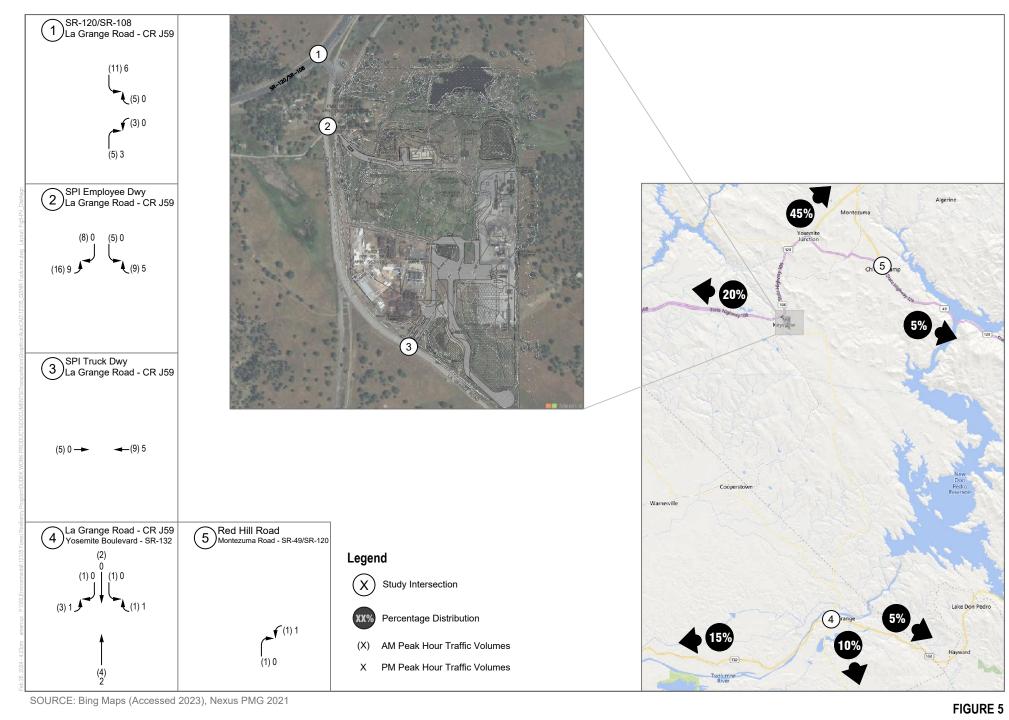
Construction of the facility is assumed to begin in late 2024 and will take approximately 14 months. During construction, the amount of vehicular traffic is estimated to be less than operational traffic. As such, all construction-related traffic would be temporary and short term and would be removed from the study area roadway network upon completion of the project, and is not included in this analysis.

## 3.2 Trip Distribution and Assignment

Regional project trip distribution percentages are based on logical travel paths to and from the project site, along with review of census data from the OnTheMap application<sup>2</sup> identifying the primary origin (home) locations of employees working within the census block group the Lassen Facility is located (see Appendix A). Project trip distribution percentages are shown in Figures 5 and 6, for passenger vehicle and truck trips, respectively. Project trips were assigned to the study area intersections by applying the above-referenced project trip generation estimates to the trip distribution percentages at each study area roadway segment and intersections. The project trip assignments are shown in Figures 5, 6, and 7 for passenger vehicle, truck, and total trip assignments, respectively.

<sup>&</sup>lt;sup>2</sup> The OnTheMap application is a web-based mapping and reporting application provided by the U.S. Census Bureau, which enables access to the Longitudinal Employer-Household Dynamics (LEHD) Origin-Destination Employment Statistics (LODES) dataset. OnTheMap can be access at <a href="https://onthemap.ces.census.gov/">https://onthemap.ces.census.gov/</a>.





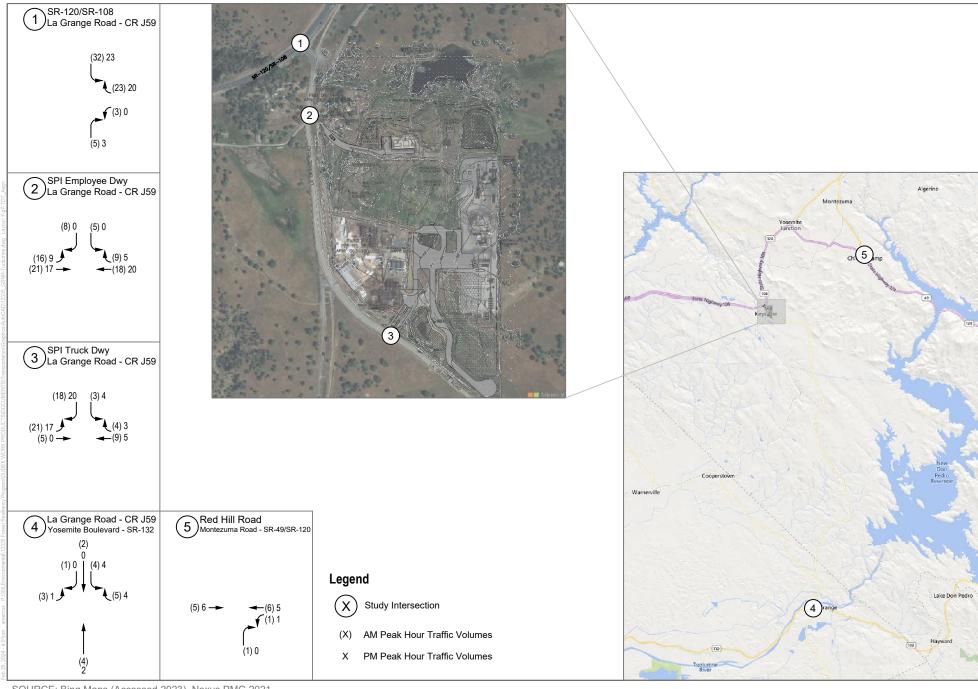












SOURCE: Bing Maps (Accessed 2023), Nexus PMG 2021



# 4 Level of Service (LOS) Analysis

The County has vehicle LOS policies to ensure that proposed developments are consistent with the County's General Plan. Therefore, an LOS analysis has been prepared to evaluate the project's consistency with the County's policies. The study intersections and roadway segments, analysis scenarios, traffic volumes, and LOS methodology and impact criteria are presented in the following section.

#### 4.1 Study Intersections and Roadway Segments

The following study intersections are included in the LOS analysis, based on proximity to the site and potential for turning movements from project traffic to occur:

- 1. SR-120 SR-108/La Grange Road CR J59 (two-way stop control)
- 2. Site Access Employee Dwy/La Grange Road CR J59 (two-way stop control)
- 3. Site Access Truck Dwy/La Grange Road CR J59 (two-way stop control)
- 4. La Grange Road CR J59/Yosemite Boulevard SR-132 (all-way stop control)
- 5. Red Hill Road/Montezuma Road SR-49 SR-120 (two-way stop control)

In addition, the following road segments were selected for analysis, based on anticipated routes and locations where the project may add the highest daily traffic volumes:

- 1. SR-120 SR-108, west of La Grange Road CR J59
- 2. La Grange Road CR J59, south of SR-120 SR-108

## 4.2 Analysis Scenarios

Intersection LOS analyses were prepared for the weekday AM and PM peak hours at the study area intersections and road segments listed above for the following analysis scenarios:

- Existing Conditions
- Existing Conditions Plus Project
- Opening Year (2025)
- Opening Year (2025) plus Project



#### 4.3 Traffic Volumes

Daily, AM and PM peak hour turning movements counts were collected at the study intersections on August 29, 2023. The raw traffic data<sup>3</sup> is provided as Appendix A. Traffic counts were adjusted to passenger car equivalents (PCE) to reflect truck traffic according to following industry standards as shown below:

Light-duty trucks (2-axle): 1.5 PCE

Medium-duty trucks (3-axle): 2.0 PCE

Heavy-duty trucks (4+-axle): 3.0 PCE

The Opening Year (2025) condition represents a short-term horizon period (less than 5 years) when the proposed project is under construction. The peak hour traffic forecasts for the Year 2025 have been projected by increasing the traffic volumes by an annual growth rate of 2.0% and adding cumulative project traffic. Four (4) cumulative projects (e.g., approved or pending developments in the review process, but not fully approved; or, projects that have been approved, but not fully constructed or occupied) were identified in the study area, and are further discussed in Chapter 6.1

#### 4.4 Operational Analysis Methodology

The Highway Capacity Manual, 6th Edition (HCM 6) methodology (Transportation Research Board 2016) was used to analyze the operation of signalized and unsignalized study intersections. Detailed LOS calculation worksheets, for each scenario analyzed, are included in Appendix B.

The HCM analysis methodology describes the operation of an intersection using a range of LOS from LOS A (free-flow conditions) to LOS F (severely congested conditions), based on the corresponding control delay experienced per vehicle for unsignalized intersections. The Synchro 11 LOS software was used to determine intersection LOS. Synchro is consistent with the HCM 6 methodology. Table 3 shows the LOS values by delay ranges for unsignalized and signalized intersections under the HCM methodology.

**Table 3. Levels of Service for Intersections using HCM Methodology** 

Level of Service	Unsignalized Intersections Control Delay (in seconds per vehicle)	Signalized Intersections Control Delay (in seconds per vehicle)
A	<u>≤</u> 10.0	≤ 10.0
В	> 10.0 to < 15.0	> 10.0 to < 20.0
С	> 15.0 to < 25.0	> 20.0 to < 35.0
D	> 25.0 to < 35.0	> 35.0 to < 55.0
E	> 35.0 to < 50.0	> 55.0 to < 80.0
F	> 50.0	> 80.0

<sup>3</sup> Counts were not collected at the Site Access Driveway North location (Intersection #2); however, volumes along this roadway are relatively low, and volumes from upstream and downstream through movements at adjacent intersections were balanced and utilized at this intersection.

Source: HCM 6 (Transportation Research Board 2016).

Roadway capacities along study area and haul route roadways were determined from Appendix D (Traffic Study) of the Tuolumne County General Plan Update DEIR (August 2016), which provides general capacity thresholds for various roadway type characteristics, including various Federal Highway Association (FHWA) functional classes as utilized by Caltrans.

Daily volume capacities are referenced for LOS "D" capacities in the Appendix Table 2 LOS Look Up Table of the Appendix D Traffic Study, and selected based on the appropriate descriptions. As noted in the Appendix Table 2 (also included in Appendix C of this TIS), all volumes thresholds are approximate and assumes average roadway characteristics. Actual threshold volume for each Level of Service listed in the table may vary depending on variety of factors including (but not limited to) roadway curvature and grade, intersection or interchange spacing, driveway spacing, percentage of trucks, RVs, and other heavy vehicles, travel lane widths, speed limits, signal timing characteristics, on-street parking, volume of cross traffic and pedestrians, etc.. as identified in HCM.

The volume-to-capacity (V/C) and LOS thresholds, where capacity is determined based on the roadway classifications noted above, are provided in Table 4.

**Table 4. Levels of Service for Roadway Segments** 

Level of Service	Roadway Segments V/C Ratio
Α	0.00 - 0.60
В	0.61 - 0.70
С	0.71 - 0.80
D	0.81 - 0.90
E	0.91 - 1.00
F	1.01 or greater

Source: HCM 6 (Transportation Research Board 2016).

Notes: V/C = Volume-to-Capacity

# 4.5 Tuolumne County General Plan Consistency Requirements

Tuolumne County uses a threshold of LOS D for the minimum acceptable operation of its transportation facilities. The County's General Plan Transportation Element (Tuolumne County 2018) contains the following policies related to transportation compliance and LOS requirements:

The Transportation Element of the Tuolumne County General Plan (2018) provides the framework for decisions in Tuolumne County concerning the countywide transportation system. Specific goals and policies identified in the Transportation Element that are relevant to the proposed project are identified below.

- Goal 4A. Preserve the County's substantial investment in the existing road system and provide for the long-range planning and development of the County's transportation system for the safe and efficient movement of people and goods.
  - Policy 4.A.1: Support and work with the TCTC to regularly conduct assessments of the current status of the highway system to determine the current level of needs in the system, and report those needs to the Board of Supervisors.
    - Policy 4.A.a. Plan, design and regulate roadways in accordance with the following functional classification system and designations which are reflected in the County's Regional Transportation Plan, and are shown on the Master Plan of Streets and Highways in Chapter 4 of the General Plan Technical Background Report:
      - Other Freeways and Expressways (Functional Class Code 2)
      - Other Principal Arterial (Functional Class Code 3)
      - Minor Arterial (Functional Class Code 4)
      - Major Collector (Functional Class Code 5)
      - Minor Collector (Functional Class Code 6)
      - Local Road (Functional Class Code 7)
      - Scenic Routes
      - Urban Streets
    - Policy 4.A.b. Develop and manage the County's roadway system to maintain the following minimum levels of service (LOS)<sup>4</sup> using methodology adopted by the Tuolumne County Transportation Council:
      - Arterials, Minors Collectors, Major Collectors, Urban Streets: LOS D, unless an exception is made
      - Local Road: LOS C
      - Minimum Peak Hour of all Intersections: LOS D
    - Policy 4.A.c. Establish priorities based on available funding for road improvement projects while balancing the need to support employment generating uses, affordable housing, and educational facilities. Emphasize, consistent with legal and funding constraints, the following road improvement projects in the County Road Improvement Program:
  - Policy 4.A.2: Dedicate, widen and construct roads according to design and access standards generally defined in Chapter 4 of the General Plan Technical Background Report and, more specifically, the County Ordinance Code and the Countywide Traffic Circulation Improvement Program. Exceptions

<sup>&</sup>lt;sup>4</sup> The County may allow exceptions to these level of service standards where it finds that the improvements or other measures required to achieve the LOS standards are unacceptable. In allowing any exception to the standards, the County shall consider the following factors, including congestion/delays, rights of way, environmental impacts, safety, aesthetics, alternative transportation modes, and other geographical, environmental, social or economic factors on which the County may base findings to allow an exceedance of the standards. Exceptions to the standards will only be allowed after all reasonably feasible measures and options are explored.



to these standards may be necessary and shall be approved by the Community Resources Agency Director, who shall ensure that safe and adequate public access and circulation are preserved by such exceptions.

- Policy 4.A.g. Require local roads serving new development to be aligned with existing local roads on abutting properties and extend existing roads to link with other roads wherever possible to provide continuity and provide safety in the local road system.
- Policy 4.A.h. Accommodate through traffic in a manner that discourages the use of neighborhood Local Roads. This through traffic, particularly truck traffic, shall be directed to appropriate routes in order to maintain public safety and local quality of life by using design measures, such as appropriate signage and traffic calming devices.
- Policy 4.A.i. Maximize intersection spacing on arterial and collector roadways and thoroughfares and minimize driveway encroachments. Except where specific site conditions warrant, no new intersection of a local road or new driveway with an arterial or collector road shall be closer to an existing local road or driveway than 500 feet in rural areas or 200 feet within urban areas.
- Policy 4.A.5: Consider the traffic impacts of development in relation to General Plan growth policies and require new development to provide mitigation for its fair share of impacts to the County's transportation system. Assess the needs of street and road users regularly through the land development application review process.
  - Policy 4.A.p. Evaluate and analyze the traffic impacts of proposed land uses in relation to stated goals and objectives of the General Plan since growth policies regarding land use decisions directly affect the existing and future transportation system.
  - Policy 4.A.q. Evaluate the impacts of new development on the County's transportation system and require such development to provide mitigation for its fair share of the impact. New development that is determined by the County to create or exacerbate an identified deficiency in the transportation system may not be approved if a plan and funding program to provide needed roadway improvements have not been approved and if the mitigation provided by the development will not correct the deficiency or if it will create an additional burden on County transportation funds. This implementation program shall not apply to new development for which the County makes a finding of overriding considerations for traffic impacts related to the new development in accordance with the California Environmental Quality Act.
  - Policy 4.A.r. Implement Vehicles Miles Traveled for evaluating transportation impacts under CEQA to be consistent with SB 743.
- Policy 4.A.6: Strive to maintain all components of the transportation system at adopted level of service standards.



Policy 4.A.t. Require new development to mitigate that development's impacts on the local and regional transportation system through the fair share contribution of improvements to the master planned system and/or the payment of Traffic Impact Mitigation Fees. Exceptions to the payment of traffic impact mitigation fees may apply to land uses listed in the Traffic Impact Mitigation Fee Schedule or when alternative sources of funding can be identified to offset foregone revenues.

Goal 4B. Encourage the use of alternative means of transportation by providing safe bicycle and pedestrian facilities within urban development boundary areas and between identified communities thereby reducing road congestion which improves circulation, health and air quality within the County.

#### Tuolumne County Regional Transportation Plan (RTP)

The Tuolumne County Regional Transportation Plan (RTP) was prepared for the Tuolumne County Transportation Commission (TCTC) to identify future transportation improvement projects and funding throughout the County (TCTC 2017). The RTP provides general regional transportation goals and proposed transportation improvement projects consistent with those goals. The applicable regional goals listed in the RTP are identified below and reviewed in Section 3.14.4.

- Regional Goal 1: Enhance the quality of life of Tuolumne County residents by providing transportation access to jobs, housing, recreation, and community services.
- Regional Goal 5: Practice environmental stewardship by protecting our air quality, natural resources, historical and cultural assets.
- Regional Goal 6: Integrate land use and transportation decisions by prioritizing infrastructure investments within the Defined Community Boundaries that strikes a balance between development, available infrastructure, conserves natural resources, and provides for a high quality of life.
- Regional Goal 7: Consider transportation safety, and security in all transportation funding decisions.
- Regional Goal 8: Support a vibrant economy by enhancing the movement of goods and people to spur economic development, growth, and job creation.

Tuolumne County Active Transportation Plan (ATP) 2020

The Tuolumne County Active Transportation Plan (ATP) 2020 was prepared by the Tuolumne County Transportation Council, and outlines needs, goals, and objectives to promote and maintain a reliable, flexible, and multimodal transportation system for Tuolumne County residents, and is consistent with the General Plan. The ATP identifies the following primary goals as they relate to the active transportation network:



- Goal 1. Develop a transportation system that maximizes the use of transportation facilities in the most efficient and cost-effective way.
- Goal 2. Plan for a balanced multimodal transportation network that meets the needs of all users of streets, roads, and highways for safe and convenient travel.
- Goal 3. Plan, support, and implement Smart Mobility Framework and Context Sensitive Solutions

#### 4.6 California Public Utilities Commission

The Public Utilities Commission of the State of California (PUC) includes Regulations Governing Standards for Warning Devices for At-Grade Highway-Rail Crossings pursuant to General Order (G.O.) No. 75-D, adopted August 24, 2006; effective September 23, 2006. Development of the Tuolumne Facility Site would include the repaving and reopening of an existing driveway (currently gated and overgrown) for employee vehicle access located at the northwestern corner of the site. This crossing would occur on GSNR's privately-owned land, and would be subject to Section 7 (Private At-Grade Crossings) of G.O. No. 75-D, which includes the following regulations:

#### 7. Private at-grade crossings

- 7.1 Pursuant to Public Utilities Code Section 7537, the Commission has the authority to determine the necessity for any private at-grade crossing and the place, manner, and conditions under which the at-grade crossing shall be constructed and maintained, and to fix and assess the cost and expense thereof. The Commission exercises such jurisdiction when it is either petitioned by one of the parties or Commission staff.
- 7.2 The establishment of a private at-grade crossing, other than a private at-grade crossing of the railroad tracks by the owning railroad, must be authorized through a written agreement between the railroad and the party requiring the crossing.
- 7.3 Standard 1-X. "PRIVATE CROSSING" sign shall be installed at all private at-grade crossings. See Figure 6 for additional specifications.
- 7.4 At all approaches to private at-grade crossings there shall be installed either a STOP sign (defined as a Standard R1-1 in the CA MUTCD) or an automatic warning device described in Sections 6.2 through 6.6.
  - a) If a STOP sign is used, the Standard 1-X sign shall be mounted on the post below it.
  - b) If a Standard 8, 8-A, 9, 9-A, or 9-E device is used, the Standard 1-X sign shall be attached to the mast of the warning device below the flashing light signals.
- 7.5 The language contained in the lower portion of the "PRIVATE CROSSING" sign shown in Figure 6 (in Public Utilities Code Section 7537), commencing with, and including the words "No Trespassing", shall be permitted at the option of the railroad.



# 4.7 Caltrans Transportation Impact Study Guide

As the owner and operator of the State Highway System, Caltrans, implements established state planning priorities in all functional plans, programs, and activities. Caltrans has the responsibility to coordinate and consult with local jurisdictions when proposed local land use planning and development may impact state highway facilities. To comply with SB 743 implementation, the Caltrans Transportation Impact Study Guide (May 2020), replaced the Guide for the Preparation of Traffic Impact Studies (Caltrans 2002). Per the 2020 Transportation Impact Study Guide, Caltrans' primary review focus is VMT, replacing LOS as the metric used in CEQA transportation analyses. Caltrans recommends use of OPR's recommended thresholds and guidance on methods of VMT assessment found in OPR's Technical Advisory (OPR 2018). In addition to VMT, Caltrans has developed an Interim Land Development and Intergovernmental Review Safety Review Practitioners Guidance which may request a targeted operational and safety analysis to address a specific geometric or operational issue related to the State Highway System and connections with the State Highway System (Caltrans 2020). To comply with this requirement, an assessment of queuing at study area intersections adjoining to roadways within the State Highway System has been included in this TIS.



# 5 Existing (2023) Conditions Analysis

This section details the existing intersection and roadway segment operations within the study area, with and without the project-added traffic. Existing traffic controls and geometrics at all study intersections are shown in Figure 8 and existing peak hour traffic volumes are shown in Figure 9. The existing plus project traffic volumes are shown on Figure 10.

# 5.1 Intersection Operations

Table 3 summarizes the results of the intersection analysis for the AM and PM peak hours for existing conditions. As shown in the table, all of the study intersections are currently operating at satisfactory levels of service (LOS D or better) under existing conditions and will continue to operate at satisfactory LOS with the project-added traffic.

**Table 3. Existing plus Project Weekday Peak Hour Intersection LOS** 

			Existing				Existing plus Project			
		Traffic	AM Pea	k	PM Pea	k	AM Pea	k	PM Pea	k
No. Intersection	Control	Delay1	LOS <sup>2</sup>	Delay <sup>1</sup>	LOS <sup>2</sup>	Delay <sup>1</sup>	LOS <sup>2</sup>	Delay <sup>1</sup>	LOS <sup>2</sup>	
1	SR-120 - SR-108/La Grange Road - CR J59	TWSC	21.2	С	22.8	С	24.1	С	24.5	С
2	Site Access Employee Dwy/La Grange Road - CR J59	TWSC	0.0	А	0.0	А	10.1	В	7.5	А
3	Site Access Truck Dwy/La Grange Road - CR J59	TWSC	9.4	А	7.5	А	9.7	А	9.4	Α
4	La Grange Road - CR J59/Yosemite Boulevard - SR-132	AWSC	8.4	А	8.4	А	8.5	А	8.5	А
5	Red Hill Road/Montezuma Road - SR-49 - SR-120	TWSC	10.2	В	10.8	В	10.3	В	10.9	В

Notes: HCM = Highway Capacity Manual; TWSC = Two-Way Stop-Controlled; X - Unsatisfactory operating conditions/LOS

#### 5.2 Roadway Segment Operations

#### Study Area Roadway Segments

Table 4 shows the results of the roadway segment LOS analysis. As shown below, the study area roadway segments are operating at acceptable ADT volume-to-capacity conditions under existing conditions, with and without the project-added traffic.

Delay in seconds per vehicle

<sup>2</sup> Level of Service (LOS)

**Table 4. Existing ADT Roadway Segment Level of Service** 

No.	Location	Capacity <sup>1</sup>	Existing ADT <sup>2</sup>	V/C Ratio	LOS	Project- Added Trips	Existing plus Project ADT	V/C Ratio	LOS	LOS D or Better?
1.	SR-120 - SR-108, west of La Grange Road - CR J59	19,550	14,535	0.743	С	20	14,555	0.745	С	Yes
2.	La Grange Road - CR J59, south of SR-120 - SR-108	13,260	4,212	0.318	A	674	4,886	0.368	A	Yes

Notes: ADT = average daily traffic; V/C = volume/capacity; Bold: Exceeds "Acceptable" LOS E or better threshold

- Capacity determined from Appendix D (Traffic Study) of the Tuolumne County General Plan Update DEIR (August 2016).
- Volume provided from average daily traffic (ADT) counts conducted on August 29, 2023

#### **Haul Routes**

Feedstock would be sourced within the Working Area, as described in Section 2.4 of the DEIR, and the primary haul routes identified in Figure 4 would be used to transport raw materials to the Tuolumne Facility. Although the specific locations of any given logging operation is unknown at this time, and it is expected that biomass acquisition would be spread out in different locations across the Working Area, representative locations along the haul routes identified in Chapter 2.1 are tabulated below, and the total average daily project haul trucks were added to the existing Caltrans counts at each location. As shown in Table 5 and illustrated in Figure 14, all locations would operate with acceptable conditions with and without the addition of total project haul trucks under Existing conditions.



Table 5. Representative Haul Routes and Levels of Service - Existing

Haul Route	Caltrans Postmile	Latitude	Longitude	Existing ADT	V/C Ratio	LOS	Project-Added Trips (Logging/Haul Trucks)	Existing plus Project ADT	V/C Ratio	LOS
Hwy 4	29.62	38.139059	-120.456141	7,283	0.362	Α	236	7,519	0.374	А
Hwy 4	18.556	38.067128	-120.59894	510	0.038	Α	236	746	0.056	А
Hwy 41	17.91	37.12444	-119.736963	16,646	0.813	D	236	16,882	0.824	D
Hwy 49	1.65	38.573869	-120.846136	2,133	0.161	Α	236	2,369	0.179	Α
Hwy 49	9.42	38.087694	-120.57103	8,011	0.604	В	236	8,247	0.622	В
Hwy 49	29.45	37.569309	-120.119433	895	0.045	Α	236	1,131	0.056	Α
Hwy 50	20.296	38.731226	-120.76013	25,282	0.340	Α	236	25,518	0.343	Α
Hwy 50	65.619	38.824307	-120.044235	16,126	0.887	D	236	16,362	0.900	D
Hwy 88	1.25	38.704996	-120.050932	2,549	0.207	Α	236	2,785	0.226	Α
Hwy 88	22.69	38.412824	-120.667363	12,485	0.639	В	236	12,721	0.651	В
Hwy 108	7.511	37.996508	-120.267276	10,924	0.412	Α	236	11,160	0.421	Α
Hwy 108	9.6	38.350174	-119.536286	1,613	0.131	Α	236	1,849	0.150	А
Hwy 120	32.184	37.838293	-120.231647	8,947	0.675	В	236	9,183	0.693	В
Hwy 120	8.19	37.84335	-120.508081	13,421	0.686	В	236	13,657	0.699	В
Hwy 132	7.58	37.706276	-120.334027	1,509	0.114	Α	236	1,745	0.132	Α
Hwy 132	45.81	37.661141	-120.483363	1,769	0.133	Α	236	2,005	0.151	Α
Hwy 140	29.689	37.564499	-119.939815	2,653	0.215	Α	236	2,889	0.234	Α
Hwy 168	15.47	36.873802	-119.557381	7,283	0.549	Α	236	7,519	0.567	А
Hwy 168	65.84	37.255427	-119.161485	1,144	0.093	Α	236	1,380	0.112	А
Road CR J59		37.840655	-120.507755	3,155	0.287	А	236	3,391	0.308	А

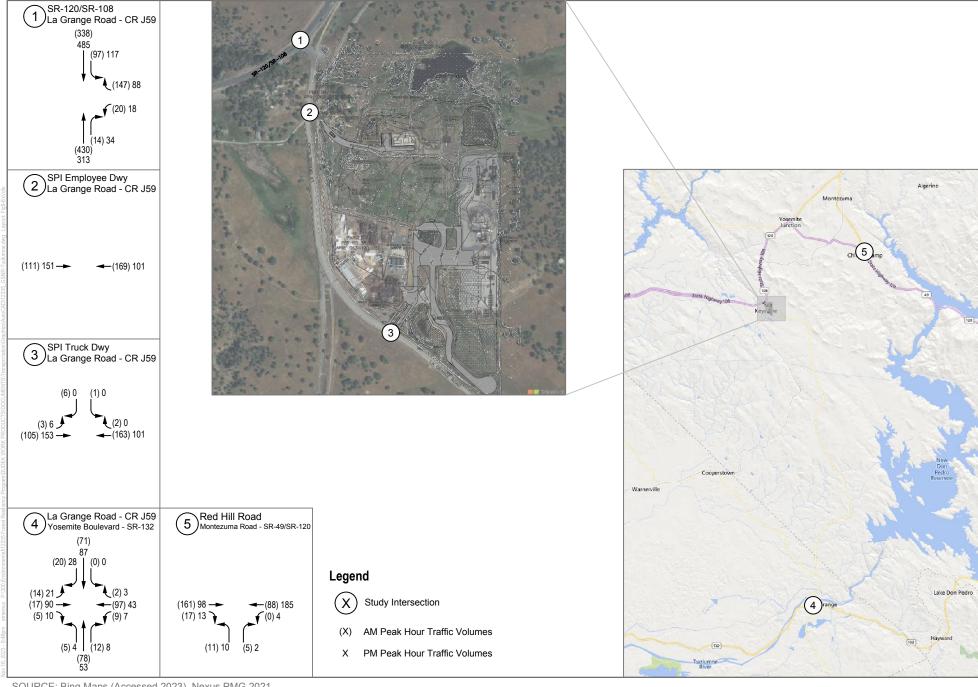
Source: Appendix C



SOURCE: Bing Maps (Accessed 2023), Nexus PMG 2021



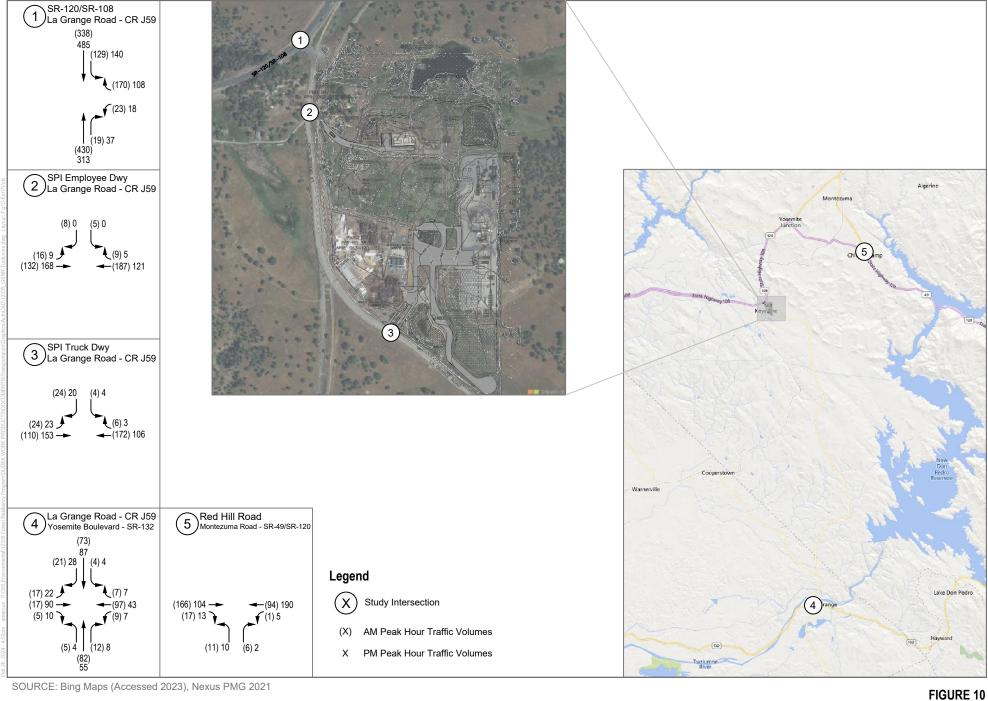




SOURCE: Bing Maps (Accessed 2023), Nexus PMG 2021





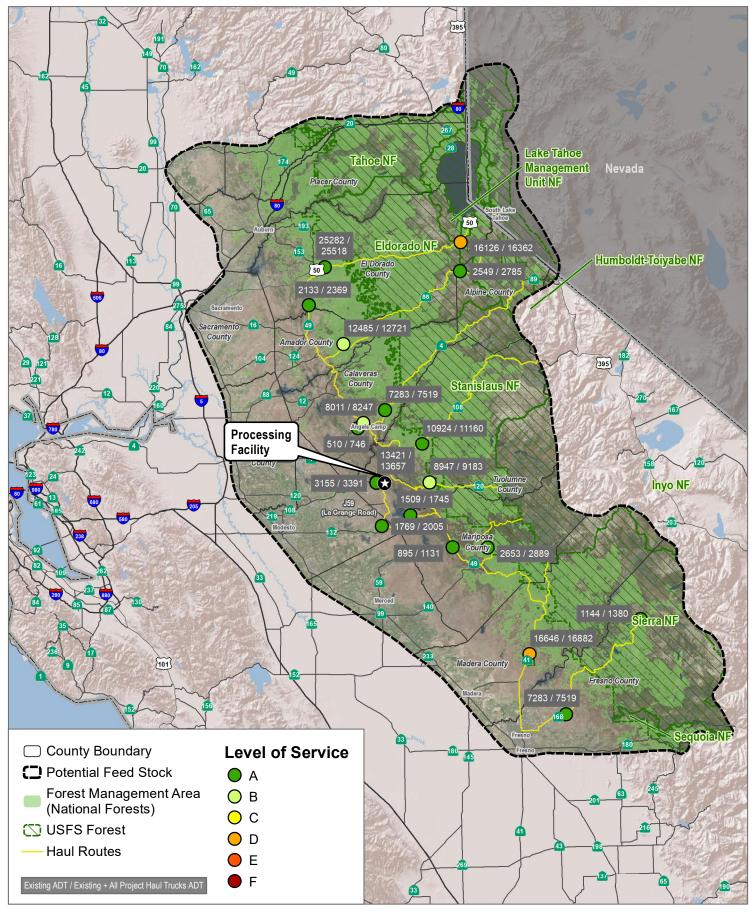


SOURCE: Bing Maps (Accessed 2023), Nexus PMG 2021









SOURCE: Bing Maps 2022; Caltrans 2021

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FIGURE 11



# 6 Opening Year (2025) Analysis

This section describes conditions within the study area in the short-term (estimated to be year 2025) when construction of the project and cumulative projects in the area would occur. The existing intersection configurations (shown in Figure 8) have been assumed to be preserved under the Opening Year (2025) conditions.

## 6.1 Cumulative Projects

Cumulative projects are projects that are proposed and in the development review process, but not yet fully approved; or projects that have been approved, but not fully constructed or occupied. Four (4) cumulative projects were identified near the proposed Tuolumne Facility. Project trip generation for the cumulative projects were estimated using trip generation rates provided by the ITE Trip Generation Handbook, 11th Edition, or derived from traffic impact analyses, where available. As shown in Appendix D, the cumulative projects are forecast to generate approximately 3,077 daily trips, 313 AM peak hour trips, and 399 PM peak hour trips. Adjusting for PCE, the cumulative projects would generate approximately 3,577 daily trips, 383 AM peak hour trips, and 467 PM peak hour trips.

Figure 12 shows the locations of all cumulative projects, along with the traffic volumes distributed throughout the network.

## 6.2 Intersection Operations

The existing intersection configurations have been assumed to be preserved under the Opening Year (2025) conditions. Figure 13 illustrates the Opening Year (2025) (no project) traffic volumes for the peak hour conditions and Figure 14 illustrates the Opening Year (2025) (with project) traffic volumes for the peak hour conditions.

Table 6 summarizes the results of the Opening Year (2025) intersection analysis for the AM and PM peak hours, with and without the project. As shown in the table, all study area intersections are forecast to operate at satisfactory levels of service (LOS D or better) under Opening Year (2025) conditions with and without the project-added traffic.

Table 6. Opening Year (2025) Weekday Peak Hour Intersection LOS

			Opening	g Year (	2025)		Opening Year (2025) Plus Project					
		Traffic	AM Peak		PM Peak		AM Peak		PM Peak			
No.	o. Intersection	Control	Delay1	LOS <sup>2</sup>	Delay1	LOS <sup>2</sup>	Delay1	LOS <sup>2</sup>	Delay <sup>1</sup>	LOS <sup>2</sup>		
1	SR-120 - SR-108/La Grange Road - CR J59	TWSC	25.3	D	31.4	D	29.0	D	34.4	D		
2	Site Access Employee Dwy/La Grange Road - CR J59	TWSC	0.0	A	0.0	A	10.5	В	7.6	A		

Table 6. Opening Year (2025) Weekday Peak Hour Intersection LOS

			Openin	g Year (	2025)		Opening Year (2025) Plus Project				
		Traffic	AM Peak		PM Peak		AM Pea	k	PM Peak		
No.	Intersection	Control	Delay <sup>1</sup>	LOS <sup>2</sup>	Delay1	LOS <sup>2</sup>	Delay1	LOS <sup>2</sup>	Delay1	LOS <sup>2</sup>	
3	Site Access Truck Dwy/La Grange Road - CR J59	TWSC	9.7	A	7.5	A	10.0	В	9.6	А	
4	La Grange Road - CR J59/Yosemite Boulevard - SR-132	AWSC	8.7	A	8.6	A	8.7	А	8.7	А	
5	Red Hill Road/Montezuma Road - SR-49 - SR- 120	TWSC	10.7	В	11.6	В	10.8	В	11.7	В	

Notes: HCM = Highway Capacity Manual; TWSC = Two-Way Stop-Controlled; X - Unsatisfactory operating conditions/LOS

## 6.3 Roadway Segment Operations

Table 7 shows the results of the roadway segment LOS analysis. As shown below, the study area roadway segments are forecast to operate at acceptable conditions under Opening Year (2025) conditions, with and without the project traffic.

Table 7. Opening Year (2025) ADT Roadway Segment Level of Service

No.	Location	Capacity <sup>1</sup>	Opening Year (2025) ADT <sup>2</sup>	V/C Ratio	LOS	Project- Added Trips	Opening Year (2025) plus Project ADT	V/C Ratio	LOS	LOS D or Better?
1.	SR-120 - SR-108, west of La Grange Road - CR J59	19,550	16,169	0.827	D	20	16,189	0.828	D	Yes
2.	La Grange Road - CR J59, south of SR-120 - SR-108	13,260	4,890	0.369	A	674	5,564	0.420	A	Yes

Notes: ADT = average daily traffic; V/C = volume/capacity; Bold: Exceeds "Acceptable" LOS E or better threshold

#### **Haul Routes**

As noted above, although the specific locations of any given logging operation is unknown at this time, and it is expected that biomass acquisition would be spread out in different locations across the Working Area,

Delay in seconds per vehicle

<sup>2</sup> Level of Service (LOS)

Capacity determined from Appendix D (Traffic Study) of the Tuolumne County General Plan Update DEIR (August 2016).

Volume provided from average daily traffic (ADT) counts conducted on August 29, 2023

representative locations along the haul routes identified in Chapter 2.1 are tabulated below, and the total average daily project haul trucks were added to the existing Caltrans counts at each location.

As shown in Table 8 and illustrated in Figure 14, all locations would operate with acceptable conditions with and without the addition of total project haul trucks under Opening Year (2025) conditions, with exception of the segment selected for US-50 at Caltrans Postmile 65.619. However, the segment is forecast to operate at LOS E under baseline Opening Year (2025) conditions, and the increase between with and without project conditions is minimal (1.2%, or an increase of 0.012 V/C). Additionally, this increase would not result in a change in LOS grade, and LOS along this segment would remain at E with the addition of all haul truck trips.

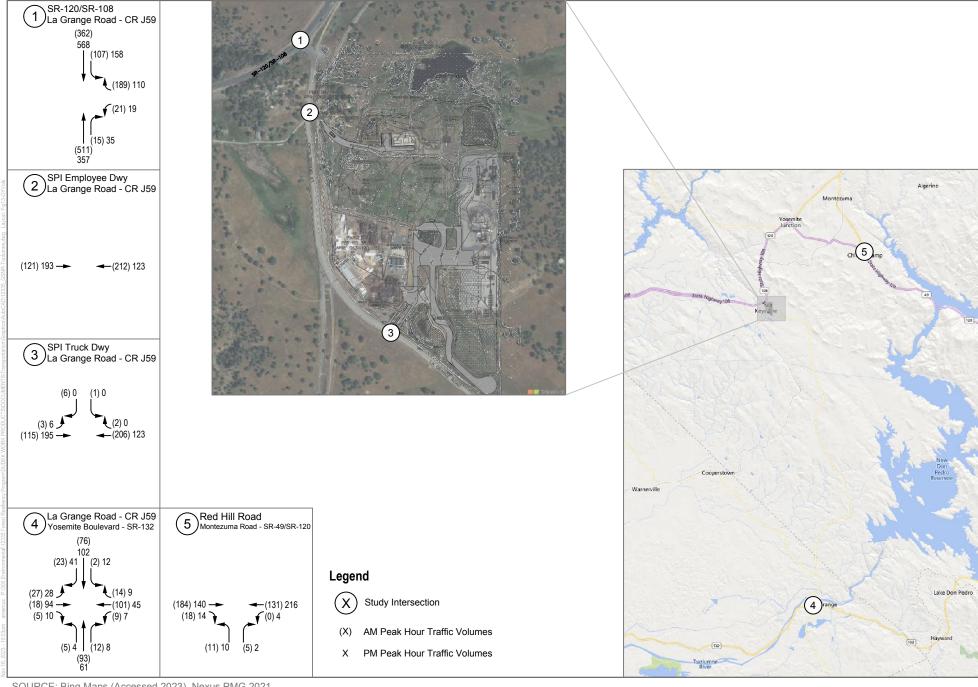


Table 8. Representative Haul Routes and Levels of Service - Opening Year (2025)

Haul Route	Caltrans Postmile	Latitude	Longitude	Opening Year (2025) ADT	V/C Ratio	LOS	Project-Added Trips (Logging/Haul Trucks)		V/C Ratio	LOS
SR-4	29.62	38.139059	-120.456141	7,577	0.377	Α	236	7,813	0.389	А
SR-4	18.556	38.067128	-120.59894	531	0.040	А	236	767	0.058	А
SR-41	17.91	37.12444	-119.736963	17,318	0.845	D	236	17,554	0.857	D
SR-49	1.65	38.573869	-120.846136	2,219	0.167	Α	236	2,455	0.185	А
SR-49	9.42	38.087694	-120.57103	8,335	0.629	В	236	8,571	0.646	В
SR-49	29.45	37.569309	-120.119433	931	0.046	Α	236	1,167	0.058	А
US-50	20.296	38.731226	-120.76013	26,303	0.354	А	236	26,539	0.357	А
US-50	65.619	38.824307	-120.044235	16,777	0.922	E	236	17,013	0.935	E
SR-88	1.25	38.704996	-120.050932	2,652	0.215	Α	236	2,888	0.234	А
SR-88	22.69	38.412824	-120.667363	12,989	0.664	В	236	13,225	0.676	В
SR-108	7.511	37.996508	-120.267276	11,365	0.429	Α	236	11,601	0.437	А
SR-108	9.6	38.350174	-119.536286	1,678	0.136	А	236	1,914	0.155	А
SR-120	32.184	37.838293	-120.231647	9,308	0.702	С	236	9,544	0.720	С
SR-120	8.19	37.84335	-120.508081	13,963	0.714	С	236	14,199	0.726	С
SR-132	7.58	37.706276	-120.334027	1,570	0.118	Α	236	1,806	0.136	А
SR-132	45.81	37.661141	-120.483363	1,840	0.139	Α	236	2,076	0.157	Α
SR-140	29.689	37.564499	-119.939815	2,760	0.224	Α	236	2,996	0.243	А
SR-167	15.47	36.873802	-119.557381	7,577	0.571	Α	236	7,813	0.589	Α
SR-168	65.84	37.255427	-119.161485	1,190	0.096	Α	236	1,426	0.116	А
Road CR J59		37.840655	-120.507755	3,282	0.298	Α	236	3,518	0.320	А

Source: Appendix C

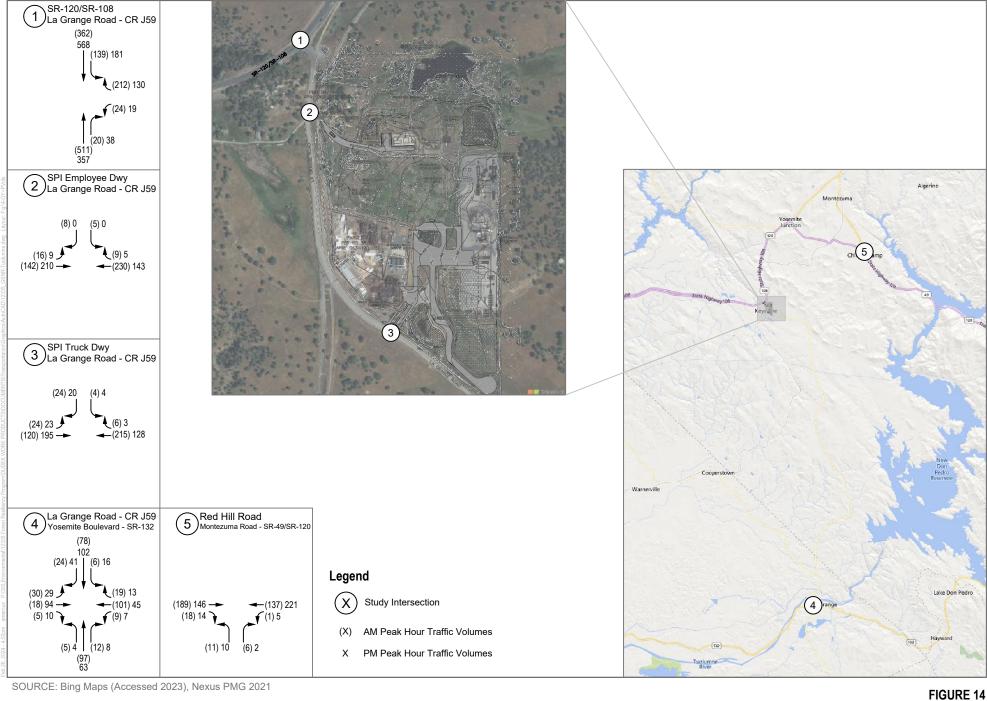




SOURCE: Bing Maps (Accessed 2023), Nexus PMG 2021



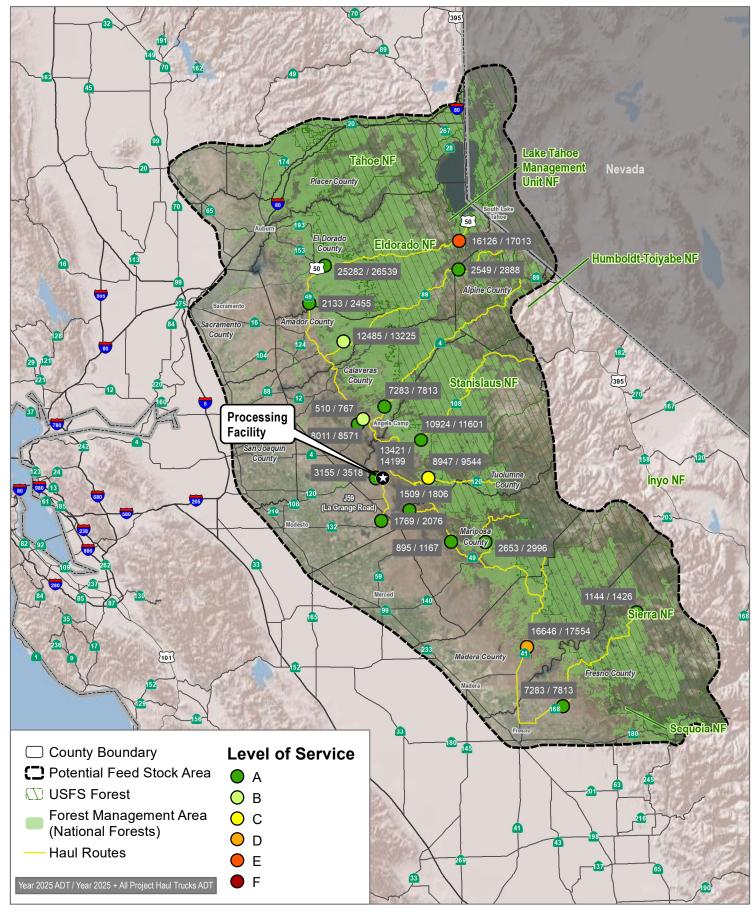












SOURCE: Bing Maps 2022; Caltrans 2021

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FIGURE 15



# 7 Project Site Access

### 7.1 Vehicular Site Access and Circulation

Vehicular and truck traffic access into the site will be provided via two existing roadways from La Grange Road – CR J59 (analyzed as intersections #2 and #3), as shown in Figure 1, Project Location and Study Area. All study area intersections have been analyzed as unsignalized intersections with stop control at the minor approach where applicable.

### 7.1.1 Project Site Access

Figure 2 illustrates the vehicular and truck traffic access, as indicated below:

- Intersection #2 via Site Access Driveway North (currently undeveloped) full access; passenger vehicles
- Intersection #3 via Site Access Driveway North (currently operational) full access; trucks

#### Truck Access

Truck traffic will utilize the SR-108/120 intersection with La Grange Road to the north (Intersection #1) and the SR-132 intersection with La Grange Road to the south (Intersection #4) to access the site via the existing driveway noted above (Intersection #3).

In Tuolumne County, SR-108 and SR-120 have terminal access, and allow the use of both STAA and California legal trucks. However, in Mariposa County, SR-120 allows only trucks that are no longer than 65 feet as per the kingpin-to-rear-axle (KRPA) advisory. Additionally, SR-132 to the south is a Caltrans designated truck route; however, east of the City of Modesto, SR-132 allows only trucks that are no longer than 65 feet as per the California Legal Route, and east of the La Grange Road intersection, a 30-foot kingpin to rear axle (KPRA) advisory sign is posted.

To verify that sufficient turning radii and pavement right-of-way (ROW) is available, a truck turn analysis using AutoTURN 2024 software has been completed to show the largest potential trucks (chip trucks) accessing the site, along with the most common log trucks.

- WB-62 Truck (Project Chip Trucks): AASHTO WB-62 design vehicles are representative of "Green" STAA Trucks allowed on SR-108/120 with a 48-foot semitrailer. Although up to 53-foot maximum semitrailers are allowed along on STAA routes, project operations would not include trucks larger than a WB-62. As shown in Figure 16, the WB-62 design vehicle would be able to maneuver the major highway intersections within the pavement provided, although may encroach over lane striping. It must be noted that the project is unlikely to utilize the La Grange Road/SR-132 intersection to the south for any project chip truck operations. The standard WB-62 design vehicle turning template is included to provide a conservative analysis at both intersections.
- WB-62 Truck with 30-foot KPRA and 44-foot semitrailer (Project Chip Trucks): AASHTO WB-62 design vehicle, modeled with an adjustment to the semitrailer length to represent a "Black" California Legal Truck, with an overall length of 65 feet. Additionally, due to the 30-foot KPRA advisory noted on SR-132 east of La

Grange Road, an additional adjustment has also been made. As shown in Figure 17, the WB-62 design vehicle with 30-foot KPRA adjustment would also be able to maneuver the major highway intersections within the pavement provided, with a slightly better turning radius than the standard WB-62, although may continue to encroach over lane striping. As noted above, the project is unlikely to utilize the La Grange Road/SR-132 intersection to the south for any project chip truck operations. This turning template, modeled with an adjustment to the overall length and KPRA given the advisory on SR-132, is included to provide a more representative truck for project operations at both intersections.

- Transcraft 45-foot Flatdeck (Project Pulp Log Trucks): A Transcraft TL-2000 45-foot flatdeck truck from has been used to represent the 45-foot fixed-axle pulp log trailers used in the project's logging operations. This truck represents the most common truck to be used in logging operations as most roundwood logs range from 16- to 20-feet long. As shown in Figure 18, this 45-foot fixed-axle truck would be able to maneuver the major highway intersections within the pavement provided, although may continue to encroach over some lane striping.
- Transcraft 45-foot Flatdeck with Rear Axle Steering (Project Standard Log Trucks): The Transcraft TL-2000 45-foot flatdeck truck, modeled with rear axle steering and a 35-foot distance between axles (representing the placement of upright log "bunks"), has been used to represent the standard log trailers used in the project's logging operations, representing approximately 30- to 40-percent of project log trucks. As shown in Figure 19, these log trucks with rear axle steering have the greatest maneuverability, and would encroach over minimal lane stripping.

Although the largest design trucks included in this turn analysis may encroach over lane striping, sufficient pavement ROW is provided at both intersections such that trucks would not be required to encroach into opposing traffic waiting at stop-controlled approaches (e.g., La Grange Road approach to SR-108/120 and SR-132 westbound approach to La Grange Road).

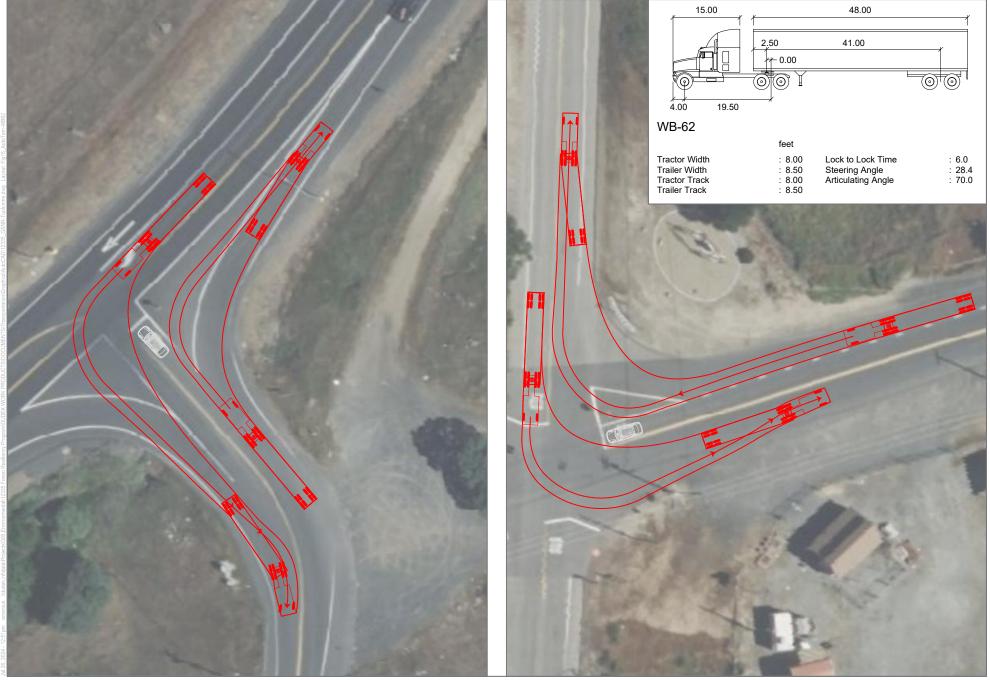
#### **Employee Access**

The proposed employee access road would be located along an existing (gated) driveway, currently overgrown and not utilized for vehicles. The alignment extends from La Grange Road, and would cross the railroad tracks at an at-grade crossing approximately 65-feet from the current edge of lane striping. As such, this crossing and any proposed improvements would be subject to the Public Utilities Commission Regulation, General Order No. 75-D (7), as noted in Chapter 4.6. The project site property is subject to a recorded agreement for utilization of the railroad crossing at Mile Post 29.5 of the Oakdale-Sonora Branch, dated March 20, 2014. The agreement is effective for 20 years, and would not require renewal until 2034; therefore, the project would be consistent with PUC regulations at this railroad crossing. Emergency Access

As previously discussed, access to the project site would be provided from the SR-120-SR-108/La Grange Road-CR J59 intersection, and at driveways along La Grange Road, utilizing the existing southerly driveway to the project site for truck access and the existing northerly driveway for employee access. The northerly driveway would be paved and improved to meet the County's access standards. All project access improvements would be reviewed by Tuolumne County. This approach would ensure compliance with all applicable design requirements. As mentioned above, the project has two main access roadways into the site, and in the event of an emergency, all the driveways would enable vehicles to enter/exit the project site. In the

event of an emergency during switching, in which the northern driveway may be blocked for up to eight (8) minutes, access to the site would continue to be available at the southern driveway. The nearest fire station (Cal Fire Green Springs Station) is located south of the site and southeast of the train tracks, which would further enable emergency access to the site in the event a train is crossing La Grange Road and/or the northern driveway. All on-site improvements will be designed with adequate width, turning radius, and grade to facilitate access by County's firefighting apparatus, and to provide alternative emergency ingress and egress. The site plan would be subject to plan review by the County's Fire Department to ensure proper access for fire and emergency response is provided and required fire suppression features are included. Therefore, the project's impact due to inadequate emergency access would be less than significant. As such, no hazardous design features would be part of the project's roadway improvements or site access.

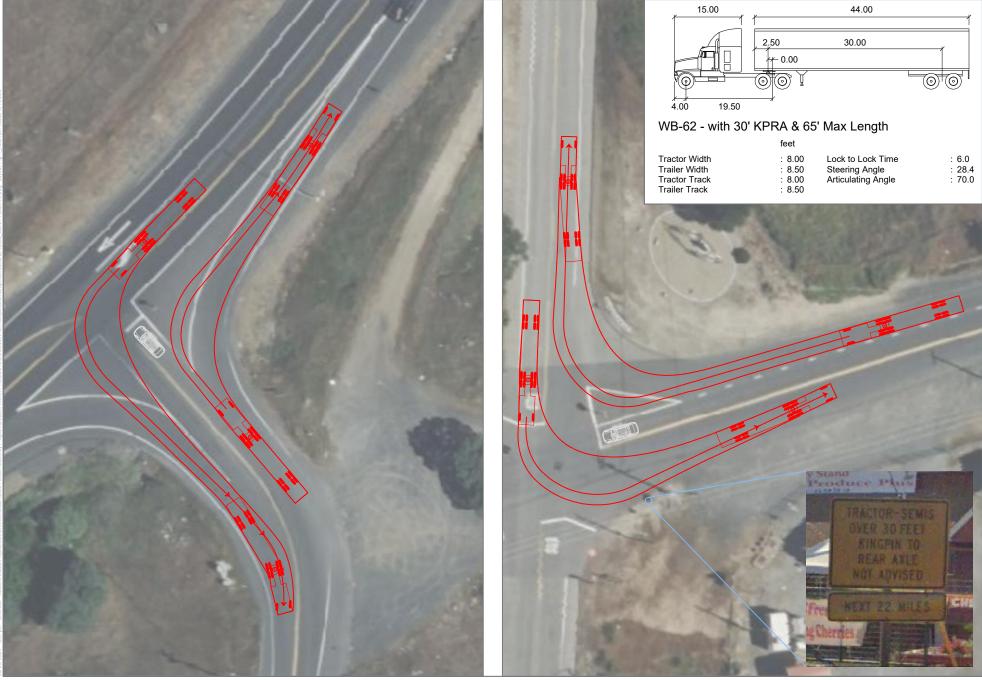




SOURCE: Bing Maps, AutoTURN Pro 2024

AutoTurn Analysis - WB 62

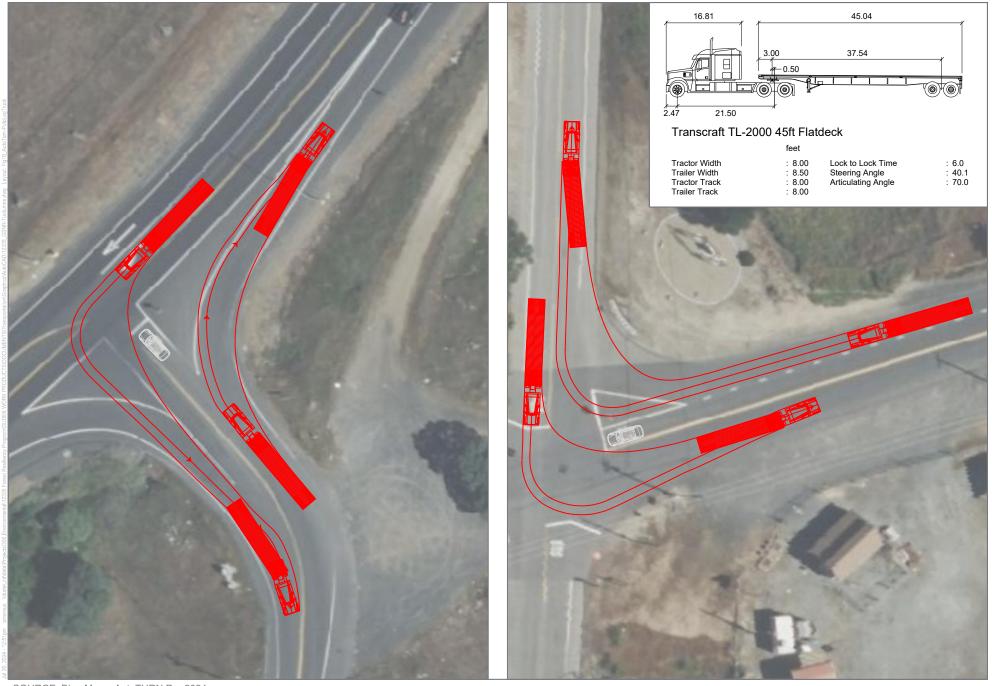
FIGURE 16



SOURCE: Bing Maps, AutoTURN Pro 2024



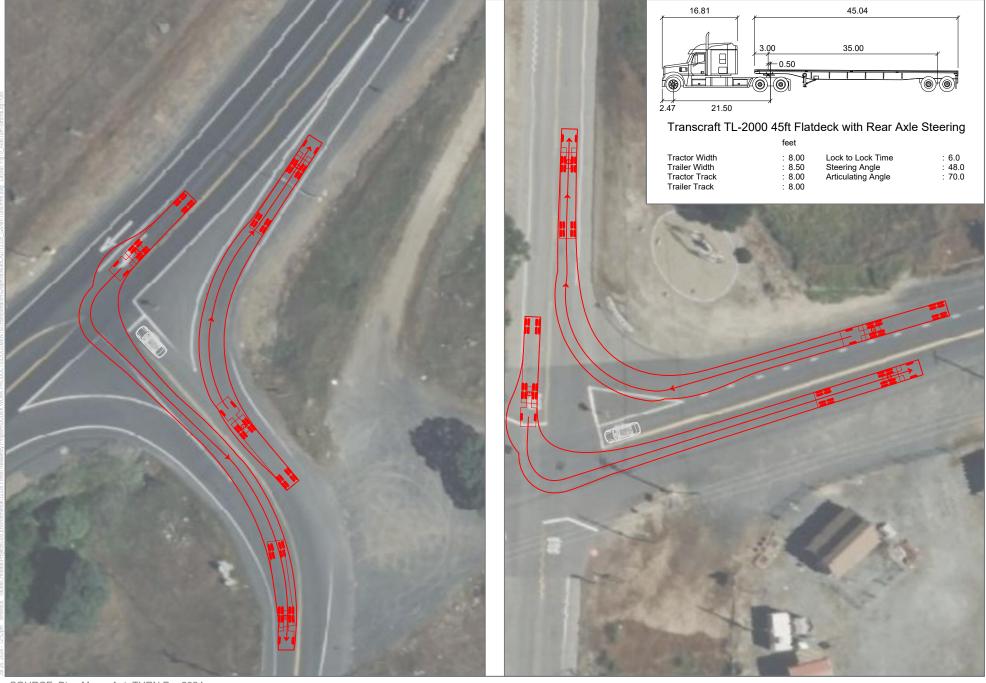
FIGURE 17



SOURCE: Bing Maps, AutoTURN Pro 2024



FIGURE 18



SOURCE: Bing Maps, AutoTURN Pro 2024



FIGURE 19

#### Off-site Queuing Analysis 7.1.2

A queuing analysis was performed for all study intersection to assess vehicle queues along the roadways, specifically at intersections with Caltrans facilities. The queuing analysis was performed for the Existing/Existing plus Project, and Opening Year (2025)/ Opening Year (2025) plus Project conditions, using Synchro/SimTraffic software, as summarized below. All SimTraffic queuing reports are provided in Appendix E.

#### **Existing Plus Project Conditions**

As shown in Table 9, Peak-Hour Queuing Summary for Existing plus Project Conditions, all intersection turning movements are anticipated to operate within available stacking distances and/or would not impede flow along major movements during the peak hours based on the 95th percentile peak hour traffic flows for the Existing plus Project traffic conditions. As such, there are no turning movements to and/or from any Caltrans facilities that are anticipated to experience queuing and/or safety issues during the weekday AM or weekday PM peak hours under Existing plus Project traffic conditions.

### Opening Year (2025) Plus Project Conditions

As shown in Table 10, Peak-Hour Queuing Summary for Opening Year (2025) plus Project Conditions, all intersection turning movements are anticipated to operate within available stacking distances and/or would not impede flow along major movements during the peak hours based on the 95th percentile peak hour traffic flows for the Opening Year (2025) plus Project traffic conditions. As such, there are no turning movements to and/or from any Caltrans facilities that are anticipated to experience queuing and/or safety issues during the weekday AM or weekday PM peak hours under Opening Year (2025) plus Project traffic conditions.

**Table 9. Peak-Hour Queuing Summary for Existing Plus Project Conditions** 

			Available Stacking Distance (Feet)	Existing (2	023)			Existing plus Project			
				95th Perce	Exceeds Stacking Distance?1		95th Percentile Queue (Feet)		Exceeds Stacking Distance?1		
No.	Intersection	Movement		AM Peak Hour	PM Peak Hour	AM	PM	AM Peak Hour	PM Peak Hour	AM	PM
1	SR-120 - SR-108/La	WBL	500	47	36	No	No	50	42	No	No
	Grange Road - CR J59	WBR	200	43	47	No	No	45	43	No	No
		NBR	130	0	49	No	No	0	18	No	No
		SBL	475	52	0	No	No	62	56	No	No
2	Site Access Employee Dwy/La Grange Road - CR J59	EBLT	500	0	0	No	No	17	15	No	No
		SBLR	50	0	0	No	No	32	0	No	No
3	Site Access Truck Dwy/La Grange Road - CR J59	EBL	300	5	8	No	No	18	19	No	No
		SBLR	150	21	0	No	No	42	36	No	No
4	La Grange Road - CR	EBLT	1,200	38	47	No	No	40	47	No	No
	J59/Yosemite	WBLT	1,000	42	38	No	No	43	41	No	No
	Boulevard - SR-132	NBLT	270	43	43	No	No	43	44	No	No
		NBR	25	35	29	Yes <sup>2</sup>	Yes <sup>2</sup>	36	29	Yes <sup>2</sup>	Yes <sup>2</sup>
		SBLT	220	45	46	No	No	44	45	No	No
		SBR	25	41	46	Yes <sup>2</sup>	Yes <sup>2</sup>	40	46	Yes <sup>2</sup>	Yes <sup>2</sup>
5	Red Hill	WBLT	180	0	6	No	No	0	12	No	No
	Road/Montezuma	NBL	215	18	20	No	No	17	16	No	No
	Road - SR-49 - SR-120	NBR	50	21	17	No	No	21	13	No	No

Source: Appendix E

 $\textbf{Notes:} \ \textbf{XBL} = [DirectionBound] \\ \textbf{Ieft:} \ \textbf{XBR} = [DirectionBound] \\ \textbf{Ieft:} \ \textbf{XBLT} = [DirectionBound] \\ \textbf{Ieft:} \\ \textbf{XBLT} = [DirectionBound] \\ \textbf{XBLT} = [DirectionB$ 



Stacking distance would be exceeded if the required stacking distance is greater than the stacking distance provided.

<sup>&</sup>lt;sup>2</sup> Queue extends past available pocket length for movement (measured as a 25-foot defacto right turn lane) but only extends approximately one vehicle length into the through (or left) turning lane.

Table 10. Peak-Hour Queuing Summary for Opening Year (2025) Plus Project Conditions

			Available Stacking	Opening Y	ear (2025)			Opening Year (2025) plus Project			
				95th Perce	Exceeds Stacking Distance?1		95th Percentile Queue (Feet)		Exceeds Stacking Distance?1		
No.	Intersection	Movement	Distance (Feet)	AM Peak Hour	PM Peak Hour	AM	PM	AM Peak Hour	PM Peak Hour	AM	PM
1	SR-120 - SR-108/La	WBL	500	53	56	No	No	99	46	No	No
	Grange Road - CR J59	WBR	200	49	45	No	No	50	45	No	No
		NBR	130	0	0	No	No	0	11	No	No
		SBL	475	62	64	No	No	65	71	No	No
2	Site Access Employee Dwy/La Grange Road - CR J59	EBLT	500	0	0	No	No	22	13	No	No
		SBLR	50	0	0	No	No	35	0	No	No
3	Site Access Truck Dwy/La Grange Road - CR J59	EBL	300	7	10	No	No	24	19	No	No
		SBLR	150	20	0	No	No	42	39	No	No
4	La Grange Road - CR	EBLT	1,200	39	48	No	No	40	50	No	No
	J59/Yosemite	WBLT	1,000	45	42	No	No	48	40	No	No
	Boulevard - SR-132	NBLT	270	45	42	No	No	41	42	No	No
		NBR	25	34	27	Yes <sup>2</sup>	Yes <sup>2</sup>	36	31	Yes <sup>2</sup>	Yes <sup>2</sup>
		SBLT	220	48	53	No	No	46	54	No	No
		SBR	25	43	52	Yes <sup>2</sup>	Yes <sup>2</sup>	44	51	Yes <sup>2</sup>	Yes <sup>2</sup>
5	Red Hill	WBLT	180	0	4	No	No	0	12	No	No
	Road/Montezuma	NBL	215	18	18	No	No	21	14	No	No
	Road - SR-49 - SR-120	NBR	50	22	17	No	No	21	15	No	No

Source: Appendix E

Notes: XBL = [DirectionBound]left; XBR = [DirectionBound]right; XBT = [DirectionBound]through; XBLTR = [DirectionBound]left-through-right; XBLT = [DirectionBound]left-through



Stacking distance would be exceeded if the required stacking distance is greater than the stacking distance provided.

<sup>&</sup>lt;sup>2</sup> Queue extends past available pocket length for movement (measured as a 25-foot defacto right turn lane) but only extends approximately one vehicle length into the through (or left) turning lane.



# 8 Vehicle Miles Traveled Analysis

On September 27, 2013, Senate Bill (SB) 743 was signed into law, which creates a process to change the way that transportation impacts are analyzed under California Environmental Quality Act (CEQA). SB 743 required the Governor's Office of Planning and Research (OPR) to amend the CEQA Guidelines to provide an alternative to LOS for evaluating transportation impacts. Under these transportation guidelines, LOS, or vehicle delay, is no longer considered an environmental impact under CEQA. OPR recommended VMT as the most appropriate measure of project transportation impacts for land use projects and land use plans. The updates to the CEQA Guidelines required under SB 743 were approved on December 28, 2018.

The CEQA Guidelines state that "generally, vehicle miles traveled (VMT) is the most appropriate measure of transportation impacts" and define VMT as "the amount and distance of automobile travel attributable to a project." "Automobile" refers to on-road passenger vehicles, specifically cars and light trucks. Other relevant considerations may include the effects of a project on transit and non-motorized travel.

The OPR Technical Advisory on Evaluating Transportation Impacts in CEQA (December 2018) provides technical assistance and recommendations for the analysis of VMT. The methodology recommendations for the VMT analysis include a discussion on vehicle types. An excerpt from the OPR Technical Advisory regarding vehicle types is below:

"Vehicle Types. Proposed Section 15064.3, subdivision (a), states, "For the purposes of this section, 'vehicle miles traveled' refers to the amount and distance of automobile travel attributable to a project." Here, the term "automobile" refers to on-road passenger vehicles, specifically cars and light trucks. Heavy-duty truck VMT could be included for modeling convenience and ease of calculation (for example, where models or data provide combined auto and heavy truck VMT). For an apples-to-apples comparison, vehicle types considered should be consistent across project assessment, significance thresholds, and mitigation."

Per Section 21099 of the Public Resource Code, the selection of the VMT criteria for determining the significance of transportation impacts was intended to promote reductions of greenhouse gas emissions (GHG); to develop multimodal transportation networks; and to diversify land uses. As mentioned in OPR's Technical Advisory, there are various legislative mandates and state policies that establish quantitative GHG emission reduction targets. Pursuant to Senate Bill 375, the California Air Resources Board GHG emissions reduction targets for metropolitan planning organizations (MPOs) call for reductions in GHG emissions only from cars and light trucks. As such VMT impacts are analyzed based on the number of employee trips within the specified boundary area, and not logging/haul truck trips.<sup>5</sup>

## 8.1 Methodology

The County of Tuolumne adopted VMT thresholds and guidance per the Tuolumne County VMT Thresholds Resolution and Staff Report on August 4, 2020 (County of Tuolumne 2020). Per the Resolution, Tuolumne County

<sup>&</sup>lt;sup>5</sup> Impacts related to logging/haul truck trips are accounted for in the Draft Environmental Impact Report (DEIR) Chapter 3.7 – Greenhouse Gas Emissions.

provides the following screening guidance to determine if a project should be expected to cause a less-thansignificant impact:

- Residential, Office, or Industrial Employment Project Located within a Low VMT Area: Low-VMT areas defined by the TCTC VMT maps.
- Small Project: Less than 110 trips per day and consistent the General Plan.
- Local Serving Retail: Local-serving and 50,000 square feet or less.
- Local Serving Public Facility: Public K-12 schools, local parks, libraries, post offices, police stations, utility buildings, etc.
- Affordable Housing: 100% affordable housing located in identified communities.
- Mixed-Use Project: Each project land use type should be considered separately and compared against the appropriate screening criteria.
- Redevelopment Project: Projects that would generate less total VMT than the existing land use they are replacing.

If a project does not meet the above screening criteria, consistent with the County and OPR guidelines, along with CEQA Guidelines Section 15064.3(b), the following specific VMT metrics are recommended to complete a VMT impact assessment:

- Residential: A project's VMT is less than or equal to the subarea average VMT per capita under baseline conditions, and the project is consistent with the County/City General Plan and the RTP.
- Office/Industrial: A project's VMT is less than or equal to the subarea average VMT per employee under baseline conditions, and the project is consistent with the County/City General Plan and the RTP.
- **Retail/Non-Office Commercial:** No net increase in total regional VMT.
- Hotel/Campground: Consistent with General Plan and less than or equal to subarea baseline average VMT per room/site.
- **Mixed-Use:** Analyze each land sue individually per the relevant thresholds.
- Redevelopment: If the redevelopment of an existing site leads to a net overall decrease, or no change in VMT, the project impact would be less than significant. If the redevelopment of an existing site leads to a net overall increase in VMT, the project would be evaluated based on the relevant thresholds as if it were a new project.

As noted above, the project primarily functions as an employment project for the purposes of VMT. As such, HBW vehicular trips were selected for evaluation to estimate trips associated with work VMT and estimate an average HBW VMT per employee within the Lake Don Pedro Subarea (County of Tuolumne 2020). Within this subarea, the County of Tuolumne recommends 100.4 VMT per employee as a threshold for VMT impacts.

The project would be considered to have a significant impact if the project VMT per employee is greater than 16.19 per the SJCOG RTDM, and 12.27 per the CSTDM. Table 11 summarizes VMT per-employee thresholds from both models.



**Table 11. VMT Threshold Summary** 

	Tuolumne County RTDM <sup>1</sup>
	VMT per Employee
Subarea Average (Tuolumne County)	100.4

Source: County of Tuolumne 2020

Notes:

VMT = vehicle miles traveled; SJCOG = San Joaquin Council of Governments; RTDM = Regional Travel Demand Model; CSDTM = California State Transportation Demand Model.

### 8.2 VMT Analysis

The following screening criteria were analyzed per the August 4, 2020, Tuolumne County VMT Thresholds Resolution and Staff Report (County of Tuolumne 2020). Any one of the following criteria would need to be satisfied in order to screen-out of significant VMT impacts:

Residential, Office, or Industrial Employment Project Located within a Low VMT Area Screening: Development in a low VMT generating area as defined by the TCTC VMT maps, and that is consistent with consistent with the County General Plan and the RTP.

The baseline average office/industrial VMT per employee values within the Lake Don Pedro Subarea were reviewed per the County VMT Resolution to determine whether the proposed project would be in a low VMT-generating area. A map of the low-VMT areas, generated by comparing locations within each subarea to the overall County average VMT per employee, are provided in Attachment B of the County VMT Resolution. A summary of the Lake Don Pedro Subarea compared to the County's VMT per employee average is provided in Table 12 below. Consistent with the County's Office/Industrial VMT per Employee Subareas low-VMT Screening Map, the project site would not be located in a low VMT generating area; therefore, the project cannot be screened out from further VMT analysis using the low VMT area screening criterion.

Table 12. Summary of Project Area VMT

Base Year (2023)	VMT <sup>1</sup>
VMT Per Employee	
Subarea Average (Lake Don Pedro Subarea)	100.4
County Average	53.3
% Difference (Project Subarea - County)	+88.5%
Threshold	53.3

**Source:** County of Tuolumne 2020 **Notes:** VMT = vehicle miles traveled

 Small Project (Less than 110 daily trips and consistent with the General Plan): The proposed project would employee 51 workers per day at the Tuolumne Site Facility, generating approximately 102 daily trips.

Attachment A (Baseline Average VMT for Subareas) of the Tuolumne County SB 743 VMT Thresholds Study (County of Tuolumne 2020)

<sup>&</sup>lt;sup>1</sup> Attachment A (Baseline Average VMT for Subareas) of the Tuolumne County SB 743 VMT Thresholds Study (County of Tuolumne 2020) (Attachment B)

Therefore, the project would meet the criteria for projects generating less than 110 daily trips and <u>can be</u> screened-out from further VMT analysis under this criterion.

- Local serving retail less than 50,000 SF: The project is not a retail land use; therefore, it <u>cannot</u> screenedout from further VMT analysis under this criterion.
- Local Serving Public Facility: Projects which serve the local community (e.g., public K-12 schools, local parks, libraries, post offices, police stations, utility buildings, etc.) and have the potential to reduce VMT should not be required to complete a VMT assessment. The project would not be categorized as a local serving land use due to its nature as an pellet processing facility and <u>cannot be</u> screened-out from further VMT analysis under this criterion.
- Affordable Housing (100% of units): The proposed project does not include affordable housing units. Therefore, the project <u>cannot be</u> screened-out from further VMT analysis under this criterion.
- Mixed-Use Project: The proposed project would not be considered mixed-use. Therefore, the project <u>cannot</u> <u>be</u> screened-out from further VMT analysis under this criterion.
- **Redevelopment Project:** The proposed project would not be considered a redevelopment project. Therefore, the project <u>cannot be</u> screened-out from further VMT analysis under this criterion.

As this project meets the Small Project screening criteria, and the project is consistent with the General Plan land use designation of HI, the Tuolumne Site Facility would have a less than significant impact to VMT under CEQA and no further VMT analysis is required.



# 9 Summary

Based on the results of the LOS, site access, and VMT analysis presented in this TIS, the following summarizes the key findings of the analysis:

- Operation of the Tuolumne Facility would generate approximately 340 daily trips, 53 AM peak hour trips and 28 PM peak hour trips. After trip generation estimates were adjusted utilizing PCE factors, the project would generate the equivalent of approximately 816 daily trips, 83 AM peak hour trips, and 58 PM peak hour trips.
- The five study area intersections currently and are forecast to operate at LOS D or better under all analysis scenarios, which meets the County's traffic impact thresholds (Table 3 and Table 9).
- All study area roadway segments and representative haul routes would are forecast to operate at LOS D or better under all analysis scenarios, which meets the County's traffic impact thresholds (Tables 4-5 and Tables 7-8), with exception of the US-50 haul route, which is forecast to operate at LOS E under Opening Year (2025) with and without total daily project haul trucks. However, US-50 is located outside of Tuolumne County's jurisdiction.
- The proposed project meets the Small Project screening criteria and is consistent with the County's M-2 land use zoning. Therefore, the Tuolumne Site Facility would have a less than significant impact to VMT under CEQA.

## 10 References

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**Appendix A**Census Data and Raw Traffic Counts

#### Home Destination Report - Where Workers Live Who are Employed in the Selection Area - by Places (Cities, CDPs, etc.)

#### Total All Jobs

	Count	Share	
Total All Jobs	127	100.0%	
Jobs Counts by Places (Cities, CDPs, etc.) Where Workers Live - All Jobs			
Jobs Counts by Flaces (Cities, CDFs, etc.) Where Workers Live - All Jobs	202	20	
	Count	Share	
amestown CDP, CA	7	5.5%	16%
Pakdale city, CA	6	4.7%	14%
resno city, CA	5	3.9%	12%
ferced city, CA	5	3.9%	12%
twater city, CA	4	3.1%	9%
onora city, CA	4	3.1%	9%
ast Sonora CDP, CA	3	2.4%	7%
os Banos city, CA	3	2.4%	7%
Iono Vista CDP, CA	3	2.4%	7%
hoenix Lake CDP, CA	3	2.4%	7%
Il Other Locations	84	66.1%	43 100.00%

2020

2020

2020

2020

2020

EMPLOYEE_DISTRIBUTION				
East	47%	45%		
West	14%	15%		
South	40%	40%		
	100%	100%		

#### Distance/Direction Report - Work Census Block to Home Census Block

#### Job Counts in Home Blocks by Distance Only

	Count	Share
Total All Jobs	127	100.0%
Less than 10 miles	19	15.0%
10 to 24 miles	38	29.9%
25 to 50 miles	35	27.6%
Greater than 50 miles	35	27.6%

#### Job Counts in Home Blocks to the North of Work Blocks by Distance

	Count	Share
Total All Jobs	8	100.0%
Less than 10 miles	3	37.5%
10 to 24 miles	0	0.0%
25 to 50 miles	2	25.0%
Greater than 50 miles	3	37.5%

#### Job Counts in Home Blocks to the Northeast of Work Blocks by Distance

	Count	Share
All Jobs	35	100.0%
than 10 miles	13	37.1%
24 miles	22	62.9%
50 miles	0	0.0%
er than 50 miles	0	0.0%

#### Job Counts in Home Blocks to the East of Work Blocks by Distance

	Count	Share
Total All Jobs	6	100.0%
Less than 10 miles	1	16.7%
10 to 24 miles	2	33.3%
25 to 50 miles	0	0.0%
Greater than 50 miles	3	50.0%

#### Job Counts in Home Blocks to the Southeast of Work Blocks by Distance

	Count	Share
otal All Jobs	17	100.0%
ess than 10 miles	0	0.0%
0 to 24 miles	3	17.6%
5 to 50 miles	2	11.8%
Greater than 50 miles	12	70.6%

#### Job Counts in Home Blocks to the South of Work Blocks by Distance

	Count	Share
Total All Jobs	22	100.0%
Less than 10 miles	0	0.0%
10 to 24 miles	0	0.0%
25 to 50 miles	16	72.7%
Greater than 50 miles	6	27.3%

#### Job Counts in Home Blocks to the Southwest of Work Blocks by Distance

	2020	
	Count	Share
Total All Jobs	11	100.0%
Less than 10 miles	0	0.0%
10 to 24 miles	3	27.3%
25 to 50 miles	7	63.6%
Greater than 50 miles	1	9.1%

#### Job Counts in Home Blocks to the West of Work Blocks by Distance

Count	Share
15	100.0%
1	6.7%
7	46.7%
7	46.7%
0	0.0%

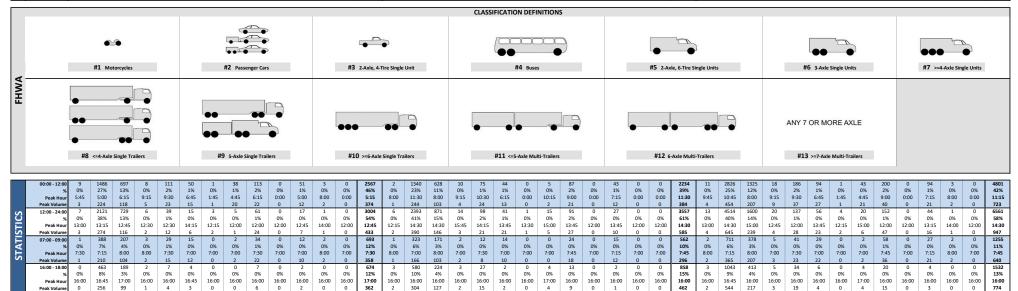
#### Job Counts in Home Blocks to the Northwest of Work Blocks by Distance

	20	020
	Count	Share
Total All Jobs	13	100.0%
Less than 10 miles	1	7.7%
10 to 24 miles	1	7.7%
25 to 50 miles	1	7.7%
Greater than 50 miles	10	76.9%

#### CLASSIFICATION SR 120/SR 108 W/O La Grange Rd/CR J59

Day: Tuesday City: Jamestown Date: 08/29/2023 Project #: CA23 090100 001

		00/25/																																					-	. ojece	C/125_0.	190100_00	-
	Time						E	ASTBOL	IND						Total						W	ESTBOU	ND						Total							TOTALS	;						Total
		#1	#2	#3	#4	#5	#6	#7	#8	#9	#10	#11	#12	#13		#1	#2	#3	#4	#5	#6	#7	#8	#9	#10	#11	#12	#13		#1	#2	#3	#4	#5	#6	#7	#8	#9	#10	#11	#12	#13	
	0:00	0	19	9	0	1	0	0	0	0	0	0	0	0	29	0	42	10	0	0	0	0	0	1	0	0	0	0	53	0	61	19	0	1	0	0	0	1	0	0	0	0	82
	1:00	0	16	3	0	0	1	0	0	1	0	0	0	0	21	0	33	5	0	0	0	0	0	0	0	0	0	0	38	0	49	8	0	0	1	0	0	1	0	0	0	0	59
	2:00	0	8	2	0	3	0	1	1	0	0	0	0	0	15	0	27	13	0	1	0	0	0	0	0	0	0	0	41	0	35	15	0	4	0	1	1	0	0	0	0	0	56
	3:00	0	21	6	0	1	1	0	0	1	0	0	0	0	30	0	37	13	0	3	0	0	0	4	0	0	0	0	57	0	58	19	0	4	1	0	0	5	0	0	0	0	87
	4:00	0	39	16	0	5	0	0	12	1	0	0	0	0	73	0	66	42	2	5	0	0	0	0	0	0	0	0	115	0	105	58	2	10	0	0	12	1	0	0	0	0	188
	5:00	1	224	77	0	15	9	0	18	9	0	12	0	0	365	0	78	53	0	1	0	0	1	3	0	2	0	0	138	1	302	130	0	16	9	0	19	12	0	14	0	0	503
_	6:00	3	184	114	0	9	9	0	2	21	0	1	0	0	343	0	144	68	2	4	12	0	1	16	0	5	0	0	252	3	328	182	2	13	21	0	3	37	0	6	0	0	595
€1	7:00	0	194	103	1	14	12	0	2	19	0	10	0	0	355	0	166	68	2	6	10	0	0	9	0	10	0	0	271	0	360	171	3	20	22	0	2	28	0	20	0	0	626
<b>&gt;</b>	8:00	1	194	104	2	15	3	0	0	15	0	2	2	0	338	1	157	103	0	6	4	0	0	15	0	5	0	0	291	2	351	207	2	21	7	0	0	30	0	7	2	0	629
9	9:00	1	191	87	3	18	4	0	1	19	0	11	0	0	335	0	171	81	3	9	2	0	0	21	0	8	0	0	295	1	362	168	6	27	6	0	1	40	0	19	0	0	630
9	10:00	2	174	94	2	19	7	0	2	12	0	5	0	0	317	1	200	85	1	17	7	0	1	13	0	6	0	0	331	3	374	179	3	36	14	0	3	25	0	11	0	0	648
₹I	11:00	1	222	82	0	11	4	0	0	15	0	10	1	0	346	0	219	87	0	23	9	0	2	5	0	7	0	0	352	1	441	169	0	34	13	0	2	20	0	17	1	0	698
m.	12:00	0	225	95	0	11	1	0	1	24	0	6	0	0	363	1	240	87	1	17	5	0	2	23	0	7	0	0	383	1	465	182	1	28	6	0	3	47	0	13	0	0	746
# I	13:00	3	263	107	2	10	3	2	0	9	0	7	0	0	406	1	199	99	2	13	11	0	2	25	0	7	0	0	359	4	462	206	4	23	14	2	2	34	0	14	0	0	765
$\equiv$ 1	14:00	1	231	78	1	1	3	0	1	7	0	0	1	0	324	0	335	120	2	16	17	1	1	20	0	9	0	0	521	1	566	198	3	17	20	1	2	27	0	9	1	0	845
	15:00	2	243	95	0	4	3	0	1	5	0	0	0	0	353	0	354	144	1	20	4	0	5	4	0	2	0	0	534	2	597	239	1	24	7	0	6	9	0	2	0	0	887
半	16:00	0	207	90	1	4	2	0	0	6	0	2	0	0	312	2	304	127	2	15	2	0	0	9	0	1	0	0	462	2	511	217	3	19	4	0	0	15	0	3	0	0	774
ನ I	17:00	0	256	99	1	3	2	0	0	1	0	0	0	0	362	1	276	97	1	12	0	0	4	4	0	1	0	0	396	1	532	196	2	15	2	0	4	5	0	1	0	0	758
ᆍ	18:00	0	220	48	0	2	0	0	0	2	0	0	0	0	272	0	171	57	3	0	0	0	0	2	0	0	0	0	233	0	391	105	3	2	0	0	0	4	0	0	0	0	505
	19:00	0	166	39	0	1	0	0	0	2	0	0	0	0	208	1	149	54	1	1	1	0	0	1	0	0	0	0	208	1	315	93	1	2	1	0	0	3	0	0	0	0	416
	20:00	1	116	32	0	0	1	0	1	0	0	0	0	0	151	0	130	33	0	0	1	0	0	2	0	0	0	0	166	1	246	65	0	0	2	0	1	2	0	0	0	0	317
	21:00	0	104	25	0	2	0	0	0	2	0	2	0	0	135	0	108	24	0	1	0	0	0	1	0	0	0	0	134	0	212	49	0	3	0	0	0	3	0	2	0	0	269
	22:00	0	50	12	0	1	0	1	0	1	0	0	0	0	65	0	80	20	0	3	0	0	0	0	0	0	0	0	103	0	130	32	0	4	0	1	0	1	0	0	0	0	168
	23:00	0	40	9	1	0	0	0	1	2	0	0	0	0	53	0	47	9	1	0	0	0	1	0	0	0	0	0	58	0	87	18	2	0	0	0	2	2	0	0	0	0	111
	Totals	16	3,607	1,426	14	150	65	4	43	174	0	68	4	0	5,571	8	3,733	1,499	24	173	85	1	20	178	0	70	0	0	5,791	24	7,340	2,925	38	323	150	5	63	352	0	138	4	0	11,362
	% of Totals	0%	65%	26%	0%	3%	1%	0%	1%	3%		1%	0%		100%	0%	64%	26%	0%	3%	1%	0%	0%	3%		1%			100%	0%	65%	26%	0%	3%	1%	0%	1%	3%		1%	0%		100%



16:00 16:00 16:00 17:00 16:00 16:00 16:00

16:00 16:00 0 0

16:00

16:00

16:00 0

16:00 16:00

16:00

16:00 16:45 17:00 16:00 16:00

#### CLASSIFICATION SR 120/SR 108 W/O La Grange Rd/CR J59

Day: Tuesday
Date: 08/29/2023

							E/	ASTBOU	ND												W	ESTBOU	ND													TOTALS							
	Time	#1	#2	#3	#4	#5	#6	#7		#9	#10	#11	#12	#13	Total	#1	#2	#3	#4	#5	#6			#9	#10	#11	#12	#13	Total	#1	#2	#3	#4	#5				#9	#10	#11	#12 #	#13	Total
	0:00	0	3	2	0	0	0	0	0	0	0	0	0	0	5	0	10	2	0	0	0	0	0	0	0	0	0	0	12	0	13	4	0	0	0	0	0	0	0	0			17
	0:15	0	7	3	0	0	0	0	0	0	0	0	0	0	10	0	12	3	0	0	0	0	0	0	0	0	0	0	15	0	19	6	0	0	0	0	0	0	0	0	0	0	25
	0:30	0	4	0	0	0	0	0	0	0	0	0	0	0	4	0	10	1	0	0	0	0	0	1	0	0	0	0	12	0	14	1	0	0	0	0	0	1	0	0	0	0	16
	0:45	0	5	4	0	1	0	0	0	0	0	0	0	0	10	0	10	4	0	0	0	0	0	0	0	0	0	0	14	0	15	8	0	1	0	0	0	0	0	0	0	0	24
	1:00	0	7	1	0	0	0	0	0	0	0	0	0	0	8	0	7	2	0	0	0	0	0	0	0	0	0	0	9	0	14	3	0	0	0	0	0	0	0	0	0	0	17
	1:15	0	0	1	0	0	0	0	0	0	0	0	0	0	1	0	8	2	0	0	0	0	0	0	0	0	0	0	10	0	8	3	0	0	0	0	0	0	0	0	0	0	11
	1:30	0	6	0	0	0	0	0	0	0	0	0	0	0	6	0	10	1	0	0	0	0	0	0	0	0	0	0	11	0	16	1	0	0	0	0	0	0	0	0	0	0	17
	1:45	0	3	1	0	0	1	0	0	1	0	0	0	0	6	0	8	0	0	0	0	0	0	0	0	0	0	0	8	0	11	1	0	0	1	0	0	1	0	0	0	0	14
	2:00	0	3	0	0	0	0	0	0	0	0	0	0	0	3	0	6	3	0	0	0	0	0	0	0	0	0	0	9	0	9	3	0	0	0	0	0	0	0	0	0	0	12
	2:15	0	2	2	0	2	0	0	0	0	0	0	0	0	6	0	9	1	0	1	0	0	0	0	0	0	0	0	11	0	11	3	0	3	0	0	0	0	0	0	0	0	17
	2:30	0	2	0	0	1	0	1	0	0	0	0	0	0	4	0	7	4	0	0	0	0	0	0	0	0	0	0	11	0	9	4	0	1	0	1	0	0	0	0	0 /	0	15
	2:45	0	1	0	0	0	0	0	1	0	0	0	0	0	2	0	5	5	0	0	0	0	0	0	0	0	0	0	10	0	6	5	0	0	0	0	1	0	0	0		0	12
	3:00	0	3	2	0	1	0	0	0	0	0	0	0	0	6	0	9	1	0	0	0	0	0	0	0	0	0	0	10	0	12	3	0	1	0	0	0	0	0	0		0	16
	3:15	0	3	0	0	0	1	0	0	1	0	0	0	0	5	0	10	6	0	2	0	0	0	1	0	0	0	0	19	0	13	6	0	2	1	0	0	2	0	0		0	24
T	3:30	0	5	2	0	0	0	0	0	0	0	0	0	0	7	0	9	4	0	0	0	0	0	1	0	0	0	0	14	0	14	6	0	0	0	0	0	1	0	0	0		21
	3:45	0	10	2	0	0	0	0	0	0	0	0	0	0	12	0	9	2	0	1	0	0	0	2	0	0	0	0	14	0	19	4	0	1	0	0	0	2	0	0	0		26
_	4:00	0	2	2	0	0	0	0	4	0	0	0	0	0	8	0	11	7	1	2	0	0	0	0	0	0	0	0	21	0	13	9	1	2	0	0	4	0	0	0	-		29
5	4:15	0	5	4	0	2	0	0	2	0	0	0	0	0	13	0	16		0	0	0	0	0	0	0	0	0	0	23	0	21	11	0	2	0	0	2	0	0	0	0	0	36
Š	4:30	0	12	5	0	2	0	0	1	1	0	0	0	0	21	0	14	8	0	2	0	0	0	0	0	0	0	0	24	0	26	13	0	4	0	0	1 1	1	0	0	0	0	45
2	4:45	0	20	5	0	1	0	0	5	0	0	0	0	0	31	0	25	20	1	1	0	0	0	0	0	0	0	0	47	0	45	25	1	2	0	0	5	0	0	0			78 86
$\exists$	5:00 5:15	0	36	7	0	2	3	0	4	0	0	4	0	0	56 88	0	18	12 16	0	0	0	0	0	0	0	0	0	0	30	0	54	19 33	0	2	3	0	4	0	0	4		0	118
⋖		0	53	17	0	,	1	0	5	3	0	2	0	0		0	14		0	0	0	0	0	0	0	0	0	0	30	0	67		0		1	0	5	3	0	2	0		
#	5:30 5:45	0	74	31 22	0	0	2	0	3	4	0	2	0	0	126 95	0	17	15 10	0	0	0	0	0	2	0	2	0	0	35	0	91	46 32	0	0	3	0	3	6	0	4	0		161 138
BREAKD	6:00	1	61 32	23	0	-	3	0	0	2	0	0	0	0	65	0	29 26	13	0	0	1	0	0	4	0	4	0	0	43 48	0	90 58	32	0	5	Δ	0	3	6	0	4	0		113
1111	6:15	١	49	22	0	1	1	0	0	7	0	0	0	0	80	0	41	14	1	2	-	0	0	6	0	1	0	0	71	0	90	36	1	4	-	0	0	13	0	1	0 '		151
- 5	6:30	2	46	32	0	2	2	0	0	1	0	1	0	0	89	0	32	21	0	0	1	0	0	4	0	0	0	0	61	2	78	53	0	2	6	0	0	8	0	1	0 '		150
۱ź	6:45	1	57	37	0	1	3	0	2	8	0	0	0	0	109	0	45	20	1	1	2	0	1	2	0	0	0	ő	72	1	102	57	1	2	5	0	3	10	0	0	0		181
5-MINUTE	7:00	0	42	27	1	3	6	0	0	3	0	1	0	0	83	0	48	12	1	1	2	0	0	2	0	1	0	0	67	0	90	39	2	4	8	0	0	5	0	2			150
7	7:15	0	44	21	0	2	3	0	0	5	0	4	0	0	79	0	46	28	0	0	3	0	0	0	0	2	0	ō	79	0	90	49	0	2	6	0	0	5	0	6	0		158
5	7:30	ō	54	24	0	6	3	0	0	6	0	3	0	0	96	0	28	6	0	4	5	0	0	1	0	3	0	ō	47	0	82	30	0	10	8	0	0	7	0	6	0		143
``	7:45	0	54	31	0	3	0	0	2	5	0	2	0	0	97	0	44	22	1	1	0	0	0	6	0	4	0	0	78	0	98	53	1	4	0	0	2	11	0	6	0		175
	8:00	0	58	20	0	3	1	0	0	2	0	0	0	0	84	0	37	31	0	0	1	0	0	2	0	3	0	0	74	0	95	51	0	3	2	0	0	4	0	3	0		158
	8:15	1	41	24	0	3	1	0	0	9	0	1	1	0	81	0	39	26	0	3	0	0	0	4	0	2	0	0	74	1	80	50	0	6	1	0	0	13	0	3	1	0	155
	8:30	0	47	27	1	4	0	0	0	2	0	1	0	0	82	0	44	18	0	2	0	0	0	6	0	0	0	0	70	0	91	45	1	6	0	0	0	8	0	1	0	0	152
	8:45	0	48	33	1	5	1	0	0	2	0	0	1	0	91	1	37	28	0	1	3	0	0	3	0	0	0	0	73	1	85	61	1	6	4	0	0	5	0	0	1		164
	9:00	0	41	19	0	3	0	0	0	6	0	6	0	0	75	0	37	16	0	3	0	0	0	4	0	1	0	0	61	0	78	35	0	6	0	0	0	10	0	7	0		136
T	9:15	0	55	22	0	5	0	0	0	4	0	2	0	0	88	0	41	28	0	0	0	0	0	5	0	2	0	0	76	0	96	50	0	5	0	0	0	9	0	4	0		164
	9:30	0	47	20	0	5	4	0	1	5	0	2	0	0	84	0	50	15	1	4	2	0	0	5	0	4	0	0	81	0	97	35	1	9	6	0	1	10	0	6	0		165
	9:45	1	48	26	3	5	0	0	0	4	0	1	0	0	88	0	43	22	2	2	0	0	0	7	0	1	0	0	77	1	91	48	5	7	0	0	0	11	0	2	0		165
	10:00	2	44	21	2	7	4	0	1	3	0	1	0	0	85	0	47	16	1	3	1	0	0	3	0	5	0	0	76	2	91	37	3	10	5	0	1	6	0	6	0		161
	10:15	0	45	34	0	6	3	0	1	4	0	0	0	0	93	0	56	31	0	5	2	0	1	4	0	1	0	0	100	0	101	65	0	11	5	0	2	8	0	1	0		193
	10:30	0	33	24	0	3	0	0	0	2	0	2	0	0	64	1	41	17	0	4	2	0	0	4	0	0	0	0	69	1	74	41	0	7	2	0	0	6	0	2	0		133
	10:45	0	52	15	0	3	0	0	0	3	0	2	0	0	75	0	56	21	0	5	2	0	0	2	0	0	0	0	86	0	108	36	0	8	2	0	0	5	0	2			161
T	11:00	0	50	16	0	3	2	0	0	2	0	2	0	0	75	0	52	19	0	4	2	0	1	1	0	1	0	0	80	0	102	35	0	7	4	0	1	3	0	3			155
	11:15	1	64	21	0	3	1	0	0	7	0	3	0	0	100	0	49	28	0	11	2	0	0	2	0	1	0	0	93	1	113	49	0	14	3	0	0	9	0	4			193
	11:30	0	58	22	0	3	0	0	0	4	0	5	1	0	93	0	73	24	0	4	3	0	0	1	0	2	0	0	107	0	131	46	0	7	3	0	0	5	0	7			200
	11:45	0	50	23	0	2	1	0	0	2	0	0	0	0	78	0	45	16	0	4	2	0	1	1	0	3	0	0	72	0	95	39	0	6	3	0	1	3	0	3	0	0	150

#### CLASSIFICATION SR 120/SR 108 W/O La Grange Rd/CR J59

Day: Tuesday
Date: 08/29/2023

							E	ASTBOU	IND												W	ESTBOU	ND						F-1-1							TOTALS							
	Time	#1	#2	#3	#4	#5	#6	#7	#8	#9	#10	#11	#12	#13	Total	#1	#2	#3	#4	#5	#6	#7	#8	#9	#10	#11	#12	#13	Total	#1	#2	#3	#4	#5	#6	#7	#8	#9	#10	#11	#12	#13	Total
	12:00	0	44	22	0	0	0	0	0	7	0	2	0	0	75	0	59	27	1	5	2	0	0	8	0	3	0	0	105	0	103	49	1	5	2	0	0	15	0	5		0	180
	12:15	Ō	56	19	0	4	o	0	1	6	0	1	0	0	87	0	67	21	0	5	0	0	0	6	0	1	0	0	100	ó	123	40	0	9	0	ó	1	12	0	2	0	ō	187
	12:30	0	56	23	0	4	0	0	0	3	0	2	0	0	88	1	62	24	0	5	3	0	1	1	0	2	0	0	99	1	118	47	0	9	3	0	1	4	0	4	0	0	187
	12:45	ا ا	69	31	0	3	1	0	0	8	0	1	0	0	113	0	52	15	0	2	0	0	1	8	0	1	0	0	79	0	121	46	0	5	1	0	1	16	0	2	0	ō I	192
	13:00	1	54	20	1	0	0	2	0	2	0	0	0	0	80	1	46	14	1	0	0	0	1	9	0	3	0	0	75	2	100	34	2	0	0	2	1	11	0	3	0	ŏ	155
	13:15	ا أ	78	22	1	5	2	0	0	5	0	2	0	0	115	0	52	33	0	6	3	0	0	3	0	2	0	0	99	0	130	55	1	11	5	0	0	8	0	4	0	ŏ	214
	13:30	1	72	43	0	2	1	0	0	2	0	4	0	0	125	0	33	23	1	4	1	0	0	3	0	1	0	0	66	1	105	66	1	6	2	0	0	5	0	5	0	0	191
	13:45	1	59	22	0	3	ō	0	0	0	0	1	0	0	86	0	68	29	0	3	7	0	1	10	0	1	0	0	119	1	127	51	0	6	7	0	1	10	0	2	0	ŏ	205
	14:00	1	65	28	1	0	0	0	0	1	0	n	0	0	96	0	69	22	0	3	3	0	0	9	0	5	0	0	111	1	134	50	1	3	3	0	0	10	0	5	0	0	207
	14:15	ءَ ا	55	15	0	1	2	0	0	0	0	0	0	0	73	0	81	18	0	4	4	1	0	4	0	2	0	0	114	0	136	33	0	-	-	1	0	4	0	2	0	ŭΙ	187
	14:30	l ő	50	16	0	0	0	0	1	2	0	0	0	0	70	0	88	33	1	-	7	, n	0	4	0	2	0	0	140	0	138	49	1	5	7	0	1	7	0	2	0	ŭΙ	210
	14:45	١	61	19	0	0	1	0	1	3	0	0	1	0	85	0	97	47	1	1	,	0	1	2	0	0	0	0	156	0	158	66	1	4	,	0	1	6	0	0	1	ůΙ	241
	15:00	-	78	32		0	3	0	0		0	0		0	117	0	88	33	1	-4	3	0	-		0	0	0		132	1	166	65		10	-	0		2	0	0	0	0	249
		1 1	66	20	0	2	3	0	0	1	0	0	0	0	90	0		22	0	0	1	0	1	1	0	2	0	0	157	1		65	0	10	4	0	1	2	0	2	0	١	249
	15:15 15:30	0			0	2	0	0	0	2	0	0	0	0		-	117	33	0	3	1	0	1	0	0	2	0	0		0	183	53	0	5	1	0	1	2	0	2	0	١	
		1	53	21	0	0	0	0	1	0	0	0	0	0	76	0	80	32	0	ь	1	0	1	2	0	0	0	0	122	1	133	53	0	6	1	0	2	2	0	0	0	١	198
	15:45	0	46	22	0	0	0	0	0	2	0	U	U	U	70	0	69	46	1	3	1	0	2	1	U	U	U	0	123	0	115	68	1	3	1	U	2	3	0	0	U	U	193
	16:00	0	66	28	1	0	1	0	0	2	0	1	Ü	0	99	1	70	27	1	4	0	0	0	5	0	1	U	0	109	1	136	55	2	4	1	0	0	/	0	2	U	U I	208
-	16:15	0	44	22	0	2	0	0	0	2	0	0	0	0	70	0	76	34	0	_ ′	0	0	0	1	0	0	0	0	118	0	120	56	0	9	0	0	0	3	0	0	0	0	188
5	16:30	0	34	17	0	1	0	0	0	2	0	0	0	0	54	1	75	33	1	2	2	0	0	2	0	0	0	0	116	1	109	50	1	3	2	0	0	4	0	0	0	0	170
≥.	16:45	0	63	23	0	1	1	0	0	0	0	1	0	0	89	0	83	33	0	2	0	0	0	1	0	0	0	0	119	0	146	56	0	3	1	0	0	1	0	1	0	0	208
8	17:00	0	60	26	0	0	0	0	0	1	0	0	0	0	87	0	56	25	1	2	0	0	1	2	0	0	0	0	87	0	116	51	1	2	0	0	1	3	0	0	0	0	174
91	17:15	0	72	24	1	1	1	0	0	0	0	0	0	0	99	0	85	27	0	2	0	0	2	1	0	0	0	0	117	0	157	51	1	3	1	0	2	1	0	0	0	0	216
ā	17:30	0	61	18	0	1	1	0	0	0	0	0	0	0	81	1	64	24	0	5	0	0	0	0	0	1	0	0	95	1	125	42	0	6	1	0	0	0	0	1	0	0	176
	17:45	0	63	31	0	1	0	0	0	0	0	0	0	0	95	0	71	21	0	3	0	0	1	1	0	0	0	0	97	0	134	52	0	4	0	0	1	1	0	0	0	0	192
BREAKI	18:00	0	59	14	0	0	0	0	0	2	0	0	0	0	75	0	54	16	1	0	0	0	0	0	0	0	0	0	71	0	113	30	1	0	0	0	0	2	0	0	0	0	146
111	18:15	0	71	12	0	2	0	0	0	0	0	0	0	0	85	0	46	14	1	0	0	0	0	1	0	0	0	0	62	0	117	26	1	2	0	0	0	1	0	0	0	0	147
F	18:30	0	49	13	0	0	0	0	0	0	0	0	0	0	62	0	30	18	0	0	0	0	0	0	0	0	0	0	48	0	79	31	0	0	0	0	0	0	0	0	0	0	110
2 .	18:45	0	41	9	0	0	0	0	0	0	0	0	0	0	50	0	41	9	1	0	0	0	0	1	0	0	0	0	52	0	82	18	1	0	0	0	0	1	0	0	0	0	102
S-MINUTE	19:00	0	57	10	0	0	0	0	0	1	0	0	0	0	68	0	42	16	0	0	0	0	0	0	0	0	0	0	58	0	99	26	0	0	0	0	0	1	0	0	0	0	126
51	19:15	0	41	6	0	0	0	0	0	0	0	0	0	0	47	0	41	14	0	1	0	0	0	0	0	0	0	0	56	0	82	20	0	1	0	0	0	0	0	0	0	0	103
ΞI	19:30	0	38	17	0	1	0	0	0	0	0	0	0	0	56	1	34	15	0	0	1	0	0	0	0	0	0	0	51	1	72	32	0	1	1	0	0	0	0	0	0	0	107
띕	19:45	0	30	6	0	0	0	0	0	1	0	0	0	0	37	0	32	9	1	0	0	0	0	1	0	0	0	0	43	0	62	15	1	0	0	0	0	2	0	0	0	0	80
	20:00	1	30	10	0	0	1	0	1	0	0	0	0	0	43	0	39	9	0	0	0	0	0	0	0	0	0	0	48	1	69	19	0	0	1	0	1	0	0	0	0	0	91
	20:15	0	33	7	0	0	0	0	0	0	0	0	0	0	40	0	29	10	0	0	0	0	0	2	0	0	0	0	41	0	62	17	0	0	0	0	0	2	0	0	0	0	81
<u> </u>	20:30	0	32	8	0	0	0	0	0	0	0	0	0	0	40	0	36	10	0	0	0	0	0	0	0	0	0	0	46	0	68	18	0	0	0	0	0	0	0	0	0	。 l	86
<u> </u>	20:45	0	21	7	ō	0	ō	0	0	0	0	0	0	ō	28	0	26	4	0	0	1	0	0	0	0	0	0	0	31	0	47	11	0	0	1	0	0	0	0	0	0	ō	59
	21:00	0	29	6	0	0	0	0	0	1	0	0	0	0	36	0	24	8	0	0	0	0	0	1	0	0	0	0	33	0	53	14	0	0	0	0	0	2	0	0	0	0	69
	21:15	0	34	9	0	1	0	0	0	0	0	2	0	0	46	0	29	4	0	0	0	0	0	0	0	0	0	0	33	0	63	13	0	1	0	0	0	0	0	2	0	0	79
	21:30	0	20	7	0	0	0	0	0	1	0	0	0	0	28	0	20	4	0	0	0	0	0	0	0	0	0	0	24	0	40	11	0	0	0	0	0	1	0	0	0	0	52
	21:45	lő	21	3	0	1	0	0	0	0	0	0	0	0	25	0	35	8	0	1	0	0	0	0	0	0	0	0	44	0	56	11	0	2	0	0	0	0	0	0	0	0	69
	22:00	0	7	4	0	0	0	0	0	1	0	0	0	0	12	0	28	4	0	1	0	0	0	0	0	0	0	0	33	0	35	8	0	1	0	0	0	1	0	0	0	0	45
	22:15	0	13	4	0	0	0	0	0	0	0	0	0	0	17	0	21	9	0	1	0	0	0	0	0	0	0	0	31	0	34	13	0	1	0	0	0	0	0	0	0	0	48
	22:30	ا ا	18	2	0	1	0	0	0	0	0	0	0	0	21	0	19	5	0	1	0	0	0	0	0	0	0	0	25	0	37	7	0	2	0	0	0	0	0	0	0	ō	46
	22:45	ا ا	12	2	0	0	0	1	0	0	0	0	0	0	15	0	12	2	0	0	0	0	0	0	0	0	0	0	14	0	24	4	0	0	0	1	0	0	0	0	0	ō	29
	23:00	0	11	3	1	0	0	0	0	1	0	0	0	0	16	0	7	2	0	0	0	0	0	0	0	0	0	0	9	0	18	5	1	0	0	0	0	1	0	0	0	0	25
	23:15	0	16	2	0	0	0	0	0	0	0	0	0	0	18	0	13	4	1	0	0	0	1	0	0	0	0	0	19	0	29	6	1	0	0	0	1	0	0	0	0	0	37
	23:30	0	6	3	0	0	0	0	1	0	0	0	0	0	10	0	16	2	0	0	0	0	0	0	0	0	0	0	18	0	22	5	0	0	0	0	1	0	0	0	0	0	28
	23:45	0	7	1	0	0	0	0	0	1	0	0	0	0	9	0	11	1	0	0	0	0	0	0	0	0	0	0	12	0	18	2	0	0	0	0	0	1	0	0	0	ů l	21
	Totals	16	3 607	1,426	14	150	65	4	43	174	0	68	4	0	5,571	8	3,733	1,499	24	173	85	1 -	20	178	0	70	0	0	5,791	24	7,340	2,925	38	323	150	5	63	352	0	138	4	0	11,362
	% of Totals								1%			1%			100%							0%	0%			1%	Ů	•	100%		65%									1%			100%

#### **VOLUME**

### SR 120/SR 108 W/O La Grange Rd/CR J59

 Day: Tuesday
 City: Jamestown

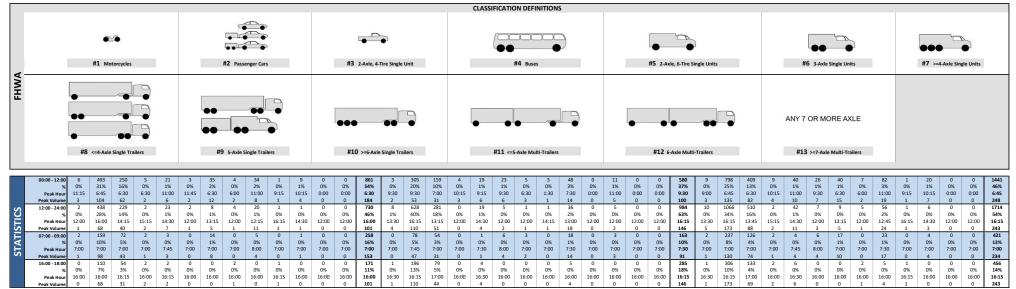
 Date: 08/29/2023
 Project #: CA23\_090100\_001

		DAI	LY TOT	ALS			NB	SB	EB	WB	Total			DAIL	Y TO	TALS		
				0			0	0	5,571	5,791	11,362							
				1	5-Minut		/al							Hour	ly Int	ervals		
TIME	NB	SB	EB	WB	TOTAL	TIME	NB	SB	EB	WB	TOTAL	TIMI		NB	SB	EB	WB	TOTAL
0:00			5	12	17	12:00			75	105	180	11	01:00			29	53	82
0:15			10	15	25	12:15			87	100	187		02:00			21	38	59
0:30 0:45			4 10	12 14	16 24	12:30 12:45			88 113	99 79	187 192		03:00 04:00			15 30	41 57	56 87
1:00			8	9	17	13:00			80	75	155	11	05:00			73	115	188
1:15			1	10	11	13:15			115	99	214		06:00			365	138	503
1:30			6	11	17	13:30			125	66	191	11	07:00			343	252	595
1:45			6	8	14	13:45			86	119	205	07:00	08:00			355	271	626
2:00			3	9	12	14:00			96	111	207	08:00	09:00			338	291	629
2:15			6	11	17	14:15			73	114	187	09:00	10:00			335	295	630
2:30			4	11	15	14:30			70	140	210		11:00			317	331	648
2:45			2	10	12	14:45			85	156	241		12:00			346	352	698
3:00			6	10	16	15:00			117	132	249		13:00			363	383	746
3:15			5 7	19	24	15:15			90	157	247	11	14:00			406	359	765
3:30 3:45			/ 12	14 14	21 26	15:30 15:45			76 70	122 123	198 193	11	15:00 16:00			324 353	521 534	845 887
4:00			8	21	29	16:00			99	109	208	11	17:00			312	462	774
4:15			13	23	36	16:15			70	118	188	11	18:00			362	396	758
4:30			21	24	45	16:30			54	116	170		19:00			272	233	505
4:45			31	47	78	16:45			89	119	208		20:00			208	208	416
5:00			56	30	86	17:00			87	87	174		21:00			151	166	317
5:15			88	30	118	17:15			99	117	216	21:00	22:00			135	134	269
5:30			126	35	161	17:30			81	95	176		23:00			65	103	168
5:45			95	43	138	17:45			95	97	192	23:00	00:00			53	58	111
6:00			65	48	113	18:00			75	71	146				ATIST	ics		
6:15			80	71	151	18:15			85	62	147			NB	SB	EB	WB	TOTAL
6:30			89	61	150	18:30			62	48	110	Peak	Period	00:00	to	12:00		
6:45			109	72	181	18:45			50	52	102	V	/olume			2567	2234	4801
7:00			83	67	150	19:00			68	58	126		k Hour			5:15	10:45	10:45
7:15			79	79	158	19:15			47	56	103	Peak V				374	366	709
7:30			96 97	47	143 175	19:30			56 37	51 43	107	Peak Hour	Factor			0.742	0.855	0.886
7:45 8:00			84	78 74	158	19:45 20:00			43	48	80 91	Poak	Period	12:00	to	00:00		
8:15			81	74	155	20:15			40	41	81		/olume	12.00	to	3004	3557	6561
8:30			82	70	152	20:30			40	46	86		k Hour			12:45	14:30	14:30
8:45			91	73	164	20:45			28	31	59		/olume			433	585	947
9:00			75	61	136	21:00			36	33	69	Peak Hour	Factor			0.866	0.932	0.951
9:15			88	76	164	21:15			46	33	79							
9:30			84	81	165	21:30			28	24	52	Peak	Period	07:00	to	09:00		
9:45			88	77	165	21:45			25	44	69		/olume			693	562	1255
10:00			85	76	161	22:00			12	33	45		k Hour			7:30	7:45	7:45
10:15			93	100	193	22:15			17	31	48	Peak V				358	296	640
10:30			64 75	69 86	133	22:30			21	25	46	Peak Hour	Factor			0.923	0.949	0.914
10:45 11:00			75 75	86 80	161 155	22:45 23:00			15 16	14 9	29 25	Dook	Period	16:00	to	18:00		
11:15			100	93	193	23:15			18	19	37		/olume	10.00	ı	674	858	1532
11:30			93	107	200	23:30			10	18	28		k Hour			17:00	16:00	16:00
11:45			78	72	150	23:45			9	12	21		/olume			362	462	774
TOTALS	0	0	2567	2234	4801	TOTALS	0	0	3004	3557	6561	Peak Hour				0.914	0.971	0.930
SPLIT %	0%	0%	53%	47%	42%	SPLIT %	0%	0%	46%	54%	58%							
600 —																		
											×	×						
500 —											/							
400 —													$\overline{}$					
300 —					-	*			<del></del>		1							
300 -				/		* <del>*</del>	X							1				
200 —				/											_	*		
				$\longrightarrow$												78	*	

### CLASSIFICATION La Grange Rd/CR J59 S/O SR 120/SR 108

Day: Tuesday
Date: 08/29/2023
Project #: CA23\_090100\_002

		00, 23, 2																																								30100_0	
Time							N	ORTHBO	UND						Total						so	UTHBOU	IND						Total							TOTALS	;						Total
		#1	#2	#3	#4	#5	#6	#7	#8	#9	#10	#11	#12	#13		#1	#2	#3	#4	#5	#6	#7	#8	#9	#10	#11	#12	#13		#1	#2	#3	#4	#5	#6	#7	#8	#9	#10	#11	#12	#13	
0:00	0	0	5	2	0	0	0	0	1	0	0	0	0	0	8	0	9	0	0	2	0	0	0	0	0	0	0	0	11	0	14	2	0	2	0	0	1	0	0	0	0	0	19
1:00		0	2	2	0	0	0	0	0	0	0	0	0	0	4	0	7	0	0	1	0	0	0	0	0	0	0	0	8	0	9	2	0	1	0	0	0	0	0	0	0	0	12
2:00	0	0	8	3	0	1	0	0	0	0	0	0	0	0	12	0	6	3	0	1	1	0	1	1	0	0	0	0	13	0	14	6	0	2	1	0	1	1	0	0	0	0	25
3:00	0	0	4	5	0	2	0	0	0	1	0	0	0	0	12	0	9	2	0	0	0	0	0	0	0	0	0	0	11	0	13	7	0	2	0	0	0	1	0	0	0	0	23
4:00		0	21	9	0	0	0	0	0	0	0	0	0	0	30	0	12	5	0	0	0	0	0	2	0	0	0	0	19	0	33	14	0	0	0	0	0	2	0	0	0	0	49
5:00	0	0	80	17	0	0	0	1	1	2	0	0	0	0	101	0	28	10	0	3	3	0	0	2	0	0	0	0	46	0	108	27	0	3	3	1	1	4	0	0	0	0	147
6:00		0	76	54	1	4	1	6	2	7	0	1	0	0	152	0	18	19	0	0	3	1	0	3	0	0	0	0	44	0	94	73	1	4	4	7	2	10	0	1	0	0	196
7:00	0	1	98	43	1	0	0	8	0	1	0	1	0	0	153	0	32	31	0	0	2	2	0	11	0	3	0	0	81	1	130	74	1	0	2	10	0	12	0	4	0	0	234
8:00	0	1	61	29	1	3	0	6	0	4	0	0	0	0	105	0	46	23	0	1	4	1	0	7	0	0	0	0	82	1	107	52	1	4	4	7	0	11	0	0	0	0	187
9:00	0	2	57	38	1	1	1	8	0	4	0	2	0	0	114	1	47	24	0	5	5	0	1	4	0	2	0	0	89	3	104	62	1	6	6	8	1	8	0	4	0	0	203
10:0	00	0	45	26	1	4	0	5	0	7	1	3	0	0	92	2	49	23	2	2	4	0	0	7	0	1	0	0	90	2	94	49	3	6	4	5	0	14	1	4	0	0	182
11:0	00	2	36	22	0	6	1	1	0	8	0	2	0	0	78	0	42	19	2	4	1	1	1	11	0	5	0	0	86	2	78	41	2	10	2	2	1	19	0	7	0	0	164
12:0	00	1	44	34	0	4	1	2	1	9	0	0	0	0	96	0	42	26	0	1	2	1	0	5	0	2	0	0	79	1	86	60	0	5	3	3	1	14	0	2	0	0	175
13:0	00	0	49	15	0	4	1	3	0	5	0	0	0	0	77	2	52	47	0	2	2	0	0	18	0	0	0	0	123	2	101	62	0	6	3	3	0	23	0	0	0	0	200
14:0	00	1	43	39	0	6	0	2	0	4	0	0	0	0	95	2	71	38	0	1	0	0	0	1	0	0	0	0	113	3	114	77	0	7	0	2	0	5	0	0	0	0	208
15:0	00	0	48	36	0	4	0	0	0	1	0	1	0	0	90	2	78	36	0	4	1	0	1	5	0	2	0	0	129	2	126	72	0	8	1	0	1	6	0	3	0	0	219
16:0	00	0	68	29	2	1	0	0	1	0	0	0	0	0	101	0	99	35	0	1	0	0	0	4	0	0	0	0	139	0	167	64	2	2	0	0	1	4	0	0	0	0	240
17:0	00	0	42	25	0	1	0	0	1	0	1	0	0	0	70	1	97	44	0	3	0	0	0	1	0	0	0	0	146	1	139	69	0	4	0	0	1	1	1	0	0	0	216
18:0	00	0	46	21	0	2	0	0	0	0	0	0	0	0	69	1	66	27	0	2	0	0	0	0	0	1	0	0	97	1	112	48	0	4	0	0	0	0	0	1	0	0	166
19:0	00	0	23	12	0	0	0	0	0	0	0	0	0	0	35	0	47	12	0	2	0	0	0	0	0	0	0	0	61	0	70	24	0	2	0	0	0	0	0	0	0	0	96
20:0	00	0	26	10	0	0	0	0	0	0	0	0	0	0	36	0	32	9	0	1	0	0	0	0	0	0	0	0	42	0	58	19	0	1	0	0	0	0	0	0	0	0	78
21:0	00	0	28	7	0	0	0	0	0	0	0	0	0	0	35	0	17	4	0	1	0	0	0	0	0	0	0	0	22	0	45	11	0	1	0	0	0	0	0	0	0	0	57
22:0	00	0	11	0	0	1	0	0	1	0	0	0	0	0	13	0	18	0	0	0	0	0	0	2	0	0	0	0	20	0	29	0	0	1	0	0	1	2	0	0	0	0	33
23:0	00	0	10	1	0	0	0	1	0	1	0	0	0	0	13	0	9	3	0	1	0	0	0	0	0	0	0	0	13	0	19	4	0	1	0	1	0	1	0	0	0	0	26
Total	als	8	931	479	7	44	5	43	8	54	2	10	0	0	1,591	11	933	440	4	38	28	6	4	84	0	16	0	0	1,564	19	1,864	919	11	82	33	49	12	138	2	26	0	0	3,155
% of	of Totals	1%	59%	30%	0%	3%	0%	3%	1%	3%	0%	1%			100%	1%	60%	28%	0%	2%	2%	0%	0%	5%		1%			100%	1%	59%	29%	0%	3%	1%	2%	0%	4%	0%	1%			100%



#### CLASSIFICATION La Grange Rd/CR J59 S/O SR 120/SR 108

Day: Tuesday
Date: 08/29/2023

							NC	ORTHBOU	LIND												SO	UTHBOUN	ND.													TOTALS							
	Time	#1	#2	#3	#4	#5	#6		#8	#9	#10	#11	#12	#13	Total	#1	#2	#3	#4	#5	#6	#7	#8	#9	#10	#11	#12	#13	Total	#1	#2	#3	#4	#5	#6	#7		#9	#10	#11	#12 #	#13	Total
	0:00	0	1	0	0	0	0	0	0	0	0	0	0	0	1	0	3	0	0	2	0	0	0	0	0	0	_	0	5	0	4	0	0	2	0	0	0	0	0	0		0	6
	0:15	١،	0	1	0	0	0	0	0	0	0	0	0	0	1	0	1	0	0	0	0	0	0	0	0	0	0	ň	1	0	1	1	0	0	0	0	0	0	0	0	0	ň	2
	0:30	١	3	ō	0	0	0	0	0	0	0	0	0	0	3	0	3	0	0	o	0	0	0	0	0	0	0	ŏ	3	0	6	ō	0	0	0	0	0	0	o	0	-	ŏ I	6
		0	3		-	-	0			-							3		0					-			-			-	2		-	0	-	0		0		- 1		١	
	0:45	0	1	1	0	0	0	0	1	0	0	0	0	0	3	0	2	0	0	0	0	0	0	0	0	0	0	0	2	0	3	1	0	0	0	0	1	0	0	0	0	0	5
	1:00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0	0	0	0	0	0	0	0	0	0	0	2	0	2	0	0	0	0	0	0	0	0	0		0	2
	1:15	0	2	1	0	0	0	0	0	0	0	0	0	0	3	0	1	0	0	0	0	0	0	0	0	0	0	0	1	0	3	1	0	0	0	0	0	0	0	0	0	0	4
	1:30	0	0	1	0	0	0	0	0	0	0	0	0	0	1	0	2	0	0	0	0	0	0	0	0	0	0	0	2	0	2	1	0	0	0	0	0	0	0	0	0	0	3
	1:45	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0	0	1	0	0	0	0	0	0	0	0	3	0	2	0	0	1	0	0	0	0	0	0	0	0	3
	2:00	0	1	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	1
	2:15	0	3	1	0	0	0	0	0	0	0	0	0	0	4	0	4	2	0	1	0	0	1	0	0	0	0	0	8	0	7	3	0	1	0	0	1	0	0	0	0	0	12
	2:30	0	4	1	0	1	0	0	0	0	0	0	0	0	6	0	1	1	0	0	1	0	0	0	0	0	0	0	3	0	5	2	0	1	1	0	0	0	0	0	0	0	9
	2:45	0	0	1	0	0	0	0	0	0	0	0	0	0	1	0	1	0	0	0	0	0	0	1	0	0	0	0	2	0	1	1	0	0	0	0	0	1	0	0	0	0	3
	3:00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	0	0	0	0	0	0	0	0	0	0	2	0	1	1	0	0	0	0	0	0	0	0	0	0	2
	3:15	0	0	2	0	1	0	0	0	1	0	0	0	0	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0	1	0	0	0	1	0	0	0	0	4
	3:30	0	0	2	0	0	0	0	0	0	0	0	0	0	2	0	4	0	0	0	0	0	0	0	0	0	0	0	4	0	4	2	0	0	0	0	0	0	0	0	0	0	6
	3:45	Ö	4	1	0	1	0	0	0	0	0	0	0	0	6	0	4	1	0	0	o	0	0	0	0	0	0	0	5	0	8	2	0	1	0	0	0	0	0	0	0	0	11
	4:00	0	5	1	0	0	0	0	0	0	0	0	0	0	6	0	3	1	0	0	0	0	0	1	0	0	0	0	5	0	8	2	0	0	0	0	0	1	0	0	0	0	11
7	4:15	١	4	2	0	0	0	0	0	0	0	0	0	0	6	0	4	3	0	o	0	0	0	1	0	0	0	0	.	0		5	0	0	0	0	0	1	0	0	0	ă I	14
5	4:30	0	3	2	0	0	0	0	0	0	0	0	0	0	5	0	2	1	0	0	0	0	0	0	0	0	0	0	3	0	5	3	0	0	0	0	0	1	0	0	-	ů l	8
$\geq$	4:45		9	4	0	0	0	_	0	-	0		- 1	0	13	- 1	3	0	0	0	-		0	0	0	0	0	0	- 1	-			0	0	0	0	0	0	0	0	0	١	16
BREAKDOW		0		1	0	0	0	0	0	0	0	0	0	0		0	3	2		0	0	0	0		0		0	0	3	0	12	3	0	0	0	0	0	0	0	0		0	25
$\Box \Box \Box$	5:00	0	15		_	_	_	0	_	_	0		0	-	16		5	2	0	1	1	0	-	0	0	0	-	0	9		20	-	-	1	1	0	-	0	0	0	-	0	
⋖	5:15	0	23	3	0	0	0	0	0	0	U	0	0	0	26	0	8	4	U	2	1	0	0	2	0	0	0	0	17	0	31	7	0	2	1	0	0	2	0	0	0	0	43
# 1	5:30	0	21	4	0	0	0	0	1	1	0	0	0	0	27	0	4	2	0	0	1	0	0	0	0	0	0	0	7	0	25	6	0	0	1	0	1	1	0	0	0	0	34
齒	5:45	0	21	9	0	0	0	1	0	1	0	0	0	0	32	0	11	2	0	0	0	0	0	0	0	0	0	0	13	0	32	11	0	0	0	1	0	1	0	0	0	0	45
	6:00	0	18	10	0	2	0	0	0	2	0	0	0	0	32	0	5	8	0	0	1	0	0	0	0	0	0	0	14	0	23	18	0	2	1	0	0	2	0	0	0	0	46
$\mathbf{E}$	6:15	0	12	8	0	2	1	0	0	3	0	0	0	0	26	0	6	6	0	0	0	0	0	0	0	0	0	0	12	0	18	14	0	2	1	0	0	3	0	0	0	0	38
=	6:30	0	22	20	0	0	0	4	0	0	0	0	0	0	46	0	0	2	0	0	2	1	0	2	0	0	0	0	7	0	22	22	0	0	2	5	0	2	0	0	0	0	53
S-MINUTE	6:45	0	24	16	1	0	0	2	2	2	0	1	0	0	48	0	7	3	0	0	0	0	0	1	0	0	0	0	11	0	31	19	1	0	0	2	2	3	0	1	0	0	59
⋝.	7:00	0	25	8	0	0	0	3	0	0	0	0	0	0	36	0	10	10	0	0	0	0	0	1	0	0	0	0	21	0	35	18	0	0	0	3	0	1	0	0	0	0	57
J.J.	7:15	0	31	18	1	0	0	3	0	1	0	0	0	0	54	0	9	5	0	0	0	2	0	1	0	1	0	0	18	0	40	23	1	0	0	5	0	2	0	1	0	0	72
띕	7:30	1	24	13	0	0	0	1	0	0	0	0	0	0	39	0	5	8	0	0	1	0	0	6	0	1	0	0	21	1	29	21	0	0	1	1	0	6	0	1	0	0	60
	7:45	0	18	4	0	0	0	1	0	0	0	1	0	0	24	0	8	8	0	0	1	0	0	3	0	1	0	0	21	0	26	12	0	0	1	1	0	3	0	2	0	0	45
	8:00	0	21	7	0	0	0	1	0	2	0	0	0	0	31	0	8	8	0	0	0	0	0	2	0	0	0	0	18	0	29	15	0	0	0	1	0	4	0	0	0	0	49
	8:15	0	12	7	0	0	0	4	0	1	0	0	0	0	24	0	19	7	0	1	1	0	0	3	0	0	0	0	31	0	31	14	0	1	1	4	0	4	0	0	0	0	55
	8:30	l o	12	7	0	3	0	1	0	0	0	0	0	0	23	0	12	1	0	0	1	1	0	2	0	0	0	0	17	0	24	8	0	3	1	2	0	2	0	0	0	o	40
	8:45	1	16	8	1	0	0	0	0	1	0	0	0	0	27	0	7	7	0	0	2	0	0	0	0	0	0	0	16	1	23	15	1	0	2	0	0	1	0	0	0	0	43
	9:00	0	14	13	0	0	0	0	0	0	0	1	0	0	28	0	12	5	0	0	0	0	0	2	0	1	0	0	20	0	26	18	0	0	0	0	0	2	0	2	0	0	48
	9:15	1	17	11	1	1	0	2	0	3	0	0	0	0	36	0	10	3	0	2	1	0	0	0	0	0	0	0	16	1	27	14	1	3	1	2	0	3	0	0	0	0	52
	9:30	Ō	8	4	ō	ō	o	1	0	1	n	0	0	0	14	0	15	7	0	2	2	0	1	2	0	0	0	ň	29	0	23	11	ō	2	2	1	1	3	0	0	0	ň	43
	9:45	1	18	10	0	0	1	5	0	0	0	1	0	0	36	1	10	9	0	1	2	0	0	0	0	1	0	0	24	2	28	19	0	1	2	-	0	0	0	2	0	0	60
	10:00	0	11	3	0	1	0	1	0	3	1	0	0	0	20	0	12	5	0	1	0	0	0	1	0	0	0	0	19	0	23	8	0	2	0	1	0	4	1	0	0	ň	39
		١	17	7	0	-	0	2	0	0	0	2	0	0	30	1	16	7	1	0	2		0	1	0	0	0	0	28	1	33	14	1	2	2	,	0	"	1	2	0	ĭ	58
	10:15	١		10	1	0	0	2	0	4	0		- 1	0	26	0	10		1	1		0	0	1	0	0	0	٥	17	0		13	1	2	2	2	U	1	0	2	0	, I	43
	10:30 10:45	0	11 6	6	0	1	0	0 2	0	0	0	0	0	0	26 16	1	12	3 8	0	0	1	0	0	2	0	1	0	0	26	1	20	14	0	1	1	0	0	٥	0	0	0	١	43
		0	_	_		1	0		0	1	0	1	0	0					1	1			0	3	0	1	-	0		0	18		1	1	1	2	0	3		2		-	
	11:00	0	12	4	0	1	0	0	0	1	0	1	0	0	19	0	11	4	1	1	0	0	0	2	0	2	0	0	21	- 1	23	8	1	2	0	0	0	3	0	3	-	0	40
	11:15	1	9	9	0	0	0	1	0	2	0	0	0	0	22	0	10	ь	U	3	0	1	1	4	0	1	0	0	26	1	19	15	0	3	0	2	1	6	0	1	0	0	48
	11:30	0	9	3	0	3	0	0	0	2	0	0	0	0	17	0	12	/	0	0	1	0	0	1	0	0	0	0	21	0	21	10	0	3	1	0	0	3	0	0	0		38
	11:45	1	6	6	0	2	1	0	0	3	0	1	0	0	20	0	9	2	1	0	0	0	0	4	0	2	0	0	18	1	15	8	1	2	1	0	0	7	0	3	0	0	38

#### CLASSIFICATION La Grange Rd/CR J59 S/O SR 120/SR 108

Day: Tuesday
Date: 08/29/2023

	T:						NO	ORTHBOL	JND					Total						SOL	JTHBOU	IND						Total							TOTALS							Total
	Time	#1	#2	#3	#4	#5	#6	#7	#8	#9	#10	#11	#12 #	.3 Total	#1	#2	#3	#4	#5	#6	#7	#8	#9	#10	#11	#12	#13	Total	#1	#2	#3	#4	#5	#6	#7	#8	#9	#10	#11	#12	#13	lotai
	12:00	1	6	9	0	0	0	0	0	0	0	0	0	16	0	11	9	0	0	1	0	0	3	0	2	0	0	26	1	17	18	0	0	1	0	0	3	0	2	0	0	42
	12:15	0	13	7	0	1	0	1	1	3	0	0	0	26	0	13	8	0	1	1	1	0	0	0	0	0	0	24	0	26	15	0	2	1	2	1	3	0	0	0	0	50
	12:30	0	14	14	0	3	1	0	0	2	0	0	0	34	0	9	3	0	0	0	0	0	1	0	0	0	0	13	0	23	17	0	3	1	0	0	3	0	0	0	0	47
	12:45	0	11	4	0	0	0	1	0	4	0	0	0		0	9	6	0	0	0	0	0	1	0	0	0	0	16	0	20	10	0	0	0	1	0	5	0	0	0	0	36
	13:00	0	11	0	0	0	0	0	0	2	0	0	0	13	0	6	9	0	0	1	0	0	4	0	0	0	0	20	0	17	9	0	0	1	0	0	6	0	0	0	0	33
	13:15	0	13	4	0	0	0	1	0	2	0	0	0		0	12	12	0	0	0	0	0	4	0	0	0	ō	28	0	25	16	0	0	0	1	0	6	0	0	0	0	48
	13:30	0	16	6	0	4	0	1	0	0	0	0	0	27	1	14	7	0	1	1	0	0	7	0	0	0	ō	31	1	30	13	0	5	1	1	0	7	0	0	0	ō	58
	13:45	ő	9	5	0	0	1	1	0	1	0	n	0		1	20	19	0	1	0	n	0	3	0	0	0	ő	44	1	29	24	0	1	1	1	0	1	0	0	0	ňI	61
	14:00	0	17	12	0	2	0	2	0	1	0	0	0		0	24	13	0	0	0	0	0	0	0	0	0	0	37	0	41	25	0	2	0	2	0	1	0	0	0	ň	71
	14:15	ľ	6	10	0	0	0	0	0	1	0	0	0		2		0	0	0	0	0	0	0	0	0	0	0	21	3	17	18	0	0	0		0	1	0	0	0	ı, I	39
	14:15	1	12	12	0	0	0	0	0	1	0	0	0	27		11 21	0	0	1	0	0	0	1	0	0	0	0	32	0	33	21	0	2	0	0	0	1	0	0	0	, I	59
		0		5	0	2	0	0	0	1	-	0	-		0		9	_	1	- 1	0	0	1	0	-	0	- 1	23	-			0	3	0	0	0	2	0	0	0	١٠	
	14:45	0	8	_	0	2	0	0	0	1	0	0	0	_	0	15	8	0	0	0	0	0	0	0	0	0	0		0	23	13	0	2	0	0	0	1	0	0		0	39
	15:00	0	16	13	0	1	0	0	0	0	0	0	0		1	19	8	0	2	1	0	1	1	0	1	0	0	34	1	35	21	0	3	1	0	1	1	0	1	0	0	64
	15:15	0	11	8	0	2	0	0	0	0	0	1	0	22	0	17	12	0	1	0	Ü	0	2	0	1	0	0	33	0	28	20	0	3	0	0	0	2	0	2	0	0	55
	15:30	0	9	7	0	0	0	0	0	1	0	0	0	17	1	21	7	0	0	0	0	0	1	0	0	0	0	30	1	30	14	0	0	0	0	0	2	0	0	0	0	47
	15:45	0	12	8	0	1	0	0	0	0	0	0	0	21	0	21	9	0	1	0	0	0	1	0	0	0	0	32	0	33	17	0	2	0	0	0	1	0	0	0	0	53
	16:00	0	15	7	2	0	0	0	1	0	0	0	0	25	0	13	11	0	0	0	0	0	1	0	0	0	0	25	0	28	18	2	0	0	0	1	1	0	0	0	0	50
_	16:15	0	21	9	0	0	0	0	0	0	0	0	0	30	0	33	9	0	0	0	0	0	2	0	0	0	0	44	0	54	18	0	0	0	0	0	2	0	0	0	0	74
- 5	16:30	0	13	6	0	0	0	0	0	0	0	0	0	19	0	29	10	0	1	0	0	0	1	0	0	0	0	41	0	42	16	0	1	0	0	0	1	0	0	0	0	60
≥ .	16:45	0	19	7	0	1	0	0	0	0	0	0	0	27	0	24	5	0	0	0	0	0	0	0	0	0	0	29	0	43	12	0	1	0	0	0	0	0	0	0	0	56
O	17:00	0	10	9	0	1	0	0	0	0	1	0	0	21	0	24	7	0	1	0	0	0	0	0	0	0	0	32	0	34	16	0	2	0	0	0	0	1	0	0	0	53
е	17:15	0	11	6	0	0	0	0	1	0	0	0	0	18	1	28	10	0	2	0	0	0	0	0	0	0	0	41	1	39	16	0	2	0	0	1	0	0	0	0	0	59
BREAKDOWN	17:30	0	10	6	0	0	0	0	0	0	0	0	0	16	0	29	11	0	0	0	0	0	1	0	0	0	0	41	0	39	17	0	0	0	0	0	1	0	0	0	0	57
ш	17:45	0	11	4	0	0	0	0	0	0	0	0	0	15	0	16	16	0	0	0	0	0	0	0	0	0	0	32	0	27	20	0	0	0	0	0	0	0	0	0	0	47
<b>~</b>	18:00	0	14	6	0	0	0	0	0	0	0	0	0	20	1	12	12	0	1	0	0	0	0	0	1	0	0	27	1	26	18	0	1	0	0	0	0	0	1	0	0	47
	18:15	0	13	5	0	1	0	0	0	0	0	0	0	19	0	24	8	0	0	0	0	0	0	0	0	0	0	32	0	37	13	0	1	0	0	0	0	0	0	0	0 I	51
ᄪ	18:30	0	11	6	0	1	0	0	0	0	0	0	0	18	0	16	0	0	0	0	0	0	0	0	0	0	0	16	0	27	6	0	1	0	0	0	0	0	0	0	o I	34
כׂ	18:45	0	8	4	0	0	0	0	0	0	0	0	0	12	0	14	7	0	1	0	0	0	0	0	0	0	0	22	0	22	11	0	1	0	0	0	0	0	0	0	o I	34
S-MINUTE	19:00	0	7	5	0	0	0	0	0	0	0	0	0		0	9	5	0	1	0	0	0	0	0	0	0	0	15	0	16	10	0	1	0	0	0	0	0	0	0	0	27
_ ₹	19:15	0	3	2	0	0	0	0	0	0	0	0	0	5	0	10	0	0	0	0	0	0	0	0	0	0	0	10	0	13	2	0	0	0	0	0	0	0	0	0	0	15
4	19:30	0	11	3	0	0	0	0	0	0	0	0	0	14	0	8	7	0	1	0	0	0	0	0	0	0	ō	16	0	19	10	0	1	0	0	0	0	0	0	0	0	30
5	19:45	0	2	2	0	0	0	0	0	0	0	0	0	Ι 4	0	20	0	0	0	0	0	0	0	0	0	0	ō	20	0	22	2	0	0	0	0	0	0	0	0	0	ō	24
``	20:00	0	5	5	0	0	0	0	0	0	0	0	0	10	0	6	0	0	0	0	0	0	0	0	0	0	0	6	0	11	5	0	0	0	0	0	0	0	0	0	o l	16
	20:15	ň	5	3	0	0	0	0	0	0	0	0	0	10 R	l ŏ	10	4	0	1	0	0	0	0	0	0	0	ő	15	n	15	7	0	1	0	n	0	0	0	0	0	ň	23
	20:30	۱		2	0	0	0	0	0	0	0	0	0	10	0	9	1	0	0	0	0	0	0	0	0	0	0	10	0	17	3	0	0	0	٥	0	0	0	0	0	ŭΙ	20
	20:45	١	9	0	0	0	0	0	0	0	0	0	0		0	7	1	0	0	0	0	0	0	0	0	0	0	11	0	15	4	0	0	0	0	0	0	0	0	0	ňΙ	19
	21:00	0	7	3	0	0	0	0	0	0	0	0	0		0	2	2	0	1	0	0	0	0	0	0	0	0	5	0	0	-	0	1	0	0	0	0	0	0	0	0	15
		0	\ '\	2	0	0	0	0	0	0	0	0			1 0	2	1	0	1	0	0	0	0	0	0	0	0	3	0	9	2	0	0	0	0	0	0	0	0	0	ı, I	
	21:15 21:30	0	,		0	0	0	0	0	0	0	0	0	9	0	2	1	0	0	0	0	0	0	0	0	0	-	3	0	42	3	0	0	0	0	0	0	0	0	0	١٠	12
		0	0	2	0	0	0	0	0	0	0	0	0		0	,	0	0	0		0	0	0	0	0	0	0		0	13	2	0	0	0	0	0	0	0	0	-	١٠	15
	21:45	0	8	0	0	0	-	0	0	0	0	0	0		0	6	1	-	0	0	-	0	0	0	-	0	0	7	0	14	1	-	0	-	0	0	0	-	0	0	0	15
	22:00	0	2	0	0	1	0	0	1	0	0	0	0		0	6	0	0	0	0	0	0	1	0	0	0	0	' '	0	0	0	0	1	0	0	1	1	0	0	0	٠ I	11
	22:15	0	2	0	0	0	0	0	0	0	0	0	0	2	0	4	0	0	0	0	0	0	0	0	0	0	0	4	0	6	0	0	0	0	0	0	0	0	0	0	0	6
	22:30	0	3	0	U	U	U	0	U	U	U	U	0	3	0	4	U	0	U	0	U	U	0	U	U	0	0	4	0	/	U	0	U	U	0	U	0	U	0	0	o	7
	22:45	0	4	0	0	0	0	0	0	0	0	0	0		0	4	0	0	0	0	0	0	1	0	0	0	0	5	0	8	0	0	0	0	0	0	1	0	0	0	0	9
	23:00	0	0	1	0	0	0	1	0	1	0	0	0	3	0	4	1	0	0	0	Ü	0	0	0	0	0	0	5	0	4	2	0	0	0	1	0	1	0	0	0	0	8
	23:15	0	4	0	0	0	0	0	0	0	0	0	0	4	0	2	1	0	1	0	0	0	0	0	0	0	0	4	0	6	1	0	1	0	0	0	0	0	0	0	0	8
	23:30	0	3	0	0	0	0	0	0	0	0	0	0	3	0	2	1	0	0	0	0	0	0	0	0	0	0	3	0	5	1	0	0	0	0	0	0	0	0	0	0	6
	23:45	0	3	0	0	0	0	0	0	0	0	0	0	3	0	1	0	0	0	0	0	0	0	0	0	0	0	1	0	4	0	0	0	0	0	0	0	0	0	0	0	4
	Totals	8	931	479	7	44	5	43	8	54	2	10	0	1,591		933	440	4	38	28	6	4	84	0	16	0	0	1,564		1,864	919	11	82	33	49	12	138	2	26	0	0	3,155
	% of Totals	1%	59%	30%	0%	3%	0%	3%	1%	3%	0%	1%		100%	1%	60%	28%	0%	2%	2%	0%	0%	5%		1%			100%	1%	59%	29%	0%	3%	1%	2%	0%	4%	0%	1%		- 1	100%

#### **VOLUME**

### La Grange Rd/CR J59 S/O SR 120/SR 108

 Day: Tuesday
 City: Jamestown

 Date: 08/29/2023
 Project #: CA23\_090100\_002

		DΔI	LY TOT	ΊΔΙς			NB	SB	EB	WB	Total		DAII	v to	TALS		
		ואס	<u> </u>	7.5			1,591	1,564	0	0	3,155		DAIL	. 10	IALS		
				1	5-Minut	es Interv	/al						Hour	ly Inte	ervals		
TIME	NB	SB	EB	WB	TOTAL	TIME	NB	SB	EB	WB	TOTAL	TIME	NB	SB	EB	WB	TOTAL
0:00	1	5			6	12:00	16	26			42	00:00 01:00	8	11			19
0:15	1	1			2	12:15	26	24			50	01:00 02:00	4	8			12
0:30	3	3			6	12:30	34	13			47	02:00 03:00	12	13			25
0:45 1:00	3	2			5 2	12:45 13:00	20 13	16 20			36 33	03:00 04:00 04:00 05:00	12 30	11 19			23 49
1:15	3	1			4	13:15	20	28			48	05:00 06:00	101	46			147
1:30	1	2			3	13:30	27	31			58	06:00 07:00	152	44			196
1:45	0	3			3	13:45	17	44			61	07:00 08:00	153	81			234
2:00	1	0			1	14:00	34	37			71	08:00 09:00	105	82			187
2:15	4	8			12	14:15	18	21			39	09:00 10:00	114	89			203
2:30	6	3			9	14:30	27	32			59	10:00 11:00	92	90			182
2:45	1	2			3	14:45	16	23			39	11:00 12:00	78	86			164
3:00	0	2			2	15:00	30	34			64	12:00 13:00	96	79			175
3:15	4 2	0 4			4 6	15:15 15:30	22 17	33 30			55 47	13:00 14:00 14:00 15:00	77 95	123 113			200 208
3:30 3:45	6	5			11	15:30 15:45	21	30 32			53	14:00 15:00 15:00 16:00	95	113			208
4:00	6	5			11	16:00	25	25			50	16:00 17:00	101	139			240
4:15	6	8			14	16:15	30	44			74	17:00 18:00	70	146			216
4:30	5	3			8	16:30	19	41			60	18:00 19:00	69	97			166
4:45	13	3			16	16:45	27	29			56	19:00 20:00	35	61			96
5:00	16	9			25	17:00	21	32			53	20:00 21:00	36	42			78
5:15	26	17			43	17:15	18	41			59	21:00 22:00	35	22			57
5:30	27	7			34	17:30	16	41			57	22:00 23:00	13	20			33
5:45	32	13			45	17:45	15	32			47	23:00 00:00	13	13			26
6:00	32	14			46	18:00	20	27			47		1	ATIST			
6:15	26	12			38	18:15	19	32			51		NB	SB	EB	WB	TOTAL
6:30	46	7			53	18:30	18	16			34	Peak Period	00:00	to	12:00		
6:45	48	11			59	18:45	12	22			34	Volume	861	580			1441
7:00 7:15	36 54	21 18			57 72	19:00 19:15	12 5	15 10			27 15	Peak Hour Peak Volume	6:30 184	9:30 100			6:45 248
7:30	39	21			60	19:30	14	16			30	Peak Hour Factor	0.852	0.862			0.861
7:45	24	21			45	19:45	4	20			24	reak flour ractor	0.832	0.002			0.801
8:00	31	18			49	20:00	10	6			16	Peak Period	12:00	to	00:00		
8:15	24	31			55	20:15	8	15			23	Volume	730	984			1714
8:30	23	17			40	20:30	10	10			20	Peak Hour	16:00	16:15			16:15
8:45	27	16			43	20:45	8	11			19	Peak Volume	101	146			243
9:00	28	20			48	21:00	10	5			15	Peak Hour Factor	0.842	0.830			0.821
9:15	36	16			52	21:15	9	3			12						
9:30	14	29			43	21:30	8	7			15	Peak Period	07:00	to	09:00		101
9:45 10:00	36 20	24 19			60 39	21:45 22:00	8	7			15 11	Volume Peak Hour	258 7:00	163 7:30			7:00
10:00	30	28			58	22:00	2	4			6	Peak Volume	153	91			234
10:15	26	28 17			43	22:15	3	4			7	Peak Volume Peak Hour Factor	0.708	0.734			0.813
10:45	16	26			42	22:45	4	5			9	. cuk riour ractor	3.700	3.734			0.013
11:00	19	21			40	23:00	3	5			8	Peak Period	16:00	to	18:00		
11:15	22	26			48	23:15	4	4			8	Volume	171	285			456
11:30	17	21			38	23:30	3	3			6	Peak Hour	16:00	16:15			16:15
11:45	20	18			38	23:45	3	1			4	Peak Volume	101	146			243
TOTALS	861	580	0	0	1441	TOTALS	730	984	0	0	1714	Peak Hour Factor	0.842	0.830			0.821
SPLIT %	60%	40%	0%	0%	46%	SPLIT %	43%	57%	0%	0%	54%						



Location: SR 120/SR 108 & La Grange Rd/CR J59 City: Jamestown Control: 1-Way Stop(WB)

NS/EW Streets:		SR 120/5	SR 108			SR 120/	SR 108			La Grange	Rd/CR J59			La Grange F	Rd/CR J59		
		NORTH	BOUND			SOUTH	BOUND			EAST	BOUND			WESTE	BOUND		
AM	0	1	1	0	1	1	0	0	0	0	0	0	0	1	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	66	0	0	19	55	0	0	0	0	0	0	4	0	29	0	173
7:15 AM	0	63	3	0	10	69	0	0	0	0	0	0	7	0	41	0	193
7:30 AM	0	77	1	0	11	35	0	0	0	0	0	0	5	0	33	0	162
7:45 AM	0	82	2	0	14	67	0	0	0	0	0	0	2	0	19	0	186
8:00 AM	0	77	2	0	14	67	0	0	0	0	0	0	3	0	26	0	189
8:15 AM	0	64	3	0	21	66	0	0	0	0	0	0	3	0	14	0	171
8:30 AM	0	73	2	0	12	64	0	0	0	0	0	0	2	0	16	0	169
8:45 AM	0	77	1	0	12	64	0	0	0	0	0	0	3	0	20	0	177
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	579	14	0	113	487	0	0	0	0	0	0	29	0	198	0	1420
APPROACH %'s:	0.00%	97.64%	2.36%	0.00%	18.83%	81.17%	0.00%	0.00%					12.78%	0.00%	87.22%	0.00%	
PEAK HR :		07:15 AM -															TOTAL
PEAK HR VOL :	0	299	8	0	49	238	0	0	0	0	0	0	17	0	119	0	730
PEAK HR FACTOR :	0.000	0.912	0.667	0.000	0.875	0.862	0.000	0.000	0.000	0.000	0.000	0.000	0.607	0.000	0.726	0.000	0.946
		0.91	14			0.8	86							0.70	)8		
		NODTU	DOLIND			COUTH	DOLIND			EACT	POLIND			WECT	OLIND		
DM	0	NORTH		0		SOUTH		0	0		BOUND	0		WESTE		0	
PM	0	1	1	0	1	1	0	0	0	0	0	0	0	1	1	0	TOTAL
	NL	1 NT	1 NR	NU	SL	1 ST	0 SR	SU	EL	0 ET	0 ER	EU	WL	1 WT	1 WR	WU	TOTAL
4:00 PM	NL 0	1 NT 89	1 NR 4	NU 0	SL 18	1 ST 95	0 SR 0	SU 0	EL 0	0 ET 0	0 ER 0	EU 0	WL 4	MT 0	1 WR 18	WU 0	228
4:00 PM 4:15 PM	NL 0 0	1 NT 89 60	1 NR 4 2	NU 0 0	SL 18 37	1 ST 95 112	0 SR 0 0	0 0	0 0	0 ET	0 ER 0 0	0 0	WL 4 6	1 WT 0 0	1 WR 18 23	0 0	228 240
4:00 PM 4:15 PM 4:30 PM	NL 0 0 0	1 NT 89 60 47	1 NR 4 2 8	NU 0 0 0	SL 18 37 31	1 ST 95 112 105	0 SR 0 0	0 0 0	0 0 0	0 ET 0	0 ER 0 0	0 0 0	WL 4 6 4	1 WT 0 0 0	1 WR 18 23 14	0 0 0	228 240 209
4:00 PM 4:15 PM 4:30 PM 4:45 PM	NL 0 0 0 0	1 NT 89 60 47 77	1 NR 4 2 8 6	NU 0 0 0	SL 18 37 31 22	1 ST 95 112 105 115	0 SR 0 0 0	0 0 0 0	0 0 0 0	0 ET 0 0 0	0 ER 0 0 0	0 0	WL 4 6	1 WT 0 0 0	1 WR 18 23 14 22	WU 0 0 0	228 240 209 244
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM	NL 0 0 0 0 0	1 NT 89 60 47 77 79	1 NR 4 2 8 6	NU 0 0 0 0	SL 18 37 31 22 25	1 ST 95 112 105 115 76	0 SR 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0	0 ET 0 0 0 0	0 ER 0 0 0 0	EU 0 0 0 0 0 0 0	WL 4 6 4 2	1 WT 0 0 0 0	1 WR 18 23 14 22 19	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	228 240 209 244 202
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 0 0 0 0 0	1 NT 89 60 47 77 79 86	1 NR 4 2 8 6 3 6	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 18 37 31 22 25 34	1 ST 95 112 105 115 76 111	0 SR 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0	0 ET 0 0 0	0 ER 0 0 0 0 0	0 0 0 0	WL 4 6 4 2	1 WT 0 0 0 0 0	1 WR 18 23 14 22 19 13	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	228 240 209 244 202 254
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	NL 0 0 0 0 0 0	1 NT 89 60 47 77 79 86 71	1 NR 4 2 8 6 3 6 5	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 18 37 31 22 25 34 29	1 ST 95 112 105 115 76 111 95	0 SR 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ET 0 0 0 0 0	0 ER 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 4 6 4 2 0 4	1 WT 0 0 0 0 0	1 WR 18 23 14 22 19 13 14	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	228 240 209 244 202 254 215
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 0 0 0 0 0	1 NT 89 60 47 77 79 86	1 NR 4 2 8 6 3 6	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 18 37 31 22 25 34	1 ST 95 112 105 115 76 111	0 SR 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0	0 ET 0 0 0 0 0	0 ER 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 4 6 4 2 0 4 1	1 WT 0 0 0 0 0	1 WR 18 23 14 22 19 13	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	228 240 209 244 202 254
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	NL 0 0 0 0 0 0	1 NT 89 60 47 77 79 86 71	1 NR 4 2 8 6 3 6 5	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 18 37 31 22 25 34 29	1 ST 95 112 105 115 76 111 95	0 SR 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ET 0 0 0 0 0	0 ER 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 4 6 4 2 0 4 1	1 WT 0 0 0 0 0	1 WR 18 23 14 22 19 13 14	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	228 240 209 244 202 254 215
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	NL 0 0 0 0 0 0	1 NT 89 60 47 77 79 86 71 80	1 NR 4 2 8 6 3 6 5 12	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 18 37 31 22 25 34 29 18	1 ST 95 112 105 115 76 111 95 95	0 SR 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ET 0 0 0 0 0 0	0 ER 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 4 6 4 2 0 4 1 1 1	1 WT 0 0 0 0 0 0	1 WR 18 23 14 22 19 13 14 14	WU 0 0 0 0 0 0	228 240 209 244 202 254 215 220
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	NL 0 0 0 0 0 0 0	1 NT 89 60 47 77 79 86 71 80	1 NR 4 2 8 6 3 6 5 12	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 18 37 31 22 25 34 29 18	1 ST 95 112 105 115 76 111 95 95	0 SR 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ET 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 4 6 4 2 0 4 1 1 WL	1 WT 0 0 0 0 0 0 0	1 WR 18 23 14 22 19 13 14 14	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	228 240 209 244 202 254 215 220
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	NL 0 0 0 0 0 0 0 0 0 0 0	1 NT 89 60 47 77 79 86 71 80 NT 589	1 NR 4 2 8 6 3 6 5 12 NR 46 7.24%	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 18 37 31 22 25 34 29 18 SL 214	1 ST 95 112 105 115 76 111 95 95 ST 804	0 SR 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ET 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 4 6 4 2 0 4 1 1 1 WL 22	1 WT 0 0 0 0 0 0 0 0 0	1 WR 18 23 14 22 19 13 14 14 14	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	228 240 209 244 202 254 215 220
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	NL 0 0 0 0 0 0 0 0 0 0 0	1 NT 89 60 47 77 79 86 71 80 NT 589 92.76%	1 NR 4 2 8 6 3 6 5 12 NR 46 7.24%	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 18 37 31 22 25 34 29 18 SL 214	1 ST 95 112 105 115 76 111 95 95 ST 804	0 SR 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ET 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 4 6 4 2 0 4 1 1 1 WL 22	1 WT 0 0 0 0 0 0 0 0 0	1 WR 18 23 14 22 19 13 14 14 14	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	228 240 209 244 202 254 215 220 TOTAL 1812
4:00 PM 4:15 PM 4:30 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:35 PM 5:45 PM  TOTAL VOLUMES: APPROACH %'s: PEAK HR:	NL 0 0 0 0 0 0 0 0 0 0 0 0	1 NT 89 60 47 77 79 86 71 80 NT 589 92.76%	1 NR 4 2 8 6 6 3 6 5 12 NR 46 7.24% 05:00 PM 20 0.625	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 18 37 31 22 25 34 29 18 SL 214 21.02%	1 ST 95 112 105 115 76 111 95 95 ST 804 78.98%	0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ET 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 4 6 4 2 0 4 1 1 1 WL 22 13.84%	1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WR 18 23 14 22 19 13 14 14 14 WR 137 86.16%	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	228 240 209 244 202 254 215 220 TOTAL 1812

Location: SR 120/SR 108 & La Grange Rd/CR J59 City: Jamestown Control: 1-Way Stop(WB)

Project ID: 23-090099-001 Date: 8/29/2023

Data - 2axle	
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NS/EW Streets:		SR 120/5	SR 108			SR 120/	SR 108	·		La Grange	Rd/CR J59			La Grange F	Rd/CR J59	Ī	
		NORTH	BOLIND			SOUTH	BOLIND			FAST	BOUND			WESTE	ROLIND		
AM	0	1	1	0	1	1	0	0	0	0	0	0	0	1	1	0	
A.1V1	NL	NT	NR	NU	SL	ST	SR	SU	EL	ĒΤ	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	5	1	0	0	3	0	0	0	0	0	0	0	0	1	0	10
7:15 AM	Ô	3	Ō	Ö	Ö	1	ñ	Ö	0	n	Ô	ñ	ő	n	2	o l	6
7:30 AM	Ô	5	Ŏ	Ö	1	2	Ô	Ö	0	Ô	Ô	Ô	ő	0	0	ō	8
7:45 AM	ō	3	Ō	ō	ō	1	Ō	ō	0	Ō	Ō	Ō	,	0	i	ō	5
8:00 AM	0	4	0	0	1	1	0	0	0	0	0	0	0	0	0	0	6
8:15 AM	0	3	0	0	0	1	0	0	0	0	0	0	0	0	1	0	5
8:30 AM	0	6	0	0	0	1	0	0	0	0	0	0	0	0	3	0	10
8:45 AM	0	8	0	0	0	3	0	0	0	0	0	0	1	0	1	0	13
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	0	37	1	0	2	13	0	0	0	0	0	0	1	0	9	0	63
APPROACH %'s:	0.00%	97.37%	2.63%	0.00%	13.33%	86.67%	0.00%	0.00%					10.00%	0.00%	90.00%	0.00%	
PEAK HR:		07:15 AM -	08:15 AM														TOTAL
PEAK HR VOL :	0	15	0	0	2	5	0	0	0	0	0	0	0	0	3	0	25
PEAK HR FACTOR :	0.000	0.750	0.000	0.000	0.500	0.625	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.375	0.000	0.781
		0.7	50			0.5	33							0.3	75		
		NORTH	BOUND			SOUTH	BOUND				BOUND			WESTE	BOUND		
PM	0	NORTH 1	BOUND 1	0	1	SOUTH 1	BOUND 0	0	0	0	0	0	0	WESTE	BOUND 1	0	
	NL	NORTH 1 NT	BOUND	NU	SL	SOUTH 1 ST	BOUND 0 SR	SU	EL	0 ET	0 ER	EU	WL	WESTE 1 WT	BOUND 1 WR	WU	TOTAL
4:00 PM	NL 0	NORTH 1 NT 2	BOUND 1 NR 1	NU 0	SL 0	SOUTH 1 ST 3	BOUND 0 SR 0	SU 0	EL 0	0 ET 0	0 ER 0	EU 0	WL 0	WESTE 1 WT 0	BOUND 1 WR 2	WU 0	8
4:00 PM 4:15 PM	NL 0 0	NORTH 1 NT 2 4	BOUND  1  NR  1  1	NU 0 0	SL 0 2	SOUTH 1 ST 3 3	BOUND 0 SR 0 0	SU 0 0	EL 0 0	0 ET 0 0	0 ER 0 0	0 0	WL 0 1	WESTE  1 WT 0 0	BOUND 1 WR 2 0	0 0	8 11
4:00 PM 4:15 PM 4:30 PM	NL 0 0 0	NORTH 1 NT 2 4 0	BOUND  1  NR  1  1  1	NU 0 0 0	SL 0 2 0	SOUTH 1 ST 3 3 5	BOUND 0 SR 0 0	0 0 0	0 0 0	0 ET 0 0 0	0 ER 0 0	0 0 0	WL 0 1 0	WESTE 1 WT 0 0 0 0	80UND 1 WR 2 0	0 0 0	8 11 7
4:00 PM 4:15 PM 4:30 PM 4:45 PM	NL 0 0 0 0	NORTH 1 NT 2 4 0 5	BOUND  1  NR  1  1  0	NU 0 0 0	SL 0 2 0 0	SOUTH 1 ST 3 3 5	BOUND 0 SR 0 0 0	0 0 0 0	EL 0 0 0 0	0 ET 0 0 0	0 ER 0 0 0	0 0 0 0	WL 0 1 0 0	WESTE  1 WT 0 0 0 0	80UND 1 WR 2 0 1 2	0 0 0 0	8 11 7 8
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM	NL 0 0 0 0 0	NORTH 1 NT 2 4 0 5	BOUND 1 NR 1 1 1 0 0	NU 0 0 0 0	SL 0 2 0 0	SOUTH 1 ST 3 3 5 1	BOUND 0 SR 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0	0 ET 0 0 0 0	0 ER 0 0 0 0	EU 0 0 0 0 0 0 0	WL 0 1 0 0	WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	30UND 1 WR 2 0 1 2	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 11 7 8 10
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 0 0 0 0 0	NORTH 1 NT 2 4 0 5 3 3	BOUND 1 NR 1 1 1 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 2 0 0 0 2 2 2 2	SOUTH 1 ST 3 3 5 1 4	BOUND 0 SR 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0	0 ET 0 0 0 0 0	0 ER 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	30UND 1 WR 2 0 1 2 1	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 11 7 8 10 6
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NORTH 1 NT 2 4 0 5 3 3 2	BOUND  1  NR  1  1  0  0  2	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 2 0 0 0 2 2 2 1	SOUTH 1 ST 3 3 5 1 4 1 4	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ET 0 0 0 0 0	0 ER 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	BOUND 1 WR 2 0 1 2 1 0 1	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 11 7 8 10 6 10
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 0 0 0 0 0	NORTH 1 NT 2 4 0 5 3 3	BOUND 1 NR 1 1 1 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 2 0 0 0 2 2 2 2	SOUTH 1 ST 3 3 5 1 4	BOUND 0 SR 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0	0 ET 0 0 0 0 0	0 ER 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	30UND 1 WR 2 0 1 2 1	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 11 7 8 10 6
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NORTH 1 NT 2 4 0 5 3 3 2 1	BOUND 1 NR 1 1 1 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 2 0 0 0 2 2 1 2 2	SOUTH 1 ST 3 3 5 1 4 1 4	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ET 0 0 0 0 0 0	0 ER 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	BOUND 1 WR 2 0 1 2 1 0 1 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 11 7 8 10 6 10 3
4:00 PM 4:15 PM 4:30 PM 4:43 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 NL	NORTH 1 NT 2 4 0 5 3 3 2 1	BOUND 1 NR 1 1 0 0 0 0 NR NR	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 2 0 0 0 2 2 1 2 2 SL	SOUTH 1 ST 3 3 5 1 4 1 4 0	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ET 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	BOUND  1  WR  2  0  1  2  1  0  1  WR	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 11 7 8 10 6 10 3
4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NORTH 1 NT 2 4 0 5 3 3 2 1 NT 20	BOUND 1 NR 1 1 1 0 0 0 2 0 NR 5	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 2 0 0 0 2 2 1 2 2 SL 9	SOUTH 1 ST 3 3 5 1 4 1 4 0 ST 21	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ET 0 0 0 0 0 0	0 ER 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	BOUND 1 WR 2 0 1 2 1 0 1 0 WR 7	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 11 7 8 10 6 10 3
4:00 PM 4:15 PM 4:30 PM 4:43 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES :	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NORTH 1 NT 2 4 0 5 3 3 2 1 NT 20 80.00%	BOUND 1 NR 1 1 1 0 0 0 0 2 0 0 NR 5 20.00%	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 2 0 0 0 2 2 1 2 2 SL	SOUTH 1 ST 3 3 5 1 4 1 4 0	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ET 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	BOUND  1  WR  2  0  1  2  1  0  1  WR	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 11 7 8 10 6 10 3 TOTAL 63
4:00 PM 4:15 PM 4:30 PM 4:30 PM 4:43 PM 5:00 PM 5:15 PM 5:30 PM 5:33 PM 5:45 PM  TOTAL VOLUMES: APPROACH %'s: PEAK HR:	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NORTH 1 NT 2 4 0 5 3 3 2 1 NT 20 80.00% 04:00 PM -	BOUND 1 NR 1 1 1 1 0 0 0 0 2 0 NR 5 20.00% 05:00 PM	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 2 0 0 0 2 2 1 2 SL 9 30.00%	SOUTH 1 ST 3 3 5 1 4 1 4 0 0 ST 21 70.00%	BOUND 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ET 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	OUND 1 WR 2 0 1 2 1 0 0 1 0 WR 7 7 87.50%	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 11 7 8 10 6 10 3 TOTAL 63
4:00 PM 4:15 PM 4:30 PM 4:35 PM 5:30 PM 5:15 PM 5:30 PM 5:45 PM  TOTAL VOLUMES: APPROACH %'s: PEAK HR:	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NORTH 1 NT 2 4 0 5 3 3 2 1 NT 20 80.00% 04:00 PM -	BOUND 1 NR 1 1 1 0 0 0 2 0 NR 5 20.00% 05:00 PM 3	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 2 0 0 0 2 2 2 1 2 2 SL 9 30.00%	SOUTH 1 ST 3 3 5 1 4 1 4 0 ST 21 70.00%	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ET 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WESTE 1	30UND 1 WR 2 0 1 2 1 0 1 0 WR 7 87.50%	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 11 7 8 10 6 10 3 TOTAL 63
4:00 PM 4:15 PM 4:30 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:35 PM 5:45 PM  TOTAL VOLUMES: APPROACH %'s: PEAK HR:	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NORTH 1 NT 2 4 0 5 3 3 2 1 NT 20 80.00% 04:00 PM -	BOUND 1 NR 1 1 0 0 0 2 0 NR 5 20.00% 05:00 PM 3 0.750	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 2 0 0 0 2 2 1 2 SL 9 30.00%	SOUTH 1 ST 3 3 5 1 4 1 4 0 0 ST 21 70.00%	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 ET 0 0 0 0 0 0 0 0	0 ER 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SOUND 1 WR 2 0 1 2 1 0 1 0 WR 7 87.50%	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 11 7 8 10 6 10 3 TOTAL 63

Location: SR 120/SR 108 & La Grange Rd/CR J59 City: Jamestown Control: 1-Way Stop(WB)

Data - 3axle

	SR 120/S	R 108			SR 120/5	SR 108			La Grange	Rd/CR J59			La Grange F	Rd/CR J59		
	NORTHE	ROLIND			SOUTH	ROLIND			FAST	BOLIND			WESTE	ROLIND		
0			0	1			n	0			0	0			n	
-	-									-						TOTAL
																4
-						_	-		-	n	_		n			3
							-			n	_		n	_		4
-	1									n			n			3
	0												0			1
Ö				1			Ô			0	Ô	1	0	1		7
Ö	1			2			Ô	0	Ô	0	Ô	ō	0	Ō		3
-	1						-	_			_		n	1		4
_	_	_	_	_	_	-		_	-	_		_	-	_		-
NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
0	13	0	0	5	7	0	0	0	0	0	0	1	0	3	0	29
0.00%	100.00%	0.00%	0.00%	41.67%	58.33%	0.00%	0.00%					25.00%	0.00%	75.00%	0.00%	
		08:15 AM														TOTAL
0	6	0	0	0	4	0	0	0	0	0	0	0	0	1	0	11
0.000					0.500			0.000								
																0.688
															'	
	NORTHE	BOUND			SOUTH	BOUND			EAST	BOUND			WESTE	BOUND		
0	1	1	0	1	1	0	0	0	0	0	0	0	1	1	0	
NII			NII I	CI	CT	CD	CLI		FT	FD	EU	14/1			14/11	TOTAL
IVL	NT	NR	NU	JL	31	JI	SU	EL	LI	LIX	EU	VVL	WT	WR	WU	
0	NT 0	NR 0	0	0	1	0	0	0	0	0	0	0	0 0	WR 0	0	1
					1 1											1
0 0 0	0	0 0 0	0 0 0	0 0 0	1 1 3	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	1 3
0 0 0	0 0 0 1	0 0 0	0 0 0	0 0 0	1 1 3 0	0 0 0	0 0 0 0	0 0 0 0	0 0 0	0 0 0 0	0 0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	1 3 1
0 0 0 0	0 0 0 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 3 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 3 1
0 0 0 0 0	0 0 0 1 0	0 0 0 0	0 0 0 0	0 0 0 0 0	1 1 3 0 1 2	0 0 0 0 0	0 0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0	1 3 1 1 2
0 0 0 0 0	0 0 0 1 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	1 1 3 0 1 2	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	1 3 1 2 0
0 0 0 0 0	0 0 0 1 0	0 0 0 0	0 0 0 0	0 0 0 0 0	1 1 3 0 1 2	0 0 0 0 0	0 0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0	1 3 1 1 2
0 0 0 0 0 0	0 0 0 1 0 0 0	0 0 0 0 0 0	0 0 0 0 0	0 0 0 0 0 0	1 1 3 0 1 2 0 1	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0	1 3 1 2 0 1
0 0 0 0 0 0 0	0 0 0 1 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	1 1 3 0 1 2 0 1	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	1 3 1 1 2 0 1
0 0 0 0 0 0 0 0	0 0 0 1 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	1 1 3 0 1 2 0 1 ST	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0	1 3 1 2 0 1
0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 0 0 0 0 0 NT 1 100.00%	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	1 1 3 0 1 2 0 1	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	1 3 1 1 2 0 1 TOTAL
0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 0 0 0 0 0 NT 1 100.00%	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 SL 0	1 1 3 0 1 2 0 1 ST 9 100.00%	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	1 3 1 1 2 0 1 TOTAL 10
0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 0 0 0 0 0 NT 1 100.00%	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	1 1 3 0 1 2 0 1 ST	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	1 3 1 1 2 0 1 TOTAL
	0 0 NL 0 0.00%	NORTHE 0 1 NL NT 0 3 0 2 0 3 0 1 0 0 2 0 1 0 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 0 0 2 0 50 0 50 0 50 0 50 0 50 0 50 0	NIL	NORTHBOUND  0 1 1 0 0  NL NT NR NU  0 3 0 0  0 2 0 0  0 3 0 0  0 1 0 0  0 0 0 0  0 1 0 0  0 2 0 0  0 1 0 0  0 1 0 0  0 1 0 0  0 1 0 0  0 1 0 0  NL NT NR NU  0 13 0 0  0.00% 100.00% 0.00% 0.00%  07:15 AM - 08:15 AM  0 6 0 0  0.000 0.500 0.000 0.000  0.500	NORTHBOUND  0 1 1 1 0 1  NL NT NR NU SL  0 3 0 0 0 0  0 2 0 0 0  0 3 0 0 0  0 1 0 0 0  0 1 0 0 0  0 1 0 0 0  0 1 0 0 0  0 1 0 0 0  0 1 0 0 0  0 1 0 0 0  0 1 0 0 0  0 1 0 0 5  NIL NT NR NU SL  0 13 0 0 0 2  NIL NT NR NU SL  0 13 0 0 0 5  0.00% 100.00% 0.00% 0.00% 41.67%  0 6 0 0 0  0.000 0.500 0.000 0.000  0 10  0 1 1 0 1	NORTHBOUND   SOUTH    0	NORTHBOUND   SOUTHBOUND   O	NORTHBOUND   SOUTHBOUND   O   O   O   O   O   O   O   O   O	NORTHBOUND   SOUTHBOUND   NL NT NR NU SL ST SR SU EL	NORTHBOUND   SOUTHBOUND   PAST	NORTHBOUND   SOUTHBOUND   PASTBOUND   O 1   1   1   0   0   0   0   0   0   0	NORTHBOUND   SOUTHBOUND   EASTBOUND   O   1   1   1   0   0   0   0   0   0   0	NORTHBOUND   SOUTHBOUND   EASTBOUND   O   O   O   O   O   O   O   O   O	NORTHBOUND   SOUTHBOUND   EASTBOUND   WESTE	NORTHBOUND   SOUTHBOUND   EASTBOUND   O   O   O   O   O   O   O   O   O	NORTHBOUND   SOUTHBOUND   EASTBOUND   O

### ${\tt National\ Data\ \&\ Surveying\ Services} \\ Intersection\ Turning\ Movement\ Count$

Location: SR 120/SR 108 & La Grange Rd/CR J59 City: Jamestown Control: 1-Way Stop(WB)

-									4axle								
NS/EW Streets:		SR 120/	SR 108			SR 120/5	SR 108			La Grange	Rd/CR J59			La Grange F	Rd/CR J59		
		NORTH	BOUND			SOUTH	BOUND			EAST	BOUND			WESTE	BOUND		
AM	0	1	1	0	1	1	0	0	0	0	0	0	0	1	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	8	0	0	1	4	0	0	0	0	0	0	0	0	2	0	15
7:15 AM	0	10	1	0	3	5	0	0	0	0	0	0	0	0	3	0	22
7:30 AM	0	10 9	0	0	6	10 9	0	0	0	0	0	0	0	0	1	0	27
7:45 AM 8:00 AM	0	3	0 1	0	5 1	4	0	0	0	0	0	0	0	0	2	0	24 12
8:00 AM 8:15 AM	0	3 11	1	0	3	8	0	0	0	0	0	0	0	0	4	0	27
8:30 AM	0	3	0	0	2	6	0	0	0	0	0	0	0	0	2	0	13
8:45 AM	0	4	0	0	0	6	0	0	0	0	0	0	0	0	1	0	11
0:45 AM	U	4	U	U	U	0	U	U	U	U	U	U	U	U	1	U	11
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	0	58	3	0	21	52	0	0	0	0	0	0	1	0	16	0	151
APPROACH %'s:	0.00%	95.08%	4.92%	0.00%	28.77%	71.23%	0.00%	0.00%					5.88%	0.00%	94.12%	0.00%	
PEAK HR:		07:15 AM -					_	_	_	_	_	_	_	_	_	_	TOTAL
PEAK HR VOL :	0	32	2	0	15	28	0	0	0	0	0	0	1	0	7	0	85
PEAK HR FACTOR :	0.000	0.800	0.500	0.000	0.625	0.700	0.000	0.000	0.000	0.000	0.000	0.000	0.250	0.000	0.583	0.000	0.787
PEAK HR FACTOR :	0.000	0.800 0.7		0.000	0.625	0.700 0.67		0.000	0.000	0.000	0.000	0.000	0.250	0.000		0.000	0.787
	0.000	0.7	73	0.000	0.625	0.67	72	0.000	0.000			0.000	0.250	0.6	57	0.000	0.787
	0.000	0.7		0.000	0.625		72	0.000	0.000		BOUND 0	0.000	0.250		57	0.000	0.787
PM		0.7	73 BOUND			SOUTHI 1 ST	72 BOUND			EAST	BOUND			0.60 WESTE	67 BOUND		
PM 4:00 PM	0 NL 0	0.7 NORTH 1 NT 3	73 BOUND 1	0 NU 0	1 SL 1	SOUTHI	BOUND 0	0 SU 0	0 EL 0	EAST 0	BOUND 0 ER 0	0	0	0.60 WESTE	BOUND 1	0	TOTAL
PM 4:00 PM 4:15 PM	0 NL	0.7 NORTH 1 NT	BOUND 1 NR	0 NU	1 SL 1 1	SOUTHI 1 ST 6 1	BOUND 0 SR	0 SU	0 EL	EAST 0 ET	BOUND 0 ER	0 EU	0 WL	0.60 WESTE 1 WT	BOUND 1 WR	0 WU	TOTAL
PM 4:00 PM 4:15 PM 4:30 PM	0 NL 0 0	0.7 NORTH 1 NT 3 2	73  BOUND   1   NR   1   1   1   1   1   1	0 NU 0 0	1 SL 1 1 0	0.67 SOUTHI 1 ST 6 1 2	BOUND 0 SR 0 0	0 SU 0 0	0 EL 0 0	EAST 0 ET 0 0 0 0	BOUND 0 ER 0 0	0 EU 0 0	0 WL 0 0	0.66 WESTE 1 WT 0 0 0	80UND 1 WR 1 0	0 WU 0 0	TOTAL 12 5 4
PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM	0 NL 0 0 0	0.7 NORTH 1 NT 3 2 1	73  BOUND  1  NR  1  1  0	0 NU 0 0	1 SL 1 1 0	0.67 SOUTHI 1 ST 6 1 2	BOUND 0 SR 0 0 0 0 0	0 SU 0 0 0	0 EL 0 0 0	EAST 0 ET 0 0 0 0 0	BOUND 0 ER 0 0 0 0 0	0 EU 0 0 0	0 WL 0 0 0	0.60 WESTE 1 WT 0 0 0	30UND 1 WR 1 0 0	0 WU 0 0 0	TOTAL 12 5 4 2
PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM	0 NL 0 0 0	0.7  NORTH  1  NT  3  2  1  1	73 BOUND 1 NR 1 1 0 0	0 NU 0 0 0	1 SL 1 1 0 0	0.65 SOUTHI 1 ST 6 1 2 1	BOUND 0 SR 0 0 0 0 0 0 0 0	0 SU 0 0 0	0 EL 0 0 0	EAST 0 ET 0 0 0 0 0 0 0 0	BOUND 0 ER 0 0 0 0 0 0 0 0	0 EU 0 0 0	0 WL 0 0 0	0.66  WESTE 1  WT 0 0 0 0 0	80UND 1 WR 1 0	0 WU 0 0 0	TOTAL 12 5 4 2
PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	0 NL 0 0 0 0	0.7  NORTH  1  NT  3  2  1  1  1	73  BOUND  1  NR  1  1  0	0 NU 0 0 0 0	1 SL 1 0 0 0	0.65 SOUTHI 1 ST 6 1 2 1 3	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SU 0 0 0 0	0 EL 0 0 0 0	EAST 0 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 EU 0 0 0 0	0 WL 0 0 0 0	0.66  WESTE 1  WT 0 0 0 0 0 0	30UND 1 WR 1 0 0 0	0 WU 0 0 0 0	TOTAL 12 5 4 2 5 4
PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	0 NL 0 0 0 0	0.7  NORTH  1  NT  3  2  1  1  1	73  BOUND  1  NR  1  1  0  0  1  1  1  1  1  1  1  1  1	0 NU 0 0 0 0	1 SL 1 0 0 0	0.67 SOUTHI 1 ST 6 1 2 1 3 1	80UND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SU 0 0 0 0	0 EL 0 0 0 0	EAST 0 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 EU 0 0 0 0 0	0 WL 0 0 0 0	0.66  WESTE 1  WT 0 0 0 0 0 0 0	30UND 1 WR 1 0 0 0 1 1 0	0 WU 0 0 0 0	TOTAL 12 5 4 2 5 4 4 4
PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	0 NL 0 0 0 0	0.7  NORTH  1  NT  3  2  1  1  1	73 BOUND 1 NR 1 1 0 0	0 NU 0 0 0 0	1 SL 1 0 0 0	0.65 SOUTHI 1 ST 6 1 2 1 3	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SU 0 0 0 0	0 EL 0 0 0 0	EAST 0 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 EU 0 0 0 0	0 WL 0 0 0 0	0.66  WESTE 1  WT 0 0 0 0 0 0	30UND 1 WR 1 0 0 0	0 WU 0 0 0 0	TOTAL 12 5 4 2 5 4
4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM	0 NL 0 0 0 0 0 0 0	0.7  NORTH  1  NT  3  2  1  1  1  0  NT	73  BOUND  1  NR  1  1  0  0  NR  NR	0 NU 0 0 0 0 0 0	1 SL 1 1 0 0 0 1 1 1 0	0.67  SOUTHI 1 ST 6 1 2 1 3 1 1 3 ST	80UND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SU 0 0 0 0 0 0	0 EL 0 0 0 0 0 0	EAST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 EU 0 0 0 0 0 0 0	0 WL 0 0 0 0 0 0 0	0.60 WESTE 1 WT 0 0 0 0 0 0 0 WT	30UND 1 WR 1 0 0 1 1 0 0 WR	0 WU 0 0 0 0 0 0	TOTAL 12 5 4 2 5 4 4 3
PM  4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM	0 NL 0 0 0 0 0 0 0 0	0.7 NORTH 1 NT 3 2 1 1 1 1 0 NT 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	773   BOUND   1	0 NU 0 0 0 0 0 0 0	1 SL 1 0 0 0 1 1 0 0	0.65  SOUTHI 1 5T 6 1 2 1 3 1 1 3 ST 18	80UND 0	0 SU 0 0 0 0 0 0 0	0 EL 0 0 0 0 0	EAST 0	BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 EU 0 0 0 0 0	0 WL 0 0 0 0 0 0 0	0.66  WESTE 1  WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	30UND 1 WR 1 0 0 0 1 1 1 0 0 0 WR 3	0 WU 0 0 0 0 0 0 0	TOTAL 12 5 4 2 5 4 3
4:00 PM 4:15 PM 4:30 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	0 NL 0 0 0 0 0 0 0 0 0 0 0 0	0.7  NORTH 1 NT 3 2 1 1 1 0  NT 10 71.43%	773	0 NU 0 0 0 0 0 0	1 SL 1 1 0 0 0 1 1 1 0	0.67  SOUTHI 1 ST 6 1 2 1 3 1 1 3 ST	80UND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SU 0 0 0 0 0 0	0 EL 0 0 0 0 0 0	EAST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 EU 0 0 0 0 0 0 0	0 WL 0 0 0 0 0 0 0	0.66  WESTE 1  WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	30UND 1 WR 1 0 0 1 1 0 0 WR	0 WU 0 0 0 0 0 0	TOTAL 12 5 4 2 5 4 4 3 TOTAL 39
4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:15 PM 5:00 PM 5:30 PM 5:30 PM 5:45 PM	0 NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.7  NORTH  1  NT  3  2  1  1  1  1  1  7  1  0  NT  10  71.43%	73  BOUND  1  NR  1  1  0  0  1  NR  4  28.57%  05:00 PM	0 NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 SL 1 1 0 0 0 1 1 1 0 0 SL 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.67  SOUTHI 1 ST 6 1 2 1 3 1 1 3 ST 18 81.82%	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 EL 0 0 0 0 0 0	EAST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	BOUND 0 ER. 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 EU 0 0 0 0 0 0 0	0 WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.60 WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	30UND 1 WR 1 0 0 0 1 1 1 0 0 0 WR 3 100.00%	0 WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 12 5 4 2 2 5 4 4 3 TOTAL 39 TOTAL
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s: PEAK HR:	0 NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.7  NORTH 1 NT 3 2 1 1 1 0 NT 10 0 04:00 PM - 7	773    BOUND   1	0 NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 SL 1 1 0 0 0 1 1 0 5 5 4 18.18%	0.67 SOUTHI 1 ST 6 1 2 1 3 1 1 3 ST 18 81.82%	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 EL 0 0 0 0 0 0 0	EAST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	BOUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 EU 0 0 0 0 0 0 0	0 WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.60 WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	30UND 1 WR 1 0 0 0 1 1 1 0 0 0 0 1 1 1 1 0 0 0 0	0 WU 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 12 5 4 2 5 4 4 3 TOTAL 39
4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:15 PM 5:00 PM 5:30 PM 5:30 PM 5:45 PM	0 NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.7  NORTH  1  NT  3  2  1  1  1  1  1  7  1  0  NT  10  71.43%	73  BOUND 1 NR 1 1 0 0 0 1 0 NR 4 28.57% 05:00 PM 3 0.750	0 NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 SL 1 1 0 0 0 1 1 1 0 0 SL 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.67  SOUTHI 1 ST 6 1 2 1 3 1 1 3 ST 18 81.82%	80UND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 EL 0 0 0 0 0 0	EAST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	BOUND 0 ER. 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 EU 0 0 0 0 0 0 0	0 WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.60 WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	30UND 1 WR 1 0 0 0 1 1 1 0 0 WR 3 100.00% 1 0 0.250	0 WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 12 5 4 2 5 4 4 3 TOTAL 39

**Location:** SR 120/SR 108 & La Grange Rd/CR J59 **City:** Jamestown

04:00 PM - 05:00 PM 0.000

0.000

0 0.000 0.000

0 0.000

0 0.000

0 0.000

0 0.000

0 0.000

0 0.000

0 0.000

0 0.000

0 0.000

0 0.000

0.000

Control: 1-Way Stop(WB)

PEAK HR : PEAK HR VOL : PEAK HR FACTOR :

Project ID: 23-090099-001 Date: 8/29/2023

TOTAL

0

		16	

NS/EW Streets:		SR 120/	/SR 108			SR 120	/SR 108			La Grange	Rd/CR J59			La Grange	Rd/CR J59		
		NORTH	HBOUND			SOUTI	HBOUND			EAST	BOUND			WEST	BOUND		
AM	0	1	1	0	1	1	0	0	0	0	0	0	0	1	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR :		07:15 AM	- 08:15 AM														TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
50.4			HBOUND				HBOUND				BOUND				BOUND		
PM	0	1	1	0	1	1	0	0	0	0	0	0	0	1	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM 4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM 5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM 5:15 PM	0	0		0	0	0	0		0	0	0	0		0	0	0	0
5:15 PM 5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM 5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM																	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR:		04:00 PM	- 05:00 PM														TOTAL

# National Data & Surveying Services Intersection Turning

Location: SR 120/SR 108 & La Grange Rd/CR J59

Royement Count
Project ID: 23-090099-001
Date: 8/29/2023

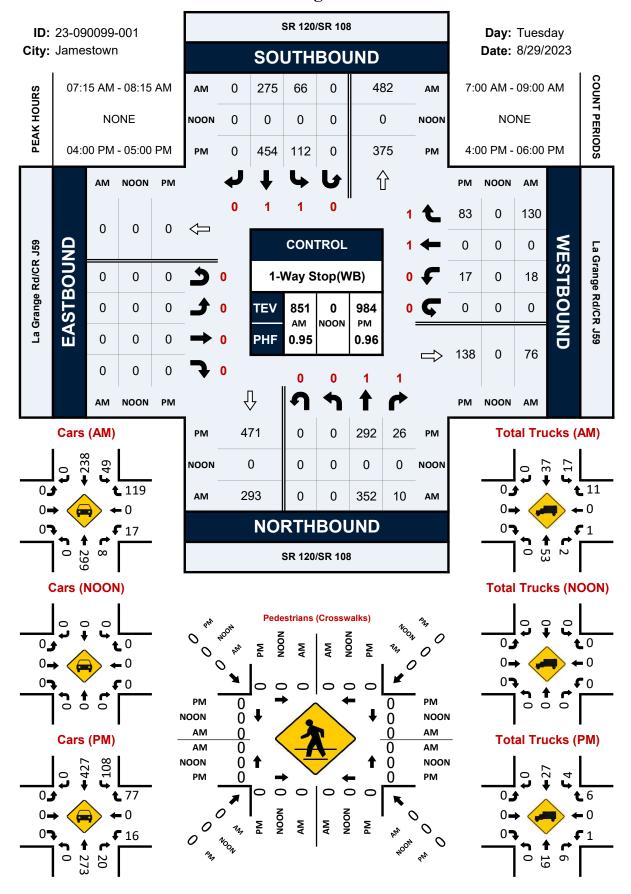
**Data - Pedestrians (Crosswalks)** 

NS/EW Streets:	SR 120	/SR 108	SR 120	)/SR 108	La Grange	Rd/CR J59	La Grange	Rd/CR J59	
AM	NORT EB	TH LEG WB	SOUT EB	TH LEG WB	EAST NB	r LEG SB	WEST NB	Γ LEG SB	TOTAL
7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 8:15 AM 8:30 AM	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
8:45 AM		0	0	0	0	0	0	0	0
TOTAL VOLUMES : APPROACH %'s :	EB 0	WB 0	EB 0	WB 0	NB 0	SB 0	NB 0	SB 0	TOTAL 0
PEAK HR : PEAK HR VOL : PEAK HR FACTOR :	<b>07:15 AM</b> 0	- <b>08:15 AM</b> 0	0	0	0	0	0	0	TOTAL 0

DM	NORT	'H LEG	SOUT	'H LEG	EAST	Γ LEG	WEST	Γ LEG	
PM	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES:	0	0	0	0	0	0	0	0	0
APPROACH %'s:									
PEAK HR :	04:00 PM	- 05:00 PM							TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR :									

### SR 120/SR 108 & La Grange Rd/CR J59

### **Peak Hour Turning Movement Count**



Location: Sierra Pacific Industries Dwy & La Grange Rd/CR J59 City: Jamestown Control: 1-Way Stop(SB)

		-		
1)2	ITA	- 1	יחו	гаі

NS/EW Streets:	Sie	erra Pacific I	Industries D	wy	Sier	ra Pacific Ir	ndustries Dv	vy		La Grange F	Rd/CR J59			La Grange F	Rd/CR J59		
		NORTI	HBOUND			SOUTH	BOUND			EASTB	OUND			WESTE	OUND		
AM	0	0	0	0	0	1	0	0	1	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	0	0	0	1	0	4	0	0	22	0	0	0	37	0	0	64
7:15 AM	0	0	0	0	0	0	1	0	0	18	0	0	0	48	0	0	67
7:30 AM	0	0	0	0	0	0	0	0	1	19	0	0	0	38	1	0	59
7:45 AM	0	0	0	0	0	0	0	0	0	17	0	0	0	23	0	0	40
8:00 AM	0	0	0	0	0	0	1	0	1	18	0	0	0	32	0	0	52
8:15 AM	0	0	0	0	0	0	1	0	0	26	0	0	0	23	0	0	50
8:30 AM	0	0	0	0	0	0	1	0	0	21	0	0	0	22	0	0	44
8:45 AM	0	0	0	0	0	0	0	0	0	15	0	0	0	28	0	0	43
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	0	0	0	0	1	0	8	0	2	156	0	0	0	251	1	0	419
APPROACH %'s :	·	·	·	ŭ	11.11%	0.00%	88.89%	0.00%	1.27%	98.73%	0.00%	0.00%	0.00%	99.60%	0.40%	0.00%	125
PEAK HR:		07:00 AM	- 08:00 AM														TOTAL
PEAK HR VOL :	0	0	0	0	1	0	5	0	1	76	0	0	0	146	1	0	230
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.250	0.000	0.313	0.000	0.250	0.864	0.000	0.000	0.000	0.760	0.250	0.000	0.858
						0.3	00			0.87	/5			0.76	6		
		NORTH	HROLIND														
PM	0		HBOUND 0	0	0	SOUTH	BOUND	0	1	EASTB	OUND	0	0	WESTE	OUND	0	
PM	0 NL	0	0	0 NU	0 SL	SOUTH 1	BOUND 0	<b>0</b> SU	1 EL	EASTB 1	OUND 0	<b>0</b> EU	0 WL	WESTE	OUND 0	0 WU	TOTAL
PM 4:00 PM				0 NU 0	0 SL 0	SOUTH	BOUND	0 SU 0	1 EL 1	EASTB	OUND	0 EU 0		WESTE	OUND	0 WU	TOTAL 57
	NL	0 NT	0 NR	NU	SL	SOUTH 1 ST	BOUND 0 SR	SU	EL	EASTB 1 ET	OUND 0 ER	EU	WL	WESTE 1 WT	OUND 0 WR	WU	
4:00 PM	NL 0	0 NT 0	0 NR 0	NU 0	SL 0	SOUTH 1 ST 0	BOUND 0 SR 0	SU 0	EL 1	EASTB 1 ET 33	OUND 0 ER 0	EU 0	WL 0	WESTE 1 WT 23	OUND 0 WR 0	WU 0	57
4:00 PM 4:15 PM	NL 0 0	0 NT 0 0	0 NR 0 0	NU 0 0	SL 0 0	SOUTH 1 ST 0	BOUND 0 SR 0	SU 0 0	EL 1 0	EASTB 1 ET 33 43	OUND 0 ER 0	0 0	WL 0 0	WESTE 1 WT 23 31	OUND 0 WR 0	0 0	57 74
4:00 PM 4:15 PM 4:30 PM	NL 0 0 0	0 NT 0 0	0 NR 0 0	NU 0 0 0	SL 0 0 0	SOUTH 1 ST 0 0	BOUND 0 SR 0 0	0 0 0	1 0 1	EASTB 1 ET 33 43 39	OUND 0 ER 0 0	0 0 0	0 0 0	WESTE 1 WT 23 31 19	OUND 0 WR 0 0	0 0 0	57 74 59
4:00 PM 4:15 PM 4:30 PM 4:45 PM	NL 0 0 0 0	0 NT 0 0 0	0 NR 0 0 0	NU 0 0 0 0	SL 0 0 0 0	SOUTH 1 ST 0 0 0 0	BOUND 0 SR 0 0 0	0 0 0 0	EL 1 0 1 0	EASTB 1 ET 33 43 39 27	OUND 0 ER 0 0 0	0 0 0 0	WL 0 0 0 0	WESTE  1 WT 23 31 19 23	OUND 0 WR 0 0 0	0 0 0 0	57 74 59 50
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM	NL 0 0 0 0	0 NT 0 0 0 0	0 NR 0 0 0 0	NU 0 0 0 0 0 0 0 0	SL 0 0 0 0	SOUTH 1 ST 0 0 0 0	BOUND 0 SR 0 0 0 0 1	SU 0 0 0 0 0 0 0 0	EL 1 0 1 0 0 0	EASTB 1 ET 33 43 39 27 31	OUND 0 ER 0 0 0 0 0	0 0 0 0 0	WL 0 0 0 0	WESTE 1 WT 23 31 19 23 21	OUND 0 WR 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	57 74 59 50 53
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 0 0 0 0 0	0 NT 0 0 0 0	0 NR 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0	SOUTH 1 ST 0 0 0 0	BOUND 0 SR 0 0 0 0 1 0 0 0	SU 0 0 0 0 0	EL 1 0 1 0 0 0 0 0	EASTB 1 ET 33 43 39 27 31 40	OUND 0 ER 0 0 0	EU 0 0 0 0 0	WL 0 0 0 0 0	WESTE 1 WT 23 31 19 23 21 17	OUND 0 WR 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	57 74 59 50 53 57
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	NL 0 0 0 0 0 0	0 NT 0 0 0 0 0	0 NR 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SOUTH 1 ST 0 0 0 0 0	BOUND 0 SR 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 1 0 1 0 0 0 0 0 0 0 0	EASTB 1 ET 33 43 39 27 31 40 42	OUND 0 ER 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WESTE  1 WT  23 31 19 23 21 17 16	OUND 0 WR 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	57 74 59 50 53 57 58
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	NL 0 0 0 0 0 0 0	0 NT 0 0 0 0 0	0 NR 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SOUTH 1 ST 0 0 0 0 0 0	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 0 1 0 0 0 0	EASTB 1 ET 33 43 43 39 27 31 40 42 28	OUND 0 ER 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WESTE 1 WT 23 31 19 23 21 17 16	OUND 0 WR 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0	57 74 59 50 53 57 58 45
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 NL	0 NT 0 0 0 0 0 0 0	0 NR 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SOUTH  1  ST  0  0  0  0  0  ST	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 1 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EASTB 1 ET 33 43 39 27 31 40 42 28	OUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WESTE 1 WT 23 31 19 23 21 17 16 17	OUND 0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	57 74 59 50 53 57 58 45
4:00 PM 4:15 PM 4:30 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 NL	0 NT 0 0 0 0 0 0 0 0 0	0 NR 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SOUTH 1 ST 0 0 0 0 0 0 0 0 ST 0	BOUND 0 SR 1	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 1 0 1 0 0 0 0 0 0 0 0 0 EL 2	EASTB 1 ET 33 43 39 27 31 40 42 28 ET 283	OUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WESTE 1 WT 23 31 19 23 21 17 16 17	OUND 0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	57 74 59 50 53 57 58 45
4:00 PM 4:15 PM 4:30 PM 4:43 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 NL	0 NT 0 0 0 0 0 0 0 0 0	0 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SOUTH 1 ST 0 0 0 0 0 0 0 0 ST 0	BOUND 0 SR 1	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 1 0 1 0 0 0 0 0 0 0 0 0 EL 2	EASTB 1 ET 33 43 39 27 31 40 42 28 ET 283	OUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WESTE 1 WT 23 31 19 23 21 17 16 17	OUND 0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	57 74 59 50 53 57 58 45 TOTAL 453
4:00 PM 4:15 PM 4:30 PM 4:43 PM 5:00 PM 5:15 PM 5:30 PM 5:35 PM 5:45 PM  TOTAL VOLUMES: APPROACH %'s: PEAK HR:	NL 0 0 0 0 0 0 0 0 0 0	0 NT 0 0 0 0 0 0 0 0 0 0 0 0 0	0 NR 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SOUTH 1 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	BOUND 0 SR 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 1 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EASTB 1 ET 33 43 43 29 27 31 40 42 28 ET 283 99.30%	OUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WESTE 1 WT 23 31 19 23 21 17 16 17 167 100.00%	OUND 0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	57 74 59 50 53 57 58 45 TOTAL 453

### ${\tt National\ Data\ \&\ Surveying\ Services} \\ Intersection\ Turning\ Movement\ Count$

Location: Sierra Pacific Industries Dwy & La Grange Rd/CR J59 City: Jamestown Control: 1-Way Stop(SB)

Data - Cars

								Dutu	- Cars								
NS/EW Streets:	Sie	erra Pacific I	Industries D	wy	Sier	ra Pacific Ir	ndustries Dv	vy		La Grange F	Rd/CR J59			La Grange R	Rd/CR J59		
		NORTI	HBOUND			SOUTH	BOUND			EASTE	OUND			WESTE	OUND		
AM	0	0	0	0	0	1	0	0	1	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	0	0	0	1	0	4	0	0	20	0	0	0	32	0	0	57
7:15 AM	0	0	0	0	0	0	0	0	0	15	0	0	0	45	0	0	60
7:30 AM	0	0	0	0	0	0	0	0	0	12	0	0	0	37	0	0	49
7:45 AM	0	0	0	0	0	0	0	0	0	13	0	0	0	20	0	0	33
8:00 AM	0	0	0	0	0	0	0	0	0	16	0	0	0	30	0	0	46
8:15 AM	0	0	0	0	0	0	0	0	0	22	0	0	0	17	0	0	39
8:30 AM	0	0	0	0	0	0	0	0	0	15	0	0	0	17	0	0	32
8:45 AM	0	0	0	0	0	0	0	0	0	13	0	0	0	24	0	0	37
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	0	0	0	0	1	0	4	0	0	126	0	0	0	222	0	0	353
APPROACH %'s:					20.00%	0.00%	80.00%	0.00%	0.00%	100.00%	0.00%	0.00%	0.00%	100.00%	0.00%	0.00%	
PEAK HR :		07:00 AM	- 08:00 AM														TOTAL
PEAK HR VOL :	0	0	0	0	1	0	4	0	0	60	0	0	0	134	0	0	199
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.250	0.000	0.250	0.000	0.000	0.750	0.000	0.000	0.000	0.744	0.000	0.000	0.829
						0.2	50			0.7	50			0.74	14		0.023
PM			HBOUND				BOUND			EASTE				WESTE			
PIVI	0 NL	0 NT	0 NR	0 NU	0 SL	1 ST	0 SR	0 SU	1 EL	1 ET	0 ER	0 EU	0 WL	1 WT	0 WR	0 WU	TOTAL
4:00 PM	0 0	0	0	0	0 0	0	0 0	0	0	29	0 0	0	0		0	0	51
4:00 PM 4:15 PM	0	0	0	0	0	0	-	U									
4:30 PM		U						Λ.	0				-	22			
		0	ň			-	0	0	0	39	0	0	Ō	29	0	Ō	68
4·45 PM	0	0	0	0	0	Ō	Ō	0	0	39 37	0	0	0	29 18	0	0	68 55
4:45 PM 5:00 PM	0	0	0	0	0	-	-	0	0	39 37 27	0 0 0	0 0 0	Ō	29 18 21	0 0 0	0 0 0	68 55 48
5:00 PM	0		0	0 0	0 0 0	0	0	0 0	0 0	39 37 27 29	0	0 0 0	0 0 0	29 18 21 18	0	0	68 55 48 48
5:00 PM 5:15 PM	0 0 0	0 0	0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 1 0	0 0 0 0	0 0 0 0	39 37 27 29 37	0 0 0	0 0 0 0	0 0 0	29 18 21 18 16	0 0 0 0	0 0 0 0	68 55 48 48 53
5:00 PM	0	0	0 0	0 0	0 0 0	0 0	0 0 1	0 0	0 0	39 37 27 29	0 0 0 0	0 0 0	0 0 0 0	29 18 21 18	0 0 0	0 0 0	68 55 48 48
5:00 PM 5:15 PM 5:30 PM	0 0 0 0 0	0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 1 0 0	0 0 0 0 0	0 0 0 0 0	39 37 27 29 37 38 26	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	29 18 21 18 16 15	0 0 0 0 0 0	0 0 0 0 0 0	68 55 48 48 53 53 43
5:00 PM 5:15 PM 5:30 PM 5:45 PM	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 1 0 0 0	0 0 0 0 0	0 0 0 0 0 0	39 37 27 29 37 38 26	0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0	29 18 21 18 16 15 17	0 0 0 0 0 0 0	0 0 0 0 0 0 0	68 55 48 48 53 53 43
5:00 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES:	0 0 0 0 0	0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0 0 5 SL	0 0 0 0 0 0 0	0 0 1 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0	39 37 27 29 37 38 26 ET 262	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	29 18 21 18 16 15 17 WT 156	0 0 0 0 0 0 0	0 0 0 0 0 0 0	68 55 48 48 53 53 43
5:00 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s:	0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 1 0 0 0	0 0 0 0 0	0 0 0 0 0 0	39 37 27 29 37 38 26	0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0	29 18 21 18 16 15 17	0 0 0 0 0 0 0	0 0 0 0 0 0 0	68 55 48 48 53 53 43 TOTAL 419
5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s:	0 0 0 0 0 0	0 0 0 0 0 0 NT 0	0 0 0 0 0 0 NR 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 SL 0 0.00%	0 0 0 0 0 0 0 ST 0 0.00%	0 0 1 0 0 0 0 SR 1 100.00%	0 0 0 0 0 0 5U 0 0.00%	0 0 0 0 0 0 0	39 37 27 29 37 38 26 ET 262 100.00%	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	29 18 21 18 16 15 17 WT 156 100.00%	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	68 55 48 48 53 53 43 TOTAL 419
5:00 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s: PEAK HR:	0 0 0 0 0 0 0 NL 0	0 0 0 0 0 0 NT 0	0 0 0 0 0 0 NR 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 SL 0 0.00%	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 1 0 0 0 0 SR 1 100.00%	0 0 0 0 0 0 5U 0 0.00%	0 0 0 0 0 0 0 0 EL 0 0.00%	39 37 27 29 37 38 26 ET 262 100.00%	0 0 0 0 0 0 0 0 0 ER 0 0.00%	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	29 18 21 18 16 15 17 WT 156 100.00%	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	68 55 48 48 53 53 43 TOTAL 419
5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s:	0 0 0 0 0 0	0 0 0 0 0 0 NT 0	0 0 0 0 0 0 NR 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 SL 0 0.00%	0 0 0 0 0 0 0 ST 0 0.00%	0 0 1 0 0 0 0 SR 1 100.00%	0 0 0 0 0 0 5U 0 0.00%	0 0 0 0 0 0 0	39 37 27 29 37 38 26 ET 262 100.00%	0 0 0 0 0 0 0 0 0 ER 0 0.00%	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	29 18 21 18 16 15 17 WT 156 100.00%	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	68 55 48 48 53 53 43 TOTAL 419

### ${\tt National\ Data\ \&\ Surveying\ Services} \\ Intersection\ Turning\ Movement\ Count$

Location: Sierra Pacific Industries Dwy & La Grange Rd/CR J59 City: Jamestown Control: 1-Way Stop(SB)

								Data -	2axle								
NS/EW Streets:	Si	ierra Pacific I	Industries D	Dwy	Sie	erra Pacific I	Industries D	Dwy		La Grange F	Rd/CR J59			La Grange I	Rd/CR J59		
		NORT	HBOUND			SOUTI	HBOUND			EASTE	OUND			WESTE	BOUND		
AM	0	0	0	0	0	1	0	0	1	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	0	0	0	0	0	0	0	0	1	0	0	0	1	0	0	2
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1
7:30 AM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	1	0	2
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1
8:30 AM 8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	3 2	0	0	4 2
8:45 AM	0	U	U	0	0	0	0	0	0	U	U	U	U	2	U	U	2
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	0	0	0	0	0	0	0	0	0	3	0	0	0	9	1	0	13
APPROACH %'s:									0.00%	100.00%	0.00%	0.00%	0.00%	90.00%	10.00%	0.00%	
PEAK HR :			- 08:00 AM														TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0	2	0	0	0	3	1	0	6
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.500	0.000	0.000	0.000	0.750	0.250	0.000	0.750
										0.5	00			1.0	00		
		NORT	HBOUND			SOUT	HBOUND			EASTE	OUND			WESTE	BOUND		
PM	0	0	0	0	0	1	0	0	1	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0	2	0	0	0	0	0	0	2
4:15 PM	0	0	0	0	0	0	0	0	0	2	0	0	0	2	0	0	4
4:30 PM	0	0	0	0	0	0	0	0	0	2	0	0	0	1	0	0	3
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0	0	2
5:00 PM	0	0	0	0	0	0	0	0	0	2	0	0	0	2	0	0	4
5:15 PM	0	0	0	0	0	0	0	0	0	2	0	0	0	0	0	0	2
5:30 PM	0	0	0	0	0	0	0	0	0	2	0	0	0	1	0	0	3
5:45 PM	0	0	0	0	0	0	0	0	0	2	0	0	0	0	0	0	2
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	0	0	0	0	0	0	0	0	0	14	0	0	0	8	0	0	22
APPROACH %'s:									0.00%	100.00%	0.00%	0.00%	0.00%	100.00%	0.00%	0.00%	
PEAK HR:			- 05:00 PM								_						TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0	6	0	0	0	5	0	0	11
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.750	0.000	0.000	0.000	0.625	0.000	0.000	0.688

Location: Sierra Pacific Industries Dwy & La Grange Rd/CR J59 City: Jamestown Control: 1-Way Stop(SB)

Data - 3axle

_																	
NS/EW Streets:	Sie	erra Pacific I	ndustries D	wy	Sier	ra Pacific Ir	ndustries Dv	vy		La Grange I	Rd/CR J59			La Grange F	Rd/CR J59		
		NORTH	HBOUND			SOUTH	BOLIND			EASTE	ULIND			WESTE	NOLIND		
AM	0	0	0	0	0	1	0	0	1	1	0	0	0	1	0	0	
AIVI .	NL	NT	NR	NU	SL	ST	SR	SU	ĒL	ĒT	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0	0	2
7:15 AM	0	0	Ö	0	0	0	1	0	Ö	Ö	n	0	0	0	0	0	1
7:30 AM	0	0	0	0	0	0	Ô	0	0	0	0	0	0	1	0	0	1
7:45 AM	0	0	Ö	0	0	0	0	0	0	0	0	0	0	ō	0	0	ō
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	Ô	Ô	Ö	Ô	o o	Ô	1	0	0	1	ñ	o l	o o	Ö	0	o l	2
8:30 AM	Ô	Ô	Ŏ	Ö	o o	Ô	ō	0	0	0	Ô	o l	o o	Ö	0	o l	0
8:45 AM	Ô	Ô	Ö	Ö	0	Ö	0	0	0	0	Ô	o l	o o	1	Ö	o l	1
0.15741	•	•	•	•	_	•	•	•	•	•	•	•	_	-	•	ŭ	-
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTA
TOTAL VOLUMES:	0	0	0	0	0	0	2	0	0	1	0	0	0	4	0	0	7
APPROACH %'s:					0.00%	0.00%	100.00%	0.00%	0.00%	100.00%	0.00%	0.00%	0.00%	100.00%	0.00%	0.00%	
PEAK HR :		07:00 AM	- 08:00 AM														TOTA
			•	0	0	0	1	0	0	0	0	0	0	3	0	0	4
PEAK HR VOL :	0	0	0														
							0.250	0.000	0.000	0.000	0.000	0.000	0.000	0.375	0.000	0.000	
PEAK HR VOL : PEAK HR FACTOR :	0 0.000	0.000	0.000	0.000	0.000	0.000	0.250 50	0.000	0.000	0.000	0.000	0.000	0.000	0.375	0.000 75	0.000	0.500
		0.000	0.000			0.000	50	0.000	0.000			0.000	0.000	0.37	75	0.000	0.500
PEAK HR FACTOR :	0.000	0.000 NORTH	0.000 HBOUND	0.000	0.000	0.000 0.2	BOUND			EASTE	OUND			0.37 WESTE	75 BOUND		0.500
	0.000	0.000 NORTH 0	0.000 HBOUND 0	0.000	0.000	0.000 0.2 SOUTH	BOUND 0	0	1	EASTE 1	OUND 0	0	0	0.33 WESTE	75 BOUND 0	0	
PEAK HR FACTOR:	0.000 0 NL	0.000 NORTH 0 NT	0.000  HBOUND 0 NR	0.000 0 NU	0.000 0 SL	0.000 0.2 SOUTH 1 ST	BOUND 0 SR	0 SU	1 EL	EASTE 1 ET	OUND 0 ER	0 EU	0 WL	0.33 WESTE 1 WT	OUND O WR	0 WU	TOTA
PEAK HR FACTOR:  PM  4:00 PM	0.000 0 NL 0	0.000 NORTH 0 NT	0.000 HBOUND 0 NR 0	0.000 0 NU 0	0.000 0 SL 0	0.000 0.2 SOUTH 1 ST 0	BOUND 0 SR 0	0 SU 0	1 EL 0	EASTE 1 ET 0	OUND 0 ER 0	0 EU 0	0 WL 0	0.33 WESTE 1 WT 0	BOUND 0 WR 0	0 WU 0	TOTA 0
PIM  4:00 PM 4:15 PM	0.000 0 NL 0 0	0.000 NORTH 0 NT 0 0	0.000 HBOUND 0 NR 0	0.000 0 NU 0 0	0.000 0 SL 0 0	0.000 0.2 SOUTH 1 ST 0 0	BOUND 0 SR 0	0 SU 0 0	1 EL 0 0	EASTE 1 ET 0	OUND 0 ER 0	0 EU 0 0	0 WL 0 0	0.33 WESTE 1 WT 0 0	80UND 0 WR 0	0 WU 0 0	TOTA 0 0
PM 4:00 PM 4:15 PM 4:30 PM	0.000 0 NL 0 0 0	0.000  NORTH 0 NT 0 0	0.000  HBOUND  0  NR  0  0  0	0.000 0 NU 0 0 0	0.000 0 SL 0 0	0.000 0.2 SOUTH 1 ST 0 0	BOUND 0 SR 0 0	0 SU 0 0	1 EL 0 0	EASTE 1 ET 0 0	OUND 0 ER 0 0	0 EU 0 0	0 WL 0 0	0.33 WESTE 1 WT 0 0	80UND 0 WR 0 0	0 WU 0 0	TOTA 0 0 0
PEAK HR FACTOR:  PM  4:00 PM  4:15 PM  4:30 PM  4:45 PM	0.000 0 NL 0 0 0 0	0.000  NORTH 0 NT 0 0 0 0	0.000  HBOUND  O  NR  O  O  O  O	0.000 0 NU 0 0 0 0	0.000 0 SL 0 0 0	0.000 0.2 SOUTH 1 ST 0 0 0	BOUND 0 SR 0 0 0 0 0	0 SU 0 0	1 EL 0 0 0	EASTE 1 ET 0 0 0 0 0 0	OUND 0 ER 0 0 0	0 EU 0 0	0 WL 0 0 0	0.33 WESTE 1 WT 0 0 0	80UND 0 WR 0 0	0 WU 0 0 0	TOTA 0 0 0 0
PEAK HR FACTOR:  PIN  4:00 PM 4:15 PM 4:30 PM 4:34 PM 5:00 PM	0.000 0 NL 0 0 0 0	0.000  NORTH 0 NT 0 0 0 0 0	0.000  HBOUND  O  NR  O  O  O  O	0.000 0 NU 0 0 0 0 0	0.000 SL 0 0 0 0	0.000 0.2 SOUTH 1 ST 0 0 0	BOUND 0 SR 0 0 0 0 0 0 0	0 SU 0 0 0	1 EL 0 0 0 0	EASTE 1 ET 0 0 0 0 0 0 0 0 0	OUND 0 ER 0 0 0 0 0 0 0	0 EU 0 0 0	0 WL 0 0 0	0.33 WESTE 1 WT 0 0 0	80UND 0 WR 0 0 0	0 WU 0 0 0	TOTA 0 0 0 0 0 0
PEAK HR FACTOR:  PM  4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	0.000 0 NL 0 0 0 0 0	0.000  NORTH 0 NT 0 0 0 0 0	0.000  HBOUND 0 NR 0 0 0 0 0 0	0.000 NU 0 0 0 0 0 0	0.000 SL 0 0 0 0 0	0.000 0.2 SOUTH 1 ST 0 0 0 0	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SU 0 0 0 0	1 EL 0 0 0 0	EASTE 1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	OUND 0 ER 0 0 0	0 EU 0 0 0 0	0 WL 0 0 0 0	0.37 WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	80UND 0 WR 0 0 0 0	0 WU 0 0 0 0	TOTA 0 0 0 0 0
PEAK HR FACTOR:  PM  4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	0.000 0 NL 0 0 0 0 0 0	0.000  NORTH  0  NT  0  0  0  0  0  0  0  0  0	0.000  HBOUND  O  NR  O  O  O  O  O  O  O	0.000 0 NU 0 0 0 0 0 0	0.000 SL 0 0 0 0 0	0.000 0.2 SOUTH 1 ST 0 0 0 0	50 BOUND 0 SR 0 0 0 0	0 SU 0 0 0 0	1 EL 0 0 0 0 0	EASTE 1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	OUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 EU 0 0 0 0	0 WL 0 0 0 0	0.37 WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	80UND 0 WR 0 0 0 0 0	0 WU 0 0 0 0	TOTA 0 0 0 0 0 0 0
PEAK HR FACTOR:  PM  4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	0.000 0 NL 0 0 0 0 0	0.000  NORTH 0 NT 0 0 0 0 0	0.000  HBOUND 0 NR 0 0 0 0 0 0	0.000 NU 0 0 0 0 0 0	0.000 SL 0 0 0 0 0	0.000 0.2 SOUTH 1 ST 0 0 0 0	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SU 0 0 0 0	1 EL 0 0 0 0	EASTE 1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	OUND 0 ER 0 0 0	0 EU 0 0 0 0	0 WL 0 0 0 0	0.37 WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	80UND 0 WR 0 0 0 0	0 WU 0 0 0 0	TOTA 0 0 0 0 0
PEAK HR FACTOR:  PM  4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:00 PM 5:15 PM 5:30 PM 5:39 PM 5:45 PM	0.000 0 NL 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000  NORTH 0 NT 0 0 0 0 0 0 0 NT	0.000  HBOUND  NR  0  0  0  0  0  NR  NR  NR  NR	0.000 0 NU 0 0 0 0 0 0 0 0 0 0	0.000 0 SL 0 0 0 0 0 0 0 SL	0.000 0.2 SOUTH 1 ST 0 0 0 0 0 0 0	50  BOUND  SR  0  0  0  0  0  0  0  SR  SR  SR	0 SU 0 0 0 0 0	1 EL 0 0 0 0 0 0 0	EASTE 1	OUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 ER	0 EU 0 0 0 0 0 0	0 WL 0 0 0 0 0 0 0	0.33  WESTE  1  WT  0  0  0  0  0  WT	80UND 0 WR 0 0 0 0 0 0 0	0 WU 0 0 0 0 0 0	TOTA 0 0 0 0 0 0 0 TOTA
PEAK HR FACTOR:  PM  4:00 PM 4:15 PM 4:30 PM 4:35 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM TOTAL VOLUMES:	0.000 0.000 NL 0 0 0 0 0 0	0.000  NORTH 0 NT 0 0 0 0 0 0 0 0	0.000  HBOUND  NR  0  0  0  0  0  0  0  0  0	0.000 NU 0 0 0 0 0 0 0 0	0.000 SL 0 0 0 0 0 0	0.000 0.2 SOUTH 1 ST 0 0 0 0 0	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SU 0 0 0 0 0	1 EL 0 0 0 0 0 0	EASTE 1 ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	OUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 EU 0 0 0 0 0	0 WL 0 0 0 0 0	0.37 WESTE 1 WT 0 0 0 0 0 0 0 0	80UND 0 WR 0 0 0 0 0	0 WU 0 0 0 0	TOTA 0 0 0 0 0 0 0 0 0
PEAK HR FACTOR:  4:00 PM 4:15 PM 4:30 PM 4:35 PM 5:00 PM 5:15 PM 5:30 PM 5:34 PM TOTAL VOLUMES: APPROACH %'s:	0.000 0 NL 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000  NORTH 0 NT 0 0 0 0 0 0 0 NT 0 NT 0 NT 0 NT	0.000  HBOUND 0 NR 0 0 0 0 0 NR NR 0 0 NR 0 0 NR 0 0 NR 0	0.000 0 NU 0 0 0 0 0 0 0 0 0 0	0.000 0 SL 0 0 0 0 0 0 0 SL	0.000 0.2 SOUTH 1 ST 0 0 0 0 0 0 0	50  BOUND  SR  0  0  0  0  0  0  0  SR  SR  SR	0 SU 0 0 0 0 0	1 EL 0 0 0 0 0 0 0	EASTE 1	OUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 ER	0 EU 0 0 0 0 0 0	0 WL 0 0 0 0 0 0 0	0.33  WESTE  1  WT  0  0  0  0  0  WT	80UND 0 WR 0 0 0 0 0 0 0	0 WU 0 0 0 0 0 0	TOTA 0 0 0 0 0 0 0 0 0 TOTA
PEAK HR FACTOR:  4:00 PM 4:15 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:39 PM 5:45 PM  TOTAL VOLUMES: APPROACH %'s: PEAK HR:	0.000 0 NL 0 0 0 0 0 0 0 0 0 NL	0.000  NORTH 0 NT 0 0 0 0 0 0 0 NT 0 0 0 0 0 0 0 0 0	0.000  HBOUND  O  NR  O  O  O  O  NR  O  O  O  O  O  O  O  O  O  O  O  O  O	0.000 0 NU 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000  O SL  O O  O O  SSL  O O  SSL  O O  O O	0.000 0.2 SOUTH 1 ST 0 0 0 0 0 0 0 0 0 0 0	BOUND 0 SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EASTE 1	OUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 EU 0 0 0 0 0 0	0 WL 0 0 0 0 0 0 0	0.33 WESTE 1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000ND 0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 WU 0 0 0 0 0 0 0	TOTA 0 0 0 0 0 0 0 0 TOTA
PEAK HR FACTOR:  4:00 PM 4:15 PM 4:30 PM 4:35 PM 5:00 PM 5:15 PM 5:30 PM 5:34 PM TOTAL VOLUMES: APPROACH %'s:	0.000 0 NL 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000  NORTH 0 NT 0 0 0 0 0 0 0 NT 0 NT 0 NT 0 NT	0.000  HBOUND 0 NR 0 0 0 0 0 NR NR 0 0 NR 0 0 NR 0 0 NR 0	0.000 0 NU 0 0 0 0 0 0 0 0 0 0	0.000 0 SL 0 0 0 0 0 0 0 SL	0.000 0.2 SOUTH 1 ST 0 0 0 0 0 0 0	50  BOUND  SR  0  0  0  0  0  0  0  SR  SR  SR	0 SU 0 0 0 0 0	1 EL 0 0 0 0 0 0 0	EASTE 1	OUND 0 ER 0 0 0 0 0 0 0 0 0 0 0 ER	0 EU 0 0 0 0 0 0	0 WL 0 0 0 0 0 0 0	0.33  WESTE  1  WT  0  0  0  0  0  WT	80UND 0 WR 0 0 0 0 0 0 0	0 WU 0 0 0 0 0 0	TOTAI 0 0 0 0 0 0 0 0

Location: Sierra Pacific Industries Dwy & La Grange Rd/CR J59 City: Jamestown Control: 1-Way Stop(SB)

Data - 4axle

_								Data -	4axle								
NS/EW Streets:	Sie	erra Pacific I	Industries D	wy	Sier	ra Pacific I	ndustries Dv	vy		La Grange F	Rd/CR J59			La Grange F	Rd/CR J59		
		NORTI	HBOUND			SOUTH	IBOUND			EASTE	OUND			WESTE	BOUND		
AM	0	0	0	0	0	1	0	0	1	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	0	0	0	0	0	0	0	0	1	0	0	0	2	0	0	3
7:15 AM	0	0	0	0	0	0	0	0	0	3	0	0	0	2	0	0	5
7:30 AM	0	0	0	0	0	0	0	0	1	6	0	0	0	0	0	0	7
7:45 AM	0	0	0	0	0	0	0	0	0	4	0	0	0	2	0	0	6
8:00 AM	0	0	0	0	0	0	1	0	1	2	0	0	0	2	0	0	6
8:15 AM	0	0	0	0	0	0	0	0	0	3	0	0	0	5	0	0	8
8:30 AM	0	0	0	0	0	0	1	0	0	5	0	0	0	2	0	0	8
8:45 AM	0	0	0	0	0	0	0	0	0	2	0	0	0	1	0	0	3
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	0	0	0	0	0	0	2	0	2	26	0	0	0	16	0	0	46
APPROACH %'s:					0.00%	0.00%	100.00%	0.00%	7.14%	92.86%	0.00%	0.00%	0.00%	100.00%	0.00%	0.00%	
PEAK HR :		07:00 AM	- 08:00 AM														TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	1	14	0	0	0	6	0	0	21
PEAK HR FACTOR:	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.250	0.583	0.000	0.000	0.000	0.750	0.000	0.000	0.750
										0.5	36			0.7	50		0.750
			HBOUND				IBOUND			EASTE				WESTE			
PM	0	0	0	0	0	1	0	0	1	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	1	2	0	0	0	1	0	0	4
4:15 PM	0	0	0	0	0	0	0	0	0	2	0	0	0	0	0	0	2
4:30 PM	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	1
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1
5:15 PM	0	0	0	0	0	0	0	0	0	1	0	0	0	1	0	0	2
5:30 PM	0	0	0	0	0	0	0	0	0	2	0	0	0	0	0	0	2
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	0	0	0	0	0	0	0	0	2	7	0	0	0	3	0	0	12
APPROACH %'s:					l				22.22%	77.78%	0.00%	0.00%	0.00%	100.00%	0.00%	0.00%	
AFFROACH /03.																	
PEAK HR:		04:00 PM	- 05:00 PM														TOTAL
	0	<b>04:00 PM</b>	- <b>05:00 PM</b> 0	0	0	0	0	0	2	4	0	0	0	1	0	0	TOTAL 7
PEAK HR:	0 0.000			0 0.000	0 0.000	0 0.000	0 0.000	0.000	2 0.500	4 0.500 0.5	0.000	0 0.000	0 0.000	1 0.250 0.2	0.000	0 0.000	-

Location: Sierra Pacific Industries Dwy & La Grange Rd/CR J59 City: Jamestown Control: 1-Way Stop(SB)

Data - Rikes

								Data	Bikes								_
NS/EW Streets:	Sic	erra Pacific I	Industries D	wy	Sie	erra Pacific I	ndustries D	wy		La Grange	Rd/CR J59			La Grange	Rd/CR J59		
		NORTI	HBOUND			SOUTI	HBOUND			EAST	BOUND			WEST	BOUND		
AM	0	0	0	0	0	1	0	0	1	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM 8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM 8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
8:45 AM	ľ	U	U	0	0				U	U	U	U	0	U	U	U	0
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR :		07:00 AM	- 08:00 AM														TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR:	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
	<u> </u>																
		NODTI	HBOUND			SOLITI	HBOUND			FAST	BOUND			WEST	BOUND		
PM	0	0	0	0		30011											
1 171	NL				. 0	1	0	0	1		0	0	0			0	
4:00 PM		NT			0 SL	1 ST	0 SR	0 SU	1 EL	1	0 ER	0 EU	0 WL	1	0	0 WU	TOTAL
	0	NT 0	NR 0	NU 0	0 SL 0	1 ST 0	0 SR 0	O SU O	1 EL 0		0 ER 0	0 EU 0	0 WL			0 WU 0	TOTAL 0
4:15 PM			NR	NU	SL	ST	SR	SU	EL	1 ET	ER	EU	WL	1 WT	0 WR	WU	
	0	0	NR 0	NU 0	SL 0	ST 0	SR 0	SU 0	EL 0	1 ET 0	ER 0	EU 0	WL 0	1 WT 0	0 WR 0	WU 0	0
4:15 PM 4:30 PM 4:45 PM	0	0	NR 0 0	NU 0 0	SL 0 0	ST 0 0	SR 0 0	SU 0 0	EL 0 0	1 ET 0 0	ER 0 0	0 0	WL 0 0	1 WT 0 0	0 WR 0 0	0 0	0
4:15 PM 4:30 PM 4:45 PM 5:00 PM	0 0 0	0 0 0 0	0 0 0	0 0 0	SL 0 0 0 0	ST 0 0 0	SR 0 0 0	0 0 0	0 0 0	1 ET 0 0 0	ER 0 0 0 0 0 0 0 0	0 0 0	0 0 0	1 WT 0 0 0	0 WR 0 0 0	0 0 0	0 0 0 0
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	0 0 0 0	0 0 0 0	NR 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0	ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0	1 ET 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	WL 0 0 0 0 0	1 WT 0 0 0 0 0	0 WR 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	0 0 0 0 0	0 0 0 0 0	NR 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0	ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0	1 ET 0 0 0 0 0 0	ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0	0 WR 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	0 0 0 0	0 0 0 0	NR 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0	ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0	1 ET 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	WL 0 0 0 0 0	1 WT 0 0 0 0 0	0 WR 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	0 0 0 0 0 0 0	0 0 0 0 0 0 0	NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 NR	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ST 0 0 0 0 0 0 0 0 0 0 0 0 ST	SR 0 0 0 0 0 0 0 0 0 0 0 SR	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 SU	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0	ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	0 0 0 0 0 0	0 0 0 0 0 0 0	NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0	ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0 0	0 WR 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES : APPROACH %'s:	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	NR 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ST 0 0 0 0 0 0 0 0 0 0 0 0 ST	SR 0 0 0 0 0 0 0 0 0 0 0 SR	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 SU	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0	ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 TOTAL
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:35 PM 5:45 PM  TOTAL VOLUMES: APPROACH %'s: PEAK HR:	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	NR 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 SL 0	ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SR 0 0 0 0 0 0 0 0 0 0 SR 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0	ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 TOTAL
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:345 PM  TOTAL VOLUMES: APPROACH %'s: PEAK HR: PEAK HR VOL:	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0	ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 TOTAL
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:35 PM 5:45 PM  TOTAL VOLUMES: APPROACH %'s: PEAK HR:	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	NR 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 SL 0	ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SR 0 0 0 0 0 0 0 0 0 0 SR 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0 0	ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 TOTAL

# National Data & Surveying Services Intersection Turning

Location: Sierra Pacific Industries Dwy & La Grange Rd/CR J59

Date: 8/29/2023

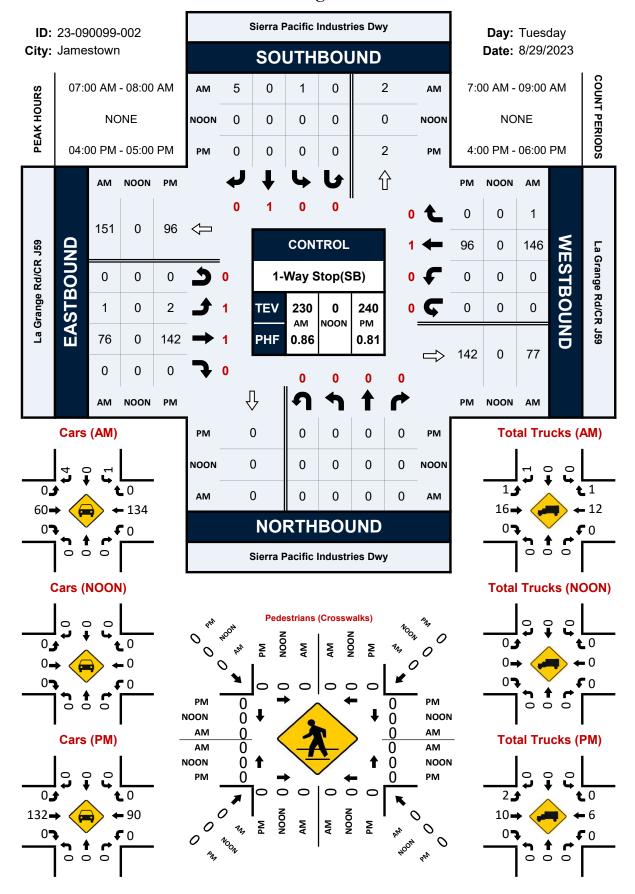
**Data - Pedestrians (Crosswalks)** 

NS/EW Streets:		ic Industries wy		fic Industries wy	La Grange	Rd/CR J59	La Grange	Rd/CR J59	
ANA	NORT	TH LEG	SOUT	TH LEG	EAST	LEG	WEST	Γ LEG	
AM	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
7:00 AM	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	0	0	0
PEAK HR:	07:00 AM	- 08:00 AM							TOTAL
PEAK HR VOL : PEAK HR FACTOR :	0	0	0	0	0	0	0	0	0

DNA	NORT	H LEG	SOUT	'H LEG	EAST	LEG	WEST	Γ LEG	
PM	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES :	0	0	0	0	0	0	0	0	0
APPROACH %'s:									
PEAK HR :	04:00 PM	- 05:00 PM							TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR :									

### Sierra Pacific Industries Dwy & La Grange Rd/CR J59

### **Peak Hour Turning Movement Count**



Location: La Grange Rd/CR J59 & Yosemite Blvd/SR 132 City: La Grange Control: 4-Way Stop

Control: 4	r-way stop	,						Data -	Total					Date.	5/29/2023		
П								Data -									
NS/EW Streets:		La Grange I	Rd/CR J59			La Grange I	Rd/CR J59		)	Yosemite Bl	vd/SR 132		`	Yosemite Bl	vd/SR 132		
		NORTH	BOUND			SOUTH	BOUND			EASTE	BOUND			WESTE	BOUND		
AM	0	1	0	0	0	1	0	0	0	1	1	0	0	1	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	11	2	0	0	6	8	0	3	4	0	0	3	29	1	0	67
7:15 AM	3	25	3	0	0	15	4	0	4	1	2	0	1	21	0	0	79
7:30 AM	0	15	2	0	0	13	4	0	3	6	1	0	1	17	0	0	62
7:45 AM	2	16	3	0	0	16	4	0	4	5	0	0	4	27	1	0	82
8:00 AM	3	11	2	0	1	12	1	0	6	4	0	0	3	9	1	0	53
8:15 AM	0	9	1	0	1	14	4	0	11	6	2	0	1	9	0	0	58
8:30 AM	0	18	2	0	1 0	15	3 5	0	1 5	7	1	0	0	13	0	0	61
8:45 AM	0	10	1	0	U	16	5	0	5	9	1	0	0	13	0	0	60
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	8	115	16	0	3	107	33	0	37	42	7	0	13	138	3	0	522
APPROACH %'s:	5.76%	82.73%	11.51%	0.00%	2.10%	74.83%	23.08%	0.00%	43.02%	48.84%	8.14%	0.00%	8.44%	89.61%	1.95%	0.00%	JLL
PEAK HR:		07:00 AM -	08:00 AM														TOTAL
PEAK HR VOL :	5	67	10	0	0	50	20	0	14	16	3	0	9	94	2	0	290
PEAK HR FACTOR :	0.417	0.670	0.833	0.000	0.000	0.781	0.625	0.000	0.875	0.667	0.375	0.000	0.563	0.810	0.500	0.000	0.884
		0.6	61			0.8	75			0.8	25			0.79	95		0.004
D0.4			BOUND				BOUND				BOUND			WESTE			
PM	0	1	0	0	0	1	0	0	0	1	1	0	0	1	1	0	
4 00 014	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	17	0	0	1	14	1	0	9	18	5	0	1	8	0	0	74
4:15 PM 4:30 PM	1 2	10 23	3 0	0	0 0	24 25	7 8	0	5	23 15	3	0	4 0	5 11	3 0	0	88
4:30 PM 4:45 PM	2	23 7	3	1	0	25	6	0	7	15 25	3	0	2	13	0	0	87 90
5:00 PM	0	11	2	1	0	12	6	0	7	23	1	0	1	12	0	0	76
5:15 PM	2	12	2	0	1	13	4	0	6	19	4	0	3	3	2	0	71
5:30 PM	0	15	3	0	0	19	3	0	7	26	0	0	0	8	0	0	81
5:45 PM	0	9	2	0	0	22	3	0	8	19	1	0	1	13	1	0	79
3. 13 111	•		-	٠	·	22	,	•		13	-	٠	•	13	-	•	,,
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	6	104	15	2	2	151	38	0	49	168	20	0	12	73	6	0	646
APPROACH %'s:	4.72%	81.89%	11.81%	1.57%	1.05%	79.06%	19.90%	0.00%	20.68%	70.89%	8.44%	0.00%	13.19%	80.22%	6.59%	0.00%	
PEAK HR:		04:15 PM -				·	·			<u> </u>		,		·	·		TOTAL
PEAK HR VOL :	4	51	8	2	0	83	27	0	19	86	10	0	7	41	3	0	341
PEAK HR FACTOR :	0.500	0.554	0.667	0.500	0.000	0.830	0.844	0.000	0.679	0.860	0.833	0.000	0.438	0.788	0.250	0.000	0.947
		0.6	50			0.8	33			0.8	21			0.8	50		5.5 17

Location: La Grange Rd/CR J59 & Yosemite Blvd/SR 132 City: La Grange Control: 4-Way Stop

Data - Cars

_								Data	- Cars								
NS/EW Streets:		La Grange F	Rd/CR J59			La Grange F	Rd/CR J59		,	osemite Blv	/d/SR 132		١	Yosemite Blv	d/SR 132		
		NORTH	BOUND			SOUTH	BOUND			EASTB	OUND			WESTB	OUND		
AM	0	1	0	0	0	1	0	0	0	1	1	0	0	1	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	10	1	0	0	6	8	0	3	3	0	0	3	28	1	0	63
7:15 AM	3	23	3	0	0	14	4	0	4	1	1	0	1	21	0	0	75
7:30 AM	0	13	2	0	0	11	4	0	3	5	1	0	1	16	0	0	56
7:45 AM	2	15	3	0	0	8	4	0	4	5	0	0	4	26	1	0	72
8:00 AM	3	6	2	0	1	11	0	0	3	4	0	0	3	9	1	0	43
8:15 AM	0	6	1	0	1	12	3	0	9	4	2	0	1	9	0	0	48
8:30 AM	0	15	2	0	1	14	3	0	0	6	1	0	0	12	0	0	54
8:45 AM	0	8	1	0	0	13	3	0	5	9	0	0	0	13	0	0	52
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	8	96	15	0	3	89	29	0	31	37	5	0	13	134	3	0	463
APPROACH %'s:	6.72%	80.67%	12.61%	0.00%	2.48%	73.55%	23.97%	0.00%	42.47%	50.68%	6.85%	0.00%	8.67%	89.33%	2.00%	0.00%	
PEAK HR :		07:00 AM -				20	20							0.4			TOTAL
PEAK HR VOL :	5	61	9	0	0	39	20	0	14	14	2 0.500	0	9	91	2	0	266
PEAK HR FACTOR :	0.417	0.663	0.750	0.000	0.000	0.696	0.625	0.000	0.875	0.700 0.83		0.000	0.563	0.813 0.79	0.500	0.000	0.887
		0.0	7/			0.0.	19			0.03	13			0.75	7		
		NORTH	BOUND			SOUTH	BOUND			EASTB	OUND			WESTB	OUND		
PM	0	1	0	0	0	1	0	0	0	1	1	0	0	1	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	17	0	0	1	14	1	0	9	18	4	0	1	8	0	0	73
4:15 PM	1	10	3	0	0	23	6	0	5	23	3	0	4	5	3	0	86
4:30 PM	2	20	0	0	0	23	8	0	0	13	3	0	0	11	0	0	80
4:45 PM	1	6	3	1	0	21	5	0	7	25	3	0	2	10	0	0	84
5:00 PM	0	11	2	0	0	12	6	0	6	22	1	0	1	12	0	0	73
5:15 PM	2	12	2	0	1	12	3	0	6	18	4	0	3	3	2	0	68
5:30 PM	0	15	3	0	0	16	3	0	7	26	0	0	0	8	0	0	78
5:45 PM	0	7	2	0	0	22	3	0	8	19	1	0	1	13	1	0	77
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	6	98	15	1	2	143	35	0	48	164	19	0	12	70	6	0	619
APPROACH %'s :	5.00%	81.67%	12.50%	0.83%	1.11%	79.44%	19.44%	0.00%	20.78%	71.00%	8.23%	0.00%	13.64%	79.55%	6.82%	0.00%	TOTAL
PEAK HR :			05:15 PM			70	25		10	02	10		_	20	2		TOTAL
PEAK HR VOL :	4	47 0.588	8	1	0	79 0.859	25 0.781	0	18	83 0.830	10 0.833	0	7	38 0.792	3	0	323
PEAK HR FACTOR :	0.500	0.588	0.667	0.250	0.000	0.859		0.000	0.643	0.830		0.000	0.438	0.792	0.250	0.000	0.939

Location: La Grange Rd/CR J59 & Yosemite Blvd/SR 132 City: La Grange Control: 4-Way Stop

Data - 2axle

									2axle								
NS/EW Streets:		La Grange F	Rd/CR J59			La Grange	Rd/CR J59		,	osemite Bl	vd/SR 132			Yosemite Blv	vd/SR 132		
		NORTH	BOUND			SOUTH	IBOUND			EASTE	OUND			WESTE	OUND		
AM	0	1	0	0	0	1	0	0	0	1	1	0	0	1	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	0	0	0	0	0	0	0	0	1	0	0	0	1	0	0	2
7:15 AM	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
7:30 AM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	1
7:45 AM	0	0	0	0	0	1	0	0	0	0	0	0	0	1	0	0	2
8:00 AM	0	1	0	0	0	0	0	0	3	0	0	0	0	0	0	0	4
8:15 AM	0	1	0	0	0	0	0	0	0	1	0	0	0	0	0	0	2
8:30 AM	0	2	0	0	0	0	0	0	0	1	0	0	0	1	0	0	4
8:45 AM	0	1	0	0	0	0	0	0	0	0	1	0	0	0	0	0	2
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	0	6	0	0	0	1	0	0	3	4	1	0	0	3	0	0	18
APPROACH %'s:	0.00%	100.00%	0.00%	0.00%	0.00%	100.00%	0.00%	0.00%	37.50%	50.00%	12.50%	0.00%	0.00%	100.00%	0.00%	0.00%	
PEAK HR :		07:00 AM -	08:00 AM														TOTAL
PEAK HR VOL :	0	1	0	0	0	1	0	0	0	2	0	0	0	2	0	0	6
PEAK HR FACTOR :	0.000	0.250	0.000	0.000	0.000	0.250	0.000	0.000	0.000	0.500	0.000	0.000	0.000	0.500	0.000	0.000	0.750
		0.25	50			0.2	50			0.5	00			0.50	00		01750
DNA		NORTH					IBOUND			EASTE				WESTE			
PM	0	1	0	0	0	1	0	0	0	1	1	0	0				
4.00 PM	NL					CT	CD	CII		CT.	ED	EU.		1	1	0	TOTAL
		NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	0	0	0	0	ST 0	0	0	EL 0	0	0	0	WL 0	WT 0	WR 0	WU 0	0
4:15 PM	0	0	0 0	0	0	0 1	0 1	0	0 0		0	0	WL 0 0	WT 0 0	WR 0 0	0 0	0 2
4:15 PM 4:30 PM	0	0 0 3	0 0 0	0 0 0	0 0 0		0	0 0 0	0 0 0	0 0 1	0 0 0	0 0 0	0 0 0	WT 0 0 0	0 0 0	0 0 0	0 2 5
4:15 PM 4:30 PM 4:45 PM	0 0 0	0 0 3 1	0 0	0 0 0	0 0 0	0 1	0 1 0 1	0 0 0	EL 0 0 0 0	0 0 1 0	0 0 0 0	0 0 0 0	WL 0 0	WT 0 0	WR 0 0 0 0	0 0 0 0	0 2 5 6
4:15 PM 4:30 PM 4:45 PM 5:00 PM	0 0 0	0 0 3 1	0 0 0	0 0 0 0	0 0 0 0	0 1 1 1	0 1	0 0 0 0	EL 0 0 0 0 0 0 0 0 0	0 0 1 0	0 0 0	0 0 0 0	WL 0 0 0 0	WT 0 0 0 0 3	0 0 0	0 0 0	0 2 5 6
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	0 0 0 0	0 0 3 1 0	0 0 0 0	0 0 0 0	0 0 0 0 0	0 1 1 1 0 1	0 1 0 1	0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 1 0	0 0 0 0	0 0 0 0 0	WL 0 0 0 0	WT 0 0 0 0 3 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 2 5 6 0 2
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	0 0 0	0 0 3 1	0 0 0 0 0	0 0 0 0	0 0 0 0	0 1 1 1 0	0 1 0 1 0	0 0 0 0	EL 0 0 0 0 0 0 0 0 0	0 0 1 0 0	0 0 0 0 0	0 0 0 0	WL 0 0 0 0 0	WT 0 0 0 0 3 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 2 5 6 0 2 2
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	0 0 0 0 0 0	0 0 3 1 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 1 1 1 0 1 2	0 1 0 1 0 1 0	0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 1 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	WL 0 0 0 0 0 0	WT 0 0 0 0 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 2 5 6 0 2 2
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	0 0 0 0 0 0 0	0 0 3 1 0 0 0 2	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 1 1 1 0 1 2 0	0 1 0 1 0 1 0 0 SR	0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 1 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WT 0 0 0 0 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 2 5 6 0 2 2 2
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	0 0 0 0 0 0 0	0 0 3 1 0 0 0 2	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 1 1 1 0 1 2 0 ST 6	0 1 0 1 0 1 0 0 5 SR 3	0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 1 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WT 0 0 0 0 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 2 5 6 0 2 2
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES : APPROACH %'s:	0 0 0 0 0 0 0 0 0 0	0 0 3 1 0 0 0 2 NT 6 100.00%	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 1 1 1 0 1 2 0	0 1 0 1 0 1 0 0 SR	0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 1 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WT 0 0 0 0 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 2 5 6 0 2 2 2 2 TOTAL
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM  TOTAL VOLUMES: APPROACH %'s: PEAK HR:	0 0 0 0 0 0 0 0 0 0 0 0	0 0 3 1 0 0 0 2 NT 6 100.00%	0 0 0 0 0 0 0 0 0 NR 0 0.00%	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 SL 0	0 1 1 1 0 1 2 0 ST 6 66.67%	0 1 0 1 0 1 0 0 SR 3 33.33%	0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 1 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WT 0 0 0 0 3 3 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 2 5 6 0 2 2 2 2 TOTAL 19
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:35 PM 5:45 PM  TOTAL VOLUMES: APPROACH %'s: PEAK HR: PEAK HR VOL:	0 0 0 0 0 0 0 0 0 0 0 0	0 0 3 1 0 0 0 2 NT 6 100.00%	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 1 1 1 0 1 2 0 ST 6 66.67%	0 1 0 1 0 1 0 0 0 SR 3 33.33%	0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 1 0 0 0 0 0 0 0 ET 1 100.00%	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WT 0 0 0 0 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 2 5 6 0 2 2 2 2 TOTAL
4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM  TOTAL VOLUMES: APPROACH %'s: PEAK HR:	0 0 0 0 0 0 0 0 0 0 0 0	0 0 3 1 0 0 0 2 NT 6 100.00%	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 SL 0	0 1 1 1 0 1 2 0 ST 6 66.67%	0 1 0 1 0 1 0 0 0 SR 3 33.33%	0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 1 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WT 0 0 0 0 3 3 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 2 5 6 0 2 2 2 2 TOTAL 19

Location: La Grange Rd/CR J59 & Yosemite Blvd/SR 132 City: La Grange Control: 4-Way Stop

_								Data -	3axle								_
NS/EW Streets:		La Grange	Rd/CR J59			La Grange F	Rd/CR J59			Yosemite Bl	vd/SR 132			Yosemite E	llvd/SR 132		
		NORT	HBOUND			SOUTH	BOUND			EASTB	OUND			WEST	BOUND		
AM	0	1	0	0	0	1	0	0	0	1	1	0	0	1	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	1	1	0	0	0	0	0	0	2
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	1
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	0	0	0	0	0	1	0	0	1	1	0	0	0	0	0	0	3
APPROACH %'s:					0.00%	100.00%	0.00%	0.00%	50.00%	50.00%	0.00%	0.00%					
PEAK HR :		07:00 AM	- 08:00 AM														TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
		NORT	HBOUND			SOUTH	BOUND			FASTB	OUND			WEST	BOUND		
PM	0	1	0	0	0	1	0	0	0	1	1	0	0	1	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	1
5:15 PM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	1
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	0	0	0	0	0	0	0	0	0	2	0	0	0	0	0	0	2
APPROACH %'s:									0.00%	100.00%	0.00%	0.00%					
PEAK HR:			- 05:15 PM					_			_	_					TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	1
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.250	0.000 50	0.000	0.000	0.000	0.000	0.000	0.250

Location: La Grange Rd/CR J59 & Yosemite Blvd/SR 132 City: La Grange Control: 4-Way Stop

Data - 4ayle

_								Data -	4axle								
NS/EW Streets:		La Grange	Rd/CR J59			La Grange l	Rd/CR J59		١	osemite Bl	vd/SR 132			Yosemite Bl	vd/SR 132		
		NORTH	BOUND			SOUTH	BOUND			EASTE	OUND			WESTE	BOUND		
AM	0	1	0	0	0	1	0	0	0	1	1	0	0	1	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	2
7:15 AM	0	1	0	0	0	1	0	0	0	0	1	0	0	0	0	0	3
7:30 AM	0	2	0	0	0	2	0	0	0	0	0	0	0	1	0	0	5
7:45 AM	0	1	0	0	0	7	0	0	0	0	0	0	0	0	0	0	8
8:00 AM	0	4	0	0	0	1	1	0	0	0	0	0	0	0	0	0	6
8:15 AM	0	2	0	0	0	2	1	0	1	0	0	0	0	0	0	0	6
8:30 AM	0	1	0	0	0	1	0	0	1	0	0	0	0	0	0	0	3
8:45 AM	0	1	0	0	0	2	2	0	0	0	0	0	0	0	0	0	5
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	0	13	1	0	0	16	4	0	2	0	1	0	0	1	0	0	38
APPROACH %'s:	0.00%	92.86%	7.14%	0.00%	0.00%	80.00%	20.00%	0.00%	66.67%	0.00%	33.33%	0.00%	0.00%	100.00%	0.00%	0.00%	
PEAK HR:		07:00 AM -	08:00 AM														TOTAL
PEAK HR VOL :	0	5	1	0	0	10	0	0	0	0	1	0	0	1	0	0	18
PEAK HR FACTOR :	0.000	0.625	0.250	0.000	0.000	0.357	0.000	0.000	0.000	0.000	0.250	0.000	0.000	0.250	0.000	0.000	0.563
		0.7	50			0.3	57			0.2	50			0.2	50		0.505
DNA			BOUND			SOUTH				EASTE				WESTE			
PM	0	1	0	0	0	1	0	0	0	1	1	0	0	1	1	0	TOT41
4.00.014	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	1
4:15 PM 4:30 PM	0	0	0	0	0	-	0	0	0	0	0	0	0	0	•	0	0
4:30 PM 4:45 PM	0	0	0	0	0	1 0	0	0	0	1 0	0	0	0	0	0	0	2
5:00 PM	0	0	0	1	0	0	0	0	1	0	0	0	0	0	0	0	2
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	1
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3.43 FM	U			_	U	U		_	U			_	U			_	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	0	0	0	1	0	2	0	0	1	1	1	0	0	0	0	0	6
APPROACH %'s:	0.00%	0.00%	0.00%	100.00%	0.00%	100.00%	0.00%	0.00%	33.33%	33.33%	33.33%	0.00%					
PEAK HR :		04:15 PM -															TOTAL
PEAK HR VOL :	0	0	0	1	0	1	0	0	1	1	0	0	0	0	0	0	4
PEAK HR FACTOR :	0.000	0.000	0.000	0.250	0.000	0.250	0.000	0.000	0.250	0.250	0.000	0.000	0.000	0.000	0.000	0.000	0.500
		0.2	50			0.2	50			0.5	JU						

Location: La Grange Rd/CR J59 & Yosemite Blvd/SR 132 City: La Grange Control: 4-Way Stop

_								Data -	Bikes								_
NS/EW Streets:		La Grange	Rd/CR J59			La Grange	Rd/CR J59			Yosemite E	Blvd/SR 132			Yosemite B	Blvd/SR 132		
		NORTH	HBOUND			SOUTI	HBOUND			EAST	BOUND			WEST	BOUND		
AM	0	1	0	0	0	1	0	0	0	1	1	0	0	1	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
APPROACH %'s:																	
PEAK HR:			- 08:00 AM				_	_	_	_	_	_	_	_	_	_	TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
																	l
		NORTI	HBOUND			SOUTI	HBOUND			EAST	BOUND			WEST	BOUND		
PM	0	1	0	0	0	1	0	0	0	1	1						
	NL	NT	NR									0	0	1	1	0	
4:00 PM	0			NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
		0	0	0	0	0	0	0	EL 0	ET 0	ER 0	EU 0	WL 0	WT 0	WR 0	WU 0	0
4:15 PM	Ō	Ō	0	0	0	0	0	0	0 0	0 0	ER 0 0	0 0	WL 0 0	WT 0 0	WR 0 0	0 0	0
4:30 PM	0	0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	WT 0 0 0	0 0 0	0 0 0	0 0 0
4:30 PM 4:45 PM	0 0 0	0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	ER 0 0 0 0	0 0 0 0	WL 0 0 0 0	WT 0 0 0 0	WR 0 0 0 0	0 0 0 0	0 0 0
4:30 PM 4:45 PM 5:00 PM	0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0 0	0 0 0 0 0	ER 0 0 0 0 0 0 0 0	0 0 0 0 0	WL 0 0 0 0	WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0
4:30 PM 4:45 PM 5:00 PM 5:15 PM	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0	WL 0 0 0 0 0	WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0
4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	0 0 0 0	0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0	WL 0 0 0 0 0 0	WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0
4:30 PM 4:45 PM 5:00 PM 5:15 PM	0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0
4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0
4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0
4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s:	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 TOTAL
4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:31 PM 5:32 PM 5:45 PM  TOTAL VOLUMES: APPROACH %'s: PEAK HR:	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 SR	0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 TOTAL
4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:33 PM 5:345 PM  TOTAL VOLUMES: APPROACH %'s: PEAK HR: PEAK HR VOL:	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 SR 0	0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 TOTAL
4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:31 PM 5:32 PM 5:45 PM  TOTAL VOLUMES: APPROACH %'s: PEAK HR:	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 SR	0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ET 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ER 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 TOTAL

# National Data & Surveying Services Intersection Turning

Location: La Grange Rd/CR J59 & Yosemite Blvd/SR 132

Date: 8/29/2023

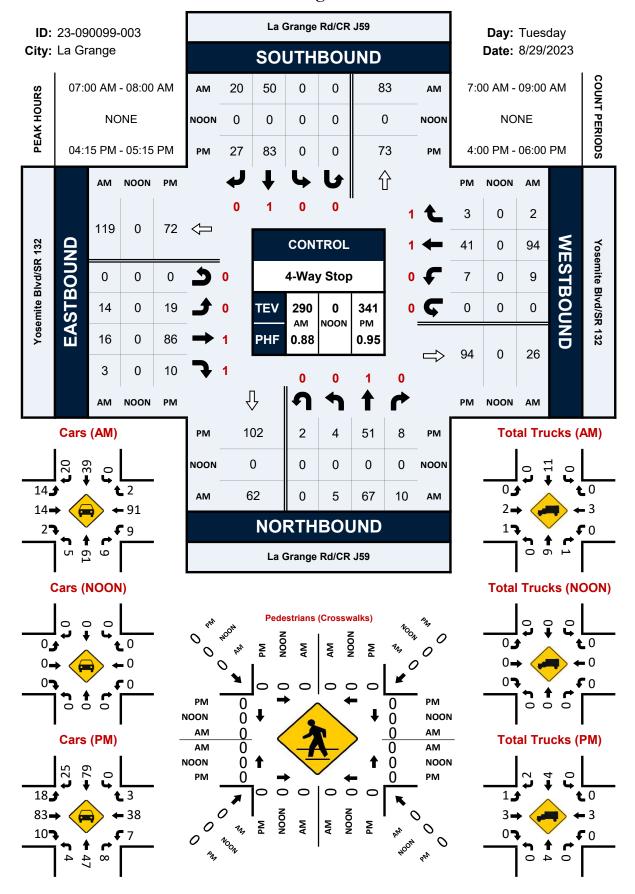
#### **Data - Pedestrians (Crosswalks)**

NS/EW Streets:	La Grange	Rd/CR J59	La Grange	Rd/CR J59	Yosemite B	Blvd/SR 132	Yosemite B	Blvd/SR 132	
AM	NORT	'H LEG	SOUT	TH LEG	EAST	LEG	WES	T LEG	
Alvi	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
7:00 AM	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES:	0	0	0	0	0	0	0	0	0
APPROACH %'s:									
PEAK HR:	07:00 AM	- 08:00 AM							TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR :									

PM	NORT	TH LEG	SOUT	TH LEG	EAST	LEG	WEST	Γ LEG	
PIVI	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	0	0	0
PEAK HR :	04:15 PM	- 05:15 PM							TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR :									

#### La Grange Rd/CR J59 & Yosemite Blvd/SR 132

#### **Peak Hour Turning Movement Count**



## ${\tt National\ Data\ \&\ Surveying\ Services} \\ Intersection\ Turning\ Movement\ Count$

Location: Red Hill Rd & Montezuma Rd/SR 49 City: Chinese Camp Control: 1-Way Stop(NB)

Control	I way stop	(110)												Ducc.	0/23/2023		
_								Data ·	- Total								_
NS/EW Streets:		Red H	lill Rd			Red I	Hill Rd			Montezuma	Rd/SR 49			Montezuma	Rd/SR 49		
		NORTH	HBOUND			SOLITI	HBOUND			FASTE	BOUND			WESTE	ROLIND		
AM	0	1	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
,	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	3	0	0	0	0	0	0	0	0	29	2	0	0	17	0	0	51
7:15 AM	2	0	1	0	0	0	0	0	0	14	0	0	0	18	0	0	35
7:30 AM	2	0	0	0	0	0	0	0	0	26	2	0	0	22	0	0	52
7:45 AM	4	0	0	0	0	0	0	0	0	19	1	0	0	19	0	0	43
8:00 AM	3	0	1	0	0	0	0	0	0	28	6	0	0	13	0	0	51
8:15 AM	2	0	1	0	0	0	0	0	0	37	6	0	0	20	0	0	66
8:30 AM	4	0	1	0	0	0	0	0	0	29	1	0	0	22	0	0	57
8:45 AM	1	0	1	0	0	0	0	0	0	38	3	0	0	20	0	0	63
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	21	0	5	0	0	0	0	0	0	220	21	0	0	151	0	0	418
APPROACH %'s:	80.77%	0.00%	19.23%	0.00%					0.00%	91.29%	8.71%	0.00%	0.00%	100.00%	0.00%	0.00%	TOTAL
PEAK HR :		- MA 00:80		0	_		•	0	_	122	16			75	0		TOTAL
PEAK HR VOL :	10 0.625	0 0.000	4 1.000	0.000	0.000	0.000	0.000	0 0.000	0.000	132 0.868	16 0.667	0.000	0.000	75 0.852	0.000	0.000	237
PEAK HR FACTOR :	0.625	0.000		0.000	0.000	0.000	0.000	0.000	0.000	0.868		0.000	0.000	0.852		0.000	0.898
		0.7	00							0.0	00			0.0	J2		
		NORTH	HBOUND			SOLIT	HBOUND			EASTE	ROLIND			WESTE	ROLIND		
PM	0	1	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	6	0	1	0	0	0	0	0	0	26	9	0	1	39	0	0	82
4:15 PM	1	0	2	0	0	0	0	0	0	19	5	0	2	34	0	1	64
4:30 PM	2	0	0	0	0	0	0	0	0	18	5	0	2	65	0	0	92
4:45 PM	2	0	0	0	0	0	0	0	0	20	1	0	0	35	0	0	58
5:00 PM	2	0	0	0	0	0	0	0	0	29	2	0	0	45	0	0	78
5:15 PM	3	0	2	0	0	0	0	0	0	30	5	0	1	29	0	0	70
5:30 PM	1	0	0	0	0	0	0	0	0	15	6	0	2	38	0	0	62
5:45 PM	1	0	2	0	0	0	0	0	0	26	4	0	0	26	0	0	59
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	18	0	7	0	0	0	0	0	0	183	37	0	8	311	0	1	565
APPROACH %'s:	72.00%	0.00%	28.00%	0.00%					0.00%	83.18%	16.82%	0.00%	2.50%	97.19%	0.00%	0.31%	TOTAL
PEAK HR :		04:30 PM -		0				0		07			2	174		0	TOTAL
PEAK HR VOL :	9	0	2	0	0	0	0	0	0	97	13	0	3	174	0	0	298
PEAK HR FACTOR :	0.750	0.000	0.250	0.000	0.000	0.000	0.000	0.000	0.000	0.808	0.650	0.000	0.375	0.669	0.000	0.000	0.810
		0.5	טכנ							0.7	OD			0.6	UC		

## ${\tt National\ Data\ \&\ Surveying\ Services} \\ Intersection\ Turning\ Movement\ Count$

Location: Red Hill Rd & Montezuma Rd/SR 49 City: Chinese Camp Control: 1-Way Stop(NB)

D	a	ta	-	Ca	rc

N	NS/EW Streets:		Red H	ill Rd			Red I	Hill Rd			Montezuma	Rd/SR 49			Montezuma	Rd/SR 49		
			NORTH	BOUND			SOUTI	HBOUND			EASTE	BOUND			WESTE	BOUND		
	AM	0	1	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
		NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
	7:00 AM	2	0	0	0	0	0	0	0	0	21	0	0	0	16	0	0	39
	7:15 AM	2	0	0	0	0	0	0	0	0	10	0	0	0	18	0	0	30
	7:30 AM	1	0	0	0	0	0	0	0	0	22	2	0	0	21	0	0	46
	7:45 AM	4	0	0	0	0	0	0	0	0	17	1	0	0	17	0	0	39
	8:00 AM	3	0	0	0	0	0	0	0	0	22	5	0	0	12	0	0	42
	8:15 AM	2	0	1	0	0	0	0	0	0	30	5	0	0	16	0	0	54
	8:30 AM	3	0	1	0	0	0	0	0	0	23	1	0	0	18	0	0	46
	8:45 AM	1	0	1	0	0	0	0	0	0	31	3	0	0	18	0	0	54
		NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TO	OTAL VOLUMES :	18	0	3	0	0	0	0	0	0	176	17	0	0	136	0	0	350
А	APPROACH %'s:	85.71%	0.00%	14.29%	0.00%					0.00%	91.19%	8.81%	0.00%	0.00%	100.00%	0.00%	0.00%	
	PEAK HR:		- MA 00:80	09:00 AM														TOTAL
	PEAK HR VOL:	9	0	3	0	0	0	0	0	0	106	14	0	0	64	0	0	196
PE/	AK HR FACTOR :	0.750	0.000	0.750	0.000	0.000	0.000	0.000	0.000	0.000	0.855	0.700	0.000	0.000	0.889	0.000	0.000	0.907
			0.7	50							0.8	57			0.88	39		0.907
			NORTH	BOUND			SOUTI	HBOUND			EASTE	BOUND			WESTE			
	PM	0	1	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
		NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
	4:00 PM	6	0	1	0	0	0	0	0	0	26	8	0	1	38	0	0	80
	4:15 PM	1	0	2	0	0	0	0	0	0	19	4	0	2	32	0	1	61
	4:30 PM	2	0	0	0	0	0	0	0	0	17	5	0	1	63	0	0	88
	4:45 PM	1	0	0	0	0	0	0	0	0	20	1	0	0	32	0	0	54
	5:00 PM	2	0	0	0	0	0	0	0	0	28	2	0	0	40	0	0	72
	5:15 PM	3	0	2	0	0	0	0	0	0	30	5	0	1	28	0	0	69
	5:30 PM	1	0	0	0	0	0	0	0	0	15	6	0	2	37	0	0	61
	5:45 PM	1	0	2	0	0	0	0	0	0	26	4	0	0	24	0	0	57
			· ·															
		NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
то	OTAL VOLUMES :	NL 17		NR 7	NU 0	SL 0	ST 0	SR 0	SU 0	EL 0	ET 181	ER 35	EU 0	WL 7	WT 294	WR 0	WU 1	TOTAL 542
	OTAL VOLUMES :		NT															
		17 70.83%	NT 0	7 29.17%	0					0	181	35	0	7	294	0	1	
	APPROACH %'s:	17 70.83%	NT 0 0.00%	7 29.17% <b>05:30 PM</b> 2	0 0.00%					0	181 83.80% 95	35 16.20%	0	7	294 97.35% 163	0 0.00%	1	542
A	APPROACH %'s : PEAK HR :	17 70.83%	NT 0 0.00% <b>04:30 PM</b> -	7 29.17% <b>05:30 PM</b> 2 0.250	0.00%	0	0	0	0	0 0.00%	181 83.80%	35 16.20% 13 0.650	0.00%	7 2.32%	294 97.35%	0 0.00% 0 0.000	1 0.33%	542 TOTAL

Location: Red Hill Rd & Montezuma Rd/SR 49 City: Chinese Camp Control: 1-Way Stop(NB)

Project ID: 23-090099-004

TOJECT ID.	23-030033-
Date:	8/29/2023

								Data -	2axle								
NS/EW Streets:		Red H	lill Rd			Red I	Hill Rd			Montezuma	Rd/SR 49			Montezuma	Rd/SR 49		
		NORTH	BOUND			SOUTI	HBOUND			EASTE	BOUND			WESTE	BOUND		
AM	0	1	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	1	0	0	0	0	0	0	0	0	2	2	0	0	1	0	0	6
7:15 AM	0	0	1	0	0	0	0	0	0	2	0	0	0	0	0	0	3
7:30 AM	1 0	0	0	0	0	0	0	0	0	2	0	0	0	0	0	0	3
7:45 AM 8:00 AM	0	0	1	0	0	0	0	0	0	3	1	0	0	- 0	0	0	6
8:15 AM	0	0	0	0	0	0	0	0	0	4	1	0	0	1	0	0	6
8:30 AM	1	0	0	0	0	0	0	0	0	1	0	0	0	2	0	0	4
8:45 AM	0	0	0	0	0	0	0	0	0	3	0	0	0	1	0	0	4
PIA CF.0	U	U	U	U	0	U	U	U	0	3	U	U	U	1	U	U	7
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	3	0	2	0	0	0	0	0	0	19	4	0	0	6	0	0	34
APPROACH %'s:	60.00%	0.00%	40.00%	0.00%					0.00%	82.61%	17.39%	0.00%	0.00%	100.00%	0.00%	0.00%	
PEAK HR:		08:00 AM -	09:00 AM														TOTAL
PEAK HR VOL :	1	0	1	0	0	0	0	0	0	11	2	0	0	5	0	0	20
PEAK HR FACTOR :	0.250	0.000	0.250	0.000	0.000	0.000	0.000	0.000	0.000	0.688	0.500	0.000	0.000	0.625	0.000	0.000	0.833
		0.5	00							0.6	50			0.6	25		
		NORTH	BOUND			SOUT	HBOUND			EASTE	BOUND			WESTE	BOUND		
PM	0	1	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	1	0	0	2	0	0	3
4:30 PM	0	0	0	0	0	0	0	0	0	1	0	0	1	2	0	0	4
4:45 PM	1	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	2
5:00 PM	0	0	0	0	0	0	0	0	0	1	0	0	0	3	0	0	4
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0	0	2
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES:	1	0	0	0	0	0	0	0	0	2	1	0	1	12	0	0	17
APPROACH %'s:	100.00%	0.00%	0.00%	0.00%					0.00%	66.67%	33.33%	0.00%	7.69%	92.31%	0.00%	0.00%	
PEAK HR:		04:30 PM -	05:30 PM														TOTAL
PEAK HR VOL :	1	0	0	0	0	0	0	0	0	2	0	0	1	7	0	0	11
PEAK HR FACTOR:	0.250	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.500	0.000	0.000	0.250	0.583	0.000	0.000	0.688
		0.2	50							0.5	00			0.6	67		0.000

Location: Red Hill Rd & Montezuma Rd/SR 49 City: Chinese Camp Control: 1-Way Stop(NB)

Data - 3axle

_								Data .	· saxie								
NS/EW Streets:		Red I	Hill Rd			Red I	Hill Rd			Montezuma	Rd/SR 49			Montezuma	Rd/SR 49		
		NORT	HBOUND			SOUTI	HBOUND			EASTE	BOUND			WESTE	OUND		
AM	0	1	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTA
7:00 AM	0	0	0	0	0	0	0	0	0	4	0	0	0	0	0	0	4
7:15 AM	0	0	0	0	0	0	0	0	0	2	0	0	0	0	0	0	2
7:30 AM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	1
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	2	0	0	0	0	0	0	2
8:15 AM	0	0	0	0	0	0	0	0	0	2	0	0	0	1	0	0	3
8:30 AM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	1
8:45 AM	0	0	0	0	0	0	0	0	0	2	0	0	0	1	0	0	3
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TO
TOTAL VOLUMES:	0	0	0	0	0	0	0	0	0	14	0	0	0	2	0	0	1
APPROACH %'s:									0.00%	100.00%	0.00%	0.00%	0.00%	100.00%	0.00%	0.00%	
PEAK HR :			- 09:00 AM														TO
PEAK HR VOL :	0	0	0	0	0	0	0	0	0	7	0	0	0	2	0	0	9
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.875 0.8	0.000 75	0.000	0.000	0.500	0.000	0.000	0.7
		NORTI	HBOUND				HBOUND				BOUND			WESTE			
PM	0	1	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TO
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TO <sup>*</sup>
	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	
TOTAL VOLUMES :													0.00%	100.00%	0.00%	0.00%	
APPROACH %'s:																	TO
APPROACH %'s : PEAK HR :		04:30 PM			_	_											
APPROACH %'s : PEAK HR : PEAK HR VOL :	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1
APPROACH %'s : PEAK HR :	0 0.000			0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	0 0.000	1 0.250 0.25	0.000	0 0.000	0.

Location: Red Hill Rd & Montezuma Rd/SR 49 City: Chinese Camp Control: 1-Way Stop(NB)

									4axle								
NS/EW Streets:		Red H	Hill Rd			Red I	Hill Rd			Montezuma	Rd/SR 49			Montezuma	Rd/SR 49		
		NORTI	HBOUND			SOUTI	HBOUND			EAST	BOUND			WESTE	BOUND		
AM	0	1	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	0	0	0	0	0	0	0	0	2	0	0	0	0	0	0	2
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	1	0	0	0	1	0	0	2
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0	0	2
8:00 AM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	1
8:15 AM	0	0	0	0	0	0		0	0	_	•	0	0	2	0	0	3
8:30 AM 8:45 AM	0	0	0	0	0	0	0	0	0	4 2	0	0	0	0	0	0	6 2
8:45 AM	U	U	U	U	0	U	U	U	U	2	U	U	U	U	U	U	2
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTA
TOTAL VOLUMES :	0	0	0	0	0	0	0	0	0	11	0	0	0	7	0	0	18
APPROACH %'s:									0.00%	100.00%	0.00%	0.00%	0.00%	100.00%	0.00%	0.00%	
PEAK HR:			- 09:00 AM														TOTA
PEAK HR VOL :	0	0	0	0	0	0	0	0	0	8	0	0	0	4	0	0	12
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.500	0.000	0.000	0.000	0.500	0.000	0.000	0.500
										0.5	000			0.5			
					-												
		NORTI	HBOUND			SOUTI	HBOUND			EASTI	BOUND			WESTE	BOUND		
PM	0	NORTH	HBOUND 0	0	0	SOUTI	HBOUND 0	0	0	EASTI 1	BOUND 0	0	0	WESTE	BOUND 0	0	
	0 NL		0 NR	0 NU	SL	1 ST	0 SR	SU	EL	1 ET		EU	0 WL			WU	
4:00 PM		1	0		SL 0	1	O SR O			1	0			1	0		TOTA
4:00 PM 4:15 PM	NL 0 0	1 NT 0 0	0 NR 0 0	NU 0 0	SL 0 0	1 ST 0 0	0 SR 0 0	SU 0 0	0 0	1 ET 0 0	0 ER 1 0	0 0	WL 0 0	1 WT 1 0	0 WR 0 0	0 0	2 0
4:00 PM 4:15 PM 4:30 PM	NL 0 0 0	1 NT 0 0 0	0 NR 0 0	0 0 0	SL 0 0 0	1 ST 0 0 0	0 SR 0 0	0 0 0	0 0 0	1 ET 0 0 0	0 ER 1 0	0 0 0	0 0 0	1 WT 1 0 0	0 WR 0 0	0 0 0	0
4:00 PM 4:15 PM 4:30 PM 4:45 PM	NL 0 0 0 0	1 NT 0 0 0 0	0 NR 0 0 0	NU 0 0 0 0	SL 0 0 0 0	1 ST 0 0 0 0	0 SR 0 0 0	SU 0 0 0 0	EL 0 0 0 0	1 ET 0 0 0	0 ER 1 0 0	0 0 0 0	WL 0 0 0 0	1 WT 1 0 0 2	0 WR 0 0 0	WU 0 0 0	2 0 0 2
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM	NL 0 0 0 0 0	1 NT 0 0 0 0	0 NR 0 0 0 0	NU 0 0 0 0 0 0 0 0	SL 0 0 0 0	1 ST 0 0 0 0 0	0 SR 0 0 0	SU 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0	0 ER 1 0 0 0	EU 0 0 0 0 0 0 0 0	WL 0 0 0 0	1 WT 1 0 0 2	0 WR 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 0 0 2
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 0 0 0 0 0	1 NT 0 0 0 0 0	0 NR 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0	1 ST 0 0 0 0 0	0 SR 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0	1 ET 0 0 0 0 0	0 ER 1 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0	1 WT 1 0 0 2 1 0	0 WR 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 0 0 2 1 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 NT 0 0 0 0 0 0	0 NR 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0	1 ST 0 0 0 0 0 0	0 SR 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0	0 ER 1 0 0 0 0	EU 0 0 0 0 0 0	WL 0 0 0 0 0 0	1 WT 1 0 0 2 1 0 0	0 WR 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 0 0 2 1 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 0 0 0 0 0	1 NT 0 0 0 0 0	0 NR 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0	1 ST 0 0 0 0 0	0 SR 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0	1 ET 0 0 0 0 0	0 ER 1 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0	1 WT 1 0 0 2 1 0	0 WR 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 0 0 2 1 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	NL 0 0 0 0 0 0 0 0	1 NT 0 0 0 0 0 0 0	0 NR 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0	0 ER 1 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 1 0 0 2 1 0 0 0 2 0 0 0 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 0 0 2 1 0 0 0
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	NL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 NT 0 0 0 0 0 0 0	0 NR 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ST 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0	0 ER 1 0 0 0 0 0	EU 0 0 0 0 0 0	WL 0 0 0 0 0 0	1 WT 1 0 0 2 1 0 0 0	0 WR 0 0 0 0 0 0	0 0 0 0 0 0 0	2 0 0 2 1 0
4:00 PM 4:15 PM 4:30 PM 4:34 PM 5:00 PM 5:15 PM 5:30 PM 5:35 PM	NL 0 0 0 0 0 0 0 0	1 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 NR 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0	0 ER 1 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 1 0 0 2 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 0 0 2 1 0 0 0 TOTA
4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM	NL 0 0 0 0 0 0 0 0	1 NT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 NR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ST 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 SR 0 0 0 0 0 0 0 0	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 ET 0 0 0 0 0 0 0 0	0 ER 1 0 0 0 0 0 0 0 0	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WT 1 0 0 2 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 WR 0 0 0 0 0 0 0 0 0	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 0 0 2 1 0 0 0

Location: Red Hill Rd & Montezuma Rd/SR 49 City: Chinese Camp Control: 1-Way Stop(NB)

_	,	,						Data ·	- Bikes								
NS/EW Streets:		Red I	Hill Rd			Red I	Hill Rd			Montezum	a Rd/SR 49			Montezum	a Rd/SR 49		
		NORT	HBOUND			SOLITI	HBOUND			FAST	BOUND			WES	FBOUND		
AM	0	1	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ĒT	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	Ō	Ō	Ō	0	0	Ō	0	0	0	Ō	Ō	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR :		00:00 AM	- 09:00 AM														TOTAL
PEAK HR VOL :	0	08.00 AM	0 <b>9.00 A</b> M	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	"
1 ZARCHIC PAGEOR	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1 0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
		NORT	HBOUND			SOUT	HBOUND			FAST	BOUND			WES	FBOUND		
PM	0	1	0	0	0	1	0	0	0	1	0	0	0	1	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
											0	0	0	0			0
5:45 PM	0	0	0	0	0	0	0	0	0	0	U	U	U	U	0	0	0
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :					_								_				_
	NL	NT 0	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES : APPROACH %'s :	NL	NT 0	NR 0	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL 0
TOTAL VOLUMES : APPROACH %'s : PEAK HR :	NL 0	NT 0 04:30 PM	NR 0 - <b>05:30 PM</b>	NU 0	SL 0	ST 0	SR 0	SU 0	EL 0	ET 0	ER 0	EU 0	WL 0	WT 0	WR 0	WU 0	TOTAL 0

# National Data & Surveying Services Intersection Turning

Location: Red Hill Rd & Montezuma Rd/SR 49

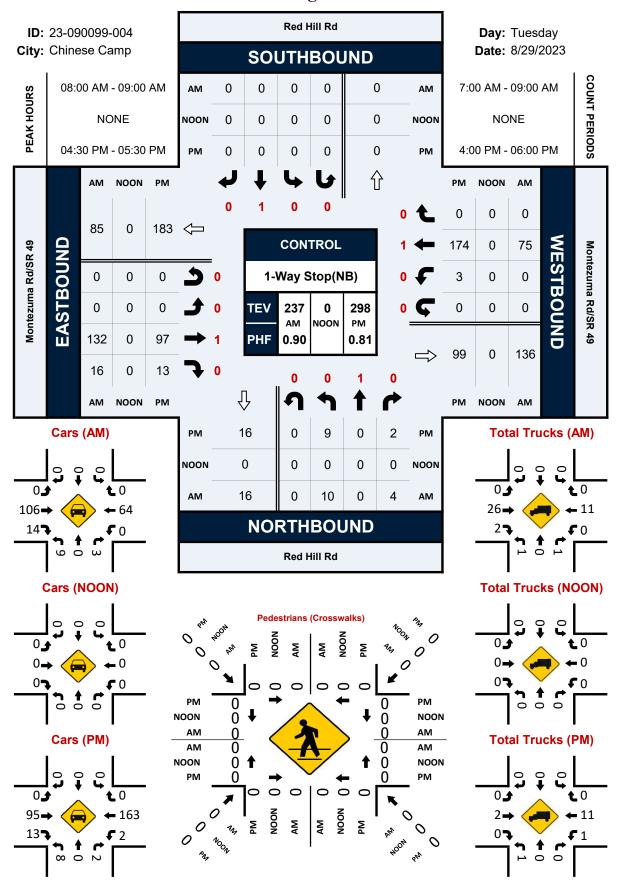
**Data - Pedestrians (Crosswalks)** 

NS/EW Streets:	Red	Hill Rd	Red	Hill Rd	Montezum	a Rd/SR 49	Montezum	a Rd/SR 49	
AM	_	TH LEG		TH LEG	_	Γ LEG		T LEG	
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
7:00 AM	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	0	0	0
PEAK HR:	08:00 AM	- 09:00 AM							TOTAL
PEAK HR VOL:	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR :									

PM	NORT	TH LEG	SOUT	'H LEG	EAST	LEG	WEST	T LEG	
PIVI	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES :	0	0	0	0	0	0	0	0	0
APPROACH %'s:									
PEAK HR:	04:30 PM	- 05:30 PM							TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR :									

#### Red Hill Rd & Montezuma Rd/SR 49

#### **Peak Hour Turning Movement Count**



# **Appendix B**LOS Worksheets

Intersection						
Int Delay, s/veh	1.4					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	YVDL	WDK 7	IND I	INDIX.	SDL 1	<u>361</u>
Traffic Vol, veh/h	<b>1</b> 20	147	<b>T</b> 430	14	<b>1</b> 97	<b>T</b> 338
Future Vol, veh/h	20	147	430	14	97	338
	0	0	430	0	0	336
Conflicting Peds, #/hr						
Sign Control RT Channelized	Stop	Stop	Free	Free	Free	Free
	-	Free	-	Free	- 475	None
Storage Length	0	25	-	75	475	-
Veh in Median Storage		-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	95	95	95	95	95	95
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	21	155	453	15	102	356
Major/Minor N	Minor1	N	/lajor1	N	//ajor2	
Conflicting Flow All	1013	-	0	-	453	0
Stage 1	453	_	-	-	-	-
Stage 2	560	-	_	-	-	-
Critical Hdwy	6.4	_	_	-	4.1	-
Critical Hdwy Stg 1	5.4	_	_	_		_
Critical Hdwy Stg 2	5.4	_	_	-	_	_
Follow-up Hdwy	3.5	_	_	_	2.2	_
Pot Cap-1 Maneuver	267	0	_	0	1118	_
Stage 1	645	0	_	0		_
Stage 2	576	0	_	0	_	_
Platoon blocked, %	010	-	_	U		_
Mov Cap-1 Maneuver	243	_	_	_	1118	_
Mov Cap-1 Maneuver	243	_	_		1110	
Stage 1	645	_		-	_	-
_			-	-	-	
Stage 2	524	-	-	<u>-</u>	-	-
Approach	WB		NB		SB	
	WB 21.2		NB 0		SB 1.9	
HCM Control Delay, s	21.2					
HCM Control Delay, s HCM LOS	21.2 C	NIDTIA	0	MDI ×Q	1.9	CDT
HCM Control Delay, s HCM LOS Minor Lane/Major Mvm	21.2 C		0 VBLn1V		1.9 SBL	SBT
HCM Control Delay, s HCM LOS  Minor Lane/Major Mvm Capacity (veh/h)	21.2 C	-	0 <u>/BLn1W</u> 243	-	1.9 SBL 1118	-
HCM Control Delay, s HCM LOS  Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio	21.2 C	-	0 VBLn1V 243 0.087	-	1.9 SBL 1118 0.091	-
HCM Control Delay, s HCM LOS  Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s)	21.2 C	-	0 VBLn1V 243 0.087 21.2	- - 0	1.9 SBL 1118 0.091 8.5	- - -
HCM Control Delay, s HCM LOS  Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio	21.2 C	-	0 VBLn1V 243 0.087	-	1.9 SBL 1118 0.091	-

Intersection						
Int Delay, s/veh	0					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		4	1>		W	
Traffic Vol, veh/h	0	111	169	0	0	0
Future Vol., veh/h	0	111	169	0	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-		-	None
Storage Length	_	-	_	-	0	-
Veh in Median Storage	.# -	0	0	_	0	_
Grade, %	, <i>''</i> -	0	0	_	0	_
Peak Hour Factor	88	88	88	88	88	88
Heavy Vehicles, %	0	0	0	0	0	0
			192			
Mvmt Flow	0	126	192	0	0	0
Major/Minor N	Major1	N	Major2	N	/linor2	
Conflicting Flow All	192	0		0	318	192
Stage 1	-	_	_	_	192	-
Stage 2	_	_	_	_	126	_
Critical Hdwy	4.1	_	_	_	6.4	6.2
Critical Hdwy Stg 1	-	_	_	<u>-</u>	5.4	- 0.2
		-	_	_	5.4	
Critical Hdwy Stg 2	-	-	-			-
Follow-up Hdwy	2.2	-	-	-	3.5	3.3
Pot Cap-1 Maneuver	1394	-	-	-	679	855
Stage 1	-	-	-	-	845	-
Stage 2	-	-	-	-	905	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver	1394	-	-	-	679	855
Mov Cap-2 Maneuver	-	-	-	-	679	-
Stage 1	-	-	-	-	845	-
Stage 2	_	-	-	-	905	-
J <b>J</b> .						
Approach	EB		WB		SB	
HCM Control Delay, s	0		0		0	
HCM LOS					Α	
Minor Lane/Major Mvm	t	EBL	EBT	WBT	WBR	SBI n1
			LDI	VVDI	יוטיי	ODLIT
Capacity (veh/h)		1394	-	-	-	-
HCM Lane V/C Ratio		-	-	-	-	-
HCM Control Delay (s)		0	-	-	-	0
HCM Lane LOS		Α	-	-	-	Α
HCM 95th %tile Q(veh)		0	-	-	-	-

Intersection						
Int Delay, s/veh	0.3					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	*	<b>↑</b>	1→		Y	
Traffic Vol, veh/h	3	105	163	2	1	6
Future Vol, veh/h	3	105	163	2	1	6
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	_		-	None
Storage Length	300	-	_	-	0	-
Veh in Median Storage	e,# -	0	0	-	0	-
Grade, %	-	0	0	_	0	_
Peak Hour Factor	86	86	86	86	86	86
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	3	122	190	2	1	7
WWW.CT IOW	Ū	122	100	_	•	
				_		
	Major1	N	Major2		/linor2	
Conflicting Flow All	192	0	-	0	319	191
Stage 1	-	-	-	-	191	-
Stage 2	_	-	-	-	128	-
Critical Hdwy	4.1	-	-	-	6.4	6.2
Critical Hdwy Stg 1	-	-	-	-	5.4	-
Critical Hdwy Stg 2	-	-	-	-	5.4	-
Follow-up Hdwy	2.2	-	-	-	3.5	3.3
Pot Cap-1 Maneuver	1394	-	-	-	678	856
Stage 1	-	-	-	-	846	-
Stage 2	_	_	-	_	903	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver	1394	-	-	-	677	856
Mov Cap-2 Maneuver	-	-	_	-	677	-
Stage 1	_	_	-	_	844	-
Stage 2	_	_	_	_	903	_
olago 2					000	
Approach	EB		WB		SB	
HCM Control Delay, s	0.2		0		9.4	
HCM LOS					Α	
Minor Lane/Major Mvn	nt	EBL	EBT	WBT	WBR :	SBLn1
Capacity (veh/h)		1394			-	825
HCM Lane V/C Ratio		0.003	_	<u>-</u>	_	0.01
HCM Control Delay (s	)	7.6	_	_	_	9.4
HCM Lane LOS		Α.	_	_	_	Э. <del>Т</del>
HCM 95th %tile Q(veh	)	0	_	_	_	0
	7					

Existing
Timing Plan: AM Peak Hour HCM 6th AWSC

Intersection												
Intersection Delay, s/veh	8.4											
Intersection LOS	Α											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		ર્લ	7									
Traffic Vol, veh/h	14	17	5	9	97	2	5	78	12	0	71	20
Future Vol, veh/h	14	17	5	9	97	2	5	78	12	0	71	20
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Heavy Vehicles, %	0	0	0	0	0	0	0	0	0	0	0	0
Mvmt Flow	16	19	6	10	110	2	6	89	14	0	81	23
Number of Lanes	0	1	1	0	1	1	0	1	1	0	1	1
Approach	EB			WB			NB				SB	
Opposing Approach	WB			EB			SB				NB	

Approach	EB	WB	NB	SB
Opposing Approach	WB	EB	SB	NB
Opposing Lanes	2	2	2	2
Conflicting Approach Left	SB	NB	EB	WB
Conflicting Lanes Left	2	2	2	2
Conflicting Approach Right	NB	SB	WB	EB
Conflicting Lanes Right	2	2	2	2
HCM Control Delay	8.2	8.9	8.3	8.1
HCM LOS	Α	A	A	A

Lane	NBLn1	NBLn2	EBLn1	EBLn2	WBLn1	WBLn2	SBLn1	SBLn2	
Vol Left, %	6%	0%	45%	0%	8%	0%	0%	0%	
Vol Thru, %	94%	0%	55%	0%	92%	0%	100%	0%	
Vol Right, %	0%	100%	0%	100%	0%	100%	0%	100%	
Sign Control	Stop								
Traffic Vol by Lane	83	12	31	5	106	2	71	20	
LT Vol	5	0	14	0	9	0	0	0	
Through Vol	78	0	17	0	97	0	71	0	
RT Vol	0	12	0	5	0	2	0	20	
Lane Flow Rate	94	14	35	6	120	2	81	23	
Geometry Grp	5	5	5	5	5	5	5	5	
Degree of Util (X)	0.132	0.016	0.053	0.007	0.171	0.003	0.113	0.027	
Departure Headway (Hd)	5.051	4.318	5.366	4.436	5.101	4.356	5.027	4.324	
Convergence, Y/N	Yes								
Cap	711	830	668	807	705	822	714	829	
Service Time	2.773	2.04	3.092	2.162	2.823	2.078	2.748	2.045	
HCM Lane V/C Ratio	0.132	0.017	0.052	0.007	0.17	0.002	0.113	0.028	
HCM Control Delay	8.5	7.1	8.4	7.2	8.9	7.1	8.4	7.2	
HCM Lane LOS	Α	Α	Α	Α	Α	Α	Α	Α	
HCM 95th-tile Q	0.5	0	0.2	0	0.6	0	0.4	0.1	

Intersection							
Int Delay, s/veh	0.6						
	EDT	EDD	WDI	WDT	NDI	NDD	
Movement	EBT	EBR	WBL	WBT	NBL	NBR	
Lane Configurations	104	47	^	4	<u>ነ</u>	7	
Traffic Vol, veh/h	161	17	0	88	11	5	
Future Vol, veh/h	161	17	0	88	11	5	
Conflicting Peds, #/hr	_ 0	_ 0	_ 0	_ 0	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-	None	-	None	
Storage Length	-	-	-	-	0	50	
Veh in Median Storage,		-	-	0	0	-	
Grade, %	0	-	-	0	0	-	
Peak Hour Factor	90	90	90	90	90	90	
Heavy Vehicles, %	0	0	0	0	0	0	
Mvmt Flow	179	19	0	98	12	6	
NA ' /NA'	4 4	_	4		ı		
	/lajor1		Major2		/linor1		
Conflicting Flow All	0	0	198	0	287	189	
Stage 1	-	-	-	-	189	-	
Stage 2	-	-	-	-	98	-	
Critical Hdwy	-	-	4.1	-	6.4	6.2	
Critical Hdwy Stg 1	-	-	-	-	5.4	-	
Critical Hdwy Stg 2	-	-	-	-	5.4	-	
Follow-up Hdwy	-	-	2.2	-	3.5	3.3	
Pot Cap-1 Maneuver	-	-	1387	-	708	858	
Stage 1	-	-	-	-	848	-	
Stage 2	-	-	-	-	931	-	
Platoon blocked, %	-	-		-			
Mov Cap-1 Maneuver	-	-	1387	-	708	858	
Mov Cap-2 Maneuver	-	-	-	-	708	-	
Stage 1	-	-	-	-	848	-	
Stage 2	_	-	-	-	931	-	
Approach	EB		WB		NB		
HCM Control Delay, s	0		0		9.9		
HCM LOS					Α		
Minor Long/Major Maren		VIDI11	VIDI 20	EDT	EDD	WDI	WDT
Minor Lane/Major Mvm		VBLn11		EBT	EBR	WBL	WBT
Capacity (veh/h)		708	858	-	-	1387	-
HCM Lane V/C Ratio		0.017		-	-	-	-
HCM Control Delay (s)		10.2	9.2	-	-	0	-
HCM Lane LOS		В	Α	-	-	Α	-
HCM 95th %tile Q(veh)		0.1	0	-	-	0	-

Intersection						
Int Delay, s/veh	1.5					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	YUL T	₩ M	<u>ND1</u>	TO IN	JDL	<u> </u>
Traffic Vol, veh/h	18	88	313	34	117	485
Future Vol, veh/h	18	88	313	34	117	485
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	Stop -	Free	riee -	Free	riee -	None
	0	25	-	75	475	None -
Storage Length Veh in Median Storage			0			0
		-		-	-	
Grade, %	0	-	0	-	-	0
Peak Hour Factor	96	96	96	96	96	96
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	19	92	326	35	122	505
Major/Minor I	Minor1	١	Major1	N	/lajor2	
Conflicting Flow All	1075	_	0	_	326	0
Stage 1	326	_	_	_	-	-
Stage 2	749	_	<u>-</u>	<u>-</u>	_	_
Critical Hdwy	6.4	_		_	4.1	_
Critical Hdwy Stg 1	5.4	_		_	4.1	-
	5.4		-			
Critical Hdwy Stg 2		-	-	-	2.2	
Follow-up Hdwy	3.5	-	-	-		-
Pot Cap-1 Maneuver	245	0	-	0	1245	-
Stage 1	736	0	-	0	-	-
Stage 2	471	0	-	0	-	-
Platoon blocked, %			-			-
Mov Cap-1 Maneuver	221	-	-	-	1245	-
Mov Cap-2 Maneuver	221	-	-	-	-	-
Stage 1	736	-	-	-	-	-
Stage 2	425	-	-	-	-	-
Approach	WB		NB		SB	
HCM Control Delay, s	22.8		0		1.6	
HCM LOS	C		U		1.0	
TOWI LOO	U					
Minor Lane/Major Mvm	nt	NBTV	VBLn1V	VBLn2	SBL	SBT
Capacity (veh/h)		-	221	-	1245	-
HCM Lane V/C Ratio		-	0.085	-	0.098	-
HCM Control Delay (s)		-	22.8	0	8.2	-
HCM Lane LOS		-	С	Α	Α	-
HCM 95th %tile Q(veh)	)	-	0.3	-	0.3	-

Intersection						
Int Delay, s/veh	0					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		स	1>		W	
Traffic Vol, veh/h	0	151	101	0	0	0
Future Vol, veh/h	0	151	101	0	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	_	-	_	-	0	-
Veh in Median Storage	e.# -	0	0	_	0	_
Grade, %		0	0	<u>-</u>	0	_
Peak Hour Factor	88	88	88	88	88	88
	0	0	00			0
Heavy Vehicles, %				0	0	
Mvmt Flow	0	172	115	0	0	0
Major/Minor I	Major1	N	Major2	N	Minor2	
Conflicting Flow All	115	0	_	0	287	115
Stage 1	-	-	_	_	115	_
Stage 2	_	-	-	_	172	_
Critical Hdwy	4.1	_	_	_	6.4	6.2
Critical Hdwy Stg 1	-	_	_	_	5.4	-
Critical Hdwy Stg 2	_	_	_	_	5.4	_
Follow-up Hdwy	2.2	<u>-</u>	_	<u>-</u>	3.5	3.3
Pot Cap-1 Maneuver	1487	_	_		708	943
Stage 1	-	_	_	<u>-</u>	915	343
Stage 2		-			863	
	-	-		-	003	-
Platoon blocked, %	4407	-	-	-	700	040
Mov Cap-1 Maneuver		-	-	-	708	943
Mov Cap-2 Maneuver	-	-	-	-	708	-
Stage 1	-	-	-	-	915	-
Stage 2	-	-	-	-	863	-
Approach	EB		WB		SB	
HCM Control Delay, s	0		0		0	
HCM LOS	U		U		A	
TIOW LOS						
Minor Lane/Major Mvm	nt	EBL	EBT	WBT	WBR	SBLn1
Capacity (veh/h)		1487	-	-	-	-
HCM Lane V/C Ratio		-	-	-	-	-
HCM Control Delay (s)		0	-	-	-	0
HCM Lane LOS		A	-	-	-	A
HCM 95th %tile Q(veh)	)	0	-	-	-	-
TIOW COM FOUND GIVEN						

0.2 EBL	0.2					
	FRI	EBT	WBT	WBR	SBL	SBR
1	7	<u> </u>	14₩	אטוי	₩.	אופט
	6	153	101	0	0	0
	6	153	101	0	0	0
	0	0	0	0	0	0
	Free	Free	Free	Free	Stop	Stop
		None	-		Stop -	None
						-
						_
						_
						81
						0
1	1	189	125	U	U	0
Major1	lajor1	١	/lajor2	N	/linor2	
125	125	0	-	0	328	125
-	-	-	-	-	125	-
_	-	-	-	-		-
4.1	4.1	_	_	-		6.2
-		-	_	_		-
_	_	_	_	_		_
22	22	_	_	_		3.3
		_	_			931
-	-	_	_			-
_	_	_	_			_
_					000	
1/7/	1/7/		_		668	931
			-			951
		-	-			-
		-	-	-		-
-	-	-	-	_	030	-
EB	EB		WB		SB	
0.3	0.3		0		0	
-4		EDI	EDT	MDT	WDD	2DI 4
nt			FRI	WRI	WBR	SBLN1
			-	-	-	-
			-	-	-	-
)			-	-	-	0
,			-	-	-	Α
1)		0	-	-	-	-
	M	300 e, # - 81 0 7  Major1 125 - 4.1 - 2.2 1474 1474 EB 0.3	300 - e, # - 0 81 81 81 0 0 7 189  Major1 N 125 0 4.1 2.2 - 1474 1474 5 - 1474 1 - 1 - 1474 1 - 1 - 1474 1 - 1 - 1474 1 - 1474 1 - 1 - 1474 1 - 1 - 1474 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	300 e,# - 0 0 e,# - 0 0 81 81 81 81 0 0 0 0 7 189 125  Major1 Major2 125 0	300 0 0 0 0	300

8.8

Α

Existing
Timing Plan: PM Peak Hour HCM 6th AWSC

Intersection												
Intersection Delay, s/veh	8.4											
Intersection LOS	Α											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		ર્લ	7		र्स	7		4	7		4	7
Traffic Vol, veh/h	21	90	10	7	43	3	4	53	8	0	87	28
Future Vol, veh/h	21	90	10	7	43	3	4	53	8	0	87	28
Peak Hour Factor	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Heavy Vehicles, %	0	0	0	0	0	0	0	0	0	0	0	0
Mvmt Flow	22	95	11	7	45	3	4	56	8	0	92	29
Number of Lanes	0	1	1	0	1	1	0	1	1	0	1	1
Approach	EB			WB			NB				SB	
Opposing Approach	WB			EB			SB				NB	
Opposing Lanes	2			2			2				2	
Conflicting Approach Left	SB			NB			EB				WB	
Conflicting Lanes Left	2			2			2				2	
Conflicting Approach Right	NB			SB			WB				EB	
Conflicting Lanes Right	2			2			2				2	

8.2

8.2

Α

Lane	NBLn1	NBLn2	EBLn1	EBLn2	WBLn1	WBLn2	SBLn1	SBLn2	
Vol Left, %	7%	0%	19%	0%	14%	0%	0%	0%	
Vol Thru, %	93%	0%	81%	0%	86%	0%	100%	0%	
Vol Right, %	0%	100%	0%	100%	0%	100%	0%	100%	
Sign Control	Stop								
Traffic Vol by Lane	57	8	111	10	50	3	87	28	
LT Vol	4	0	21	0	7	0	0	0	
Through Vol	53	0	90	0	43	0	87	0	
RT Vol	0	8	0	10	0	3	0	28	
Lane Flow Rate	60	8	117	11	53	3	92	29	
Geometry Grp	5	5	5	5	5	5	5	5	
Degree of Util (X)	0.085	0.01	0.166	0.013	0.075	0.004	0.128	0.035	
Departure Headway (Hd)	5.117	4.379	5.115	4.317	5.158	4.385	5.035	4.332	
Convergence, Y/N	Yes								
Cap	701	818	703	830	696	817	713	828	
Service Time	2.839	2.101	2.833	2.036	2.881	2.107	2.754	2.051	
HCM Lane V/C Ratio	0.086	0.01	0.166	0.013	0.076	0.004	0.129	0.035	
HCM Control Delay	8.3	7.1	8.9	7.1	8.3	7.1	8.5	7.2	
HCM Lane LOS	Α	Α	Α	Α	Α	Α	Α	Α	
HCM 95th-tile Q	0.3	0	0.6	0	0.2	0	0.4	0.1	

HCM Control Delay

HCM LOS

8.2

Intersection							
Int Delay, s/veh	0.5						
Movement	EBT	EBR	WBL	WBT	NBL	NBR	
Lane Configurations	\$	LDIK	1100	4	NDE.	7	
Traffic Vol, veh/h	98	13	4	185	10	2	
Future Vol, veh/h	98	13	4	185	10	2	
Conflicting Peds, #/hr	0	0	0	0	0	0	
	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-	None	-	None	
Storage Length	_	-	_	-	0	50	
Veh in Median Storage,		-	-	0	0	-	
Grade, %	0	_	_	0	0	_	
Peak Hour Factor	81	81	81	81	81	81	
Heavy Vehicles, %	0	0	0	0	0	0	
Mymt Flow	121	16	5	228	12	2	
N. S		_					
	ajor1		Major2		/linor1		
Conflicting Flow All	0	0	137	0	367	129	
Stage 1	-	-	-	-	129	-	
Stage 2	-	-	-	-	238	-	
Critical Hdwy	-	-	4.1	-	6.4	6.2	
Critical Hdwy Stg 1	-	-	-	-	5.4	-	
Critical Hdwy Stg 2	-	-	-	-	5.4	-	
Follow-up Hdwy	-	-	2.2	-	3.5	3.3	
Pot Cap-1 Maneuver	-	-	1459	-	637	926	
Stage 1	-	-	-	-	902	-	
Stage 2	-	-	-	-	806	-	
Platoon blocked, %	-	-		-			
Mov Cap-1 Maneuver	-	-	1459	-	634	926	
Mov Cap-2 Maneuver	-	-	-	-	634	-	
Stage 1	-	-	-	-	902	-	
Stage 2	-	-	-	-	803	-	
Approach	EB		WB		NB		
HCM Control Delay, s	0		0.2		10.5		
HCM LOS	U		0.2		В		
TIOWI LOO					D		
Minor Lane/Major Mvmt	1	NBLn11		EBT	EBR	WBL	WBT
Capacity (veh/h)		634	926	-		1459	-
HCM Lane V/C Ratio		0.019		-	-	0.003	-
HCM Control Delay (s)		10.8	8.9	-	-	7.5	0
HCM Lane LOS		В	Α	-	-	Α	Α
HCM 95th %tile Q(veh)		0.1	0	-	-	0	-
HCM 95th %tile Q(veh)		0.1	0	-	-	0	-

Intersection						
Int Delay, s/veh	1.8					
		WDD	NDT	NDD	CDI	CDT
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	<u>ች</u>	170	100	7	ነ	<b>†</b>
Traffic Vol, veh/h	23	170	430	19	129	338
Future Vol, veh/h	23	170	430	19	129	338
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	Free	-	Free	-	None
Storage Length	0	25	-	75	475	-
Veh in Median Storage	,#0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	95	95	95	95	95	95
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	24	179	453	20	136	356
Major/Minor	Nim a m4		1-11		1-10	
	Minor1		/lajor1		Major2	
Conflicting Flow All	1081	-	0	-	453	0
Stage 1	453	-	-	-	-	-
Stage 2	628	-	-	-	-	-
Critical Hdwy	6.4	-	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	-	-	-	2.2	-
Pot Cap-1 Maneuver	243	0	-	0	1118	-
Stage 1	645	0	-	0	-	-
Stage 2	536	0	-	0	-	-
Platoon blocked, %			_			_
Mov Cap-1 Maneuver	213	_	_	-	1118	-
Mov Cap-2 Maneuver	213	_	_	_	-	_
Stage 1	645	_	_	_	_	_
Stage 2	471	_	_		_	
Staye Z	4/1	-	_	-	_	-
Approach	WB		NB		SB	
HCM Control Delay, s	24.1		0		2.4	
HCM LOS	С					
Minor Lane/Major Mvm	+	NIDTM	VBLn1V	VDI 50	SBL	SBT
	l	INDIV				SDI
Capacity (veh/h)		-	213	-	1118	-
HCM Lane V/C Ratio		-	0.114		0.121	-
HCM Control Delay (s)		-	24.1	0	8.7	-
HCM Lane LOS		-	С	Α	Α	-
HCM 95th %tile Q(veh)		-	0.4	-	0.4	-

Intersection						
Int Delay, s/veh	0.7					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		4	1>		Y	
Traffic Vol, veh/h	16	132	187	9	5	8
Future Vol, veh/h	16	132	187	9	5	8
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage	e, # -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	88	88	88	88	88	88
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	18	150	213	10	6	9
N. A (N. A.)						
	Major1		Major2		/linor2	
Conflicting Flow All	223	0	-	0	404	218
Stage 1	-	-	-	-	218	-
Stage 2	-	-	-	-	186	-
Critical Hdwy	4.1	-	-	-	6.4	6.2
Critical Hdwy Stg 1	-	-	-	-	5.4	-
Critical Hdwy Stg 2	_	-	-	-	5.4	_
Follow-up Hdwy	2.2	-	-	-	3.5	3.3
Pot Cap-1 Maneuver	1358	_	_	-	606	827
Stage 1	-	_	_	_	823	-
Stage 2	_	_	_	_	851	_
Platoon blocked, %		_	_	<u>-</u>	001	
Mov Cap-1 Maneuver	1358	_	_	_	598	827
Mov Cap-1 Maneuver	1000		_	-	598	- 021
Stage 1		-	-		811	
	-	-	-	-		-
Stage 2	-	-	-	-	851	-
Approach	EB		WB		SB	
HCM Control Delay, s	0.8		0		10.1	
HCM LOS	0.0		- 0		В	
TIOWI LOG					D	
Minor Lane/Major Mvm	nt	EBL	EBT	WBT	WBR S	SBLn1
Capacity (veh/h)		1358	_	-	-	721
HCM Lane V/C Ratio		0.013	-	-	-	0.02
HCM Control Delay (s)		7.7	0	-	-	10.1
HCM Lane LOS		A	A	_	_	В
HCM 95th %tile Q(veh)	)	0	-	_	_	0.1
		J				J. 1

Intersection						
Int Delay, s/veh	1.4					
		EDT	VAIDT	MOD	051	000
	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		<b>†</b>	4		Y	
Traffic Vol, veh/h	24	110	172	6	4	24
Future Vol, veh/h	24	110	172	6	4	24
Conflicting Peds, #/hr	0	0	0	0	0	0
	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	300	-	-	-	0	-
Veh in Median Storage, #	# -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	86	86	86	86	86	86
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	28	128	200	7	5	28
Mailan/Minan	-:4		4-:0		A: 0	
	ajor1		Major2		Minor2	221
Conflicting Flow All	207	0	-	0	388	204
Stage 1	-	-	-	-	204	-
Stage 2	-	-	-	-	184	-
Critical Hdwy	4.1	-	-	-	6.4	6.2
Critical Hdwy Stg 1	-	-	-	-	5.4	-
Critical Hdwy Stg 2	-	-	-	-	5.4	-
Follow-up Hdwy	2.2	-	-	-	3.5	3.3
Pot Cap-1 Maneuver	1376	-	-	-	619	842
Stage 1	-	-	-	-	835	-
Stage 2	-	-	-	-	852	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver	1376	-	-	-	607	842
Mov Cap-2 Maneuver	-	-	-	-	607	-
Stage 1	-	-	_	-	818	-
Stage 2	_	_	_	_	852	_
					00=	
Approach	EB		WB		SB	
HCM Control Delay, s	1.4		0		9.7	
HCM LOS					Α	
Minor Lane/Major Mvmt		EBL	EBT	WBT	WBR S	SBI n1
		1376		וטייי	77017	798
Capacity (veh/h)			-	-	-	0.041
HCM Control Doloy (a)		0.02	-	-		
HCM Control Delay (s)		7.7	-	-	-	9.7 A
HCM Lane LOS HCM 95th %tile Q(veh)		0.1	-	-	-	0.1

Intersection												
Intersection Delay, s/veh	8.5											
Intersection LOS	Α											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		र्स	7		ર્ન	7		र्स	7		ર્ન	7
Traffic Vol, veh/h	17	17	5	9	97	7	5	82	12	4	73	21
Future Vol, veh/h	17	17	5	9	97	7	5	82	12	4	73	21
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Heavy Vehicles, %	0	0	0	0	0	0	0	0	0	0	0	0
Mvmt Flow	19	19	6	10	110	8	6	93	14	5	83	24
Number of Lanes	0	1	1	0	1	1	0	1	1	0	1	1
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	2			2			2			2		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	2			2			2			2		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	2			2			2			2		
HCM Control Delay	8.3			8.8			8.4			8.2		
HCM LOS	Α			Α			Α			Α		
Lane		NBLn1	NBLn2	EBLn1	EBLn2	WBLn1	WBLn2	SBLn1	SBLn2			

Lane	NBLn1	NBLn2	EBLn1	EBLn2	WBLn1	WBLn2	SBLn1	SBLn2	
Vol Left, %	6%	0%	50%	0%	8%	0%	5%	0%	
Vol Thru, %	94%	0%	50%	0%	92%	0%	95%	0%	
Vol Right, %	0%	100%	0%	100%	0%	100%	0%	100%	
Sign Control	Stop								
Traffic Vol by Lane	87	12	34	5	106	7	77	21	
LT Vol	5	0	17	0	9	0	4	0	
Through Vol	82	0	17	0	97	0	73	0	
RT Vol	0	12	0	5	0	7	0	21	
Lane Flow Rate	99	14	39	6	120	8	88	24	
Geometry Grp	7	7	7	7	7	7	7	7	
Degree of Util (X)	0.14	0.016	0.058	0.007	0.172	0.01	0.123	0.029	
Departure Headway (Hd)	5.081	4.349	5.434	4.479	5.142	4.397	5.08	4.351	
Convergence, Y/N	Yes								
Cap	707	824	660	799	699	815	707	823	
Service Time	2.804	2.072	3.161	2.206	2.864	2.118	2.804	2.075	
HCM Lane V/C Ratio	0.14	0.017	0.059	0.008	0.172	0.01	0.124	0.029	
HCM Control Delay	8.6	7.1	8.5	7.2	8.9	7.2	8.5	7.2	
HCM Lane LOS	А	Α	Α	Α	Α	Α	Α	Α	
HCM 95th-tile Q	0.5	0	0.2	0	0.6	0	0.4	0.1	

Int Delay, s/veh
Movement
Novement
Lane Configurations
Traffic Vol, veh/h
Future Vol, veh/h
Conflicting Peds, #/hr   O   O   O   O   O   O   O   Sign Control   Free   Free   Free   Free   Free   Stop   Stop   RT Channelized   - None   - None   - None   Storage Length   -   -   -   -   O   O   O   O   O   O
Sign Control         Free RTee         Free RTee RTee RTee         Free RT Channelized         Free RT Channelized         Free RT Channelized         None RT Channelized         Non RT Channelized         None R
RT Channelized
Storage Length
Veh in Median Storage, #         0         -         -         0         0         -           Grade, %         0         -         -         0         0         -           Peak Hour Factor         90         90         90         90         90         90           Heavy Vehicles, %         0         0         0         0         0         0           Mwnt Flow         184         19         1         104         12         7           Major/Minor         Major1         Major2         Minor1         Minor1         Conflicting Flow All         0         0         203         0         300         194           Stage 1         -         -         -         194         -         -         194         -         -         106         -         -         -         194         -         -         -         194         -         -         -         106         -         -         -         -         -         106         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -
Veh in Median Storage, #         0         -         -         0         0         -           Grade, %         0         -         -         0         0         -           Peak Hour Factor         90         90         90         90         90         90           Heavy Vehicles, %         0         0         0         0         0         0           Mwnt Flow         184         19         1         104         12         7           Major/Minor         Major1         Major2         Minor1         Minor1         Conflicting Flow All         0         0         203         0         300         194           Stage 1         -         -         -         194         -         -         194         -         -         106         -         -         -         194         -         -         -         194         -         -         -         106         -         -         -         -         -         106         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -
Grade, %         0         -         -         0         0         -           Peak Hour Factor         90
Peak Hour Factor         90
Major/Minor   Major1   Major2   Minor1
Mymit Flow         184         19         1         104         12         7           Major/Minor         Major1         Major2         Minor1           Conflicting Flow All         0         0         203         0         300         194           Stage 1         -         -         -         194         -           Stage 2         -         -         -         106         -           Critical Hdwy         Stg 1         -         -         -         5.4         -           Critical Hdwy Stg 2         -         -         -         5.4         -         -           Critical Hdwy Stg 2         -         -         -         5.4         -         -           Critical Hdwy Stg 2         -         -         -         5.4         -         -           Follow-up Hdwy         -         -         2.2         -         3.5         3.3           Pot Cap-1 Maneuver         -         1381         -         696         853           Stage 1         -         -         -         -         -         -         -         -         -         -         -         -         -
Major/Minor         Major1         Major2         Minor1           Conflicting Flow All         0         0         203         0         300         194           Stage 1         -         -         -         194         -           Stage 2         -         -         -         106         -           Critical Hdwy         -         4.1         -         6.4         6.2           Critical Hdwy Stg 1         -         -         -         5.4         -           Critical Hdwy Stg 2         -         -         -         5.4         -           Follow-up Hdwy         -         2.2         -         3.5         3.3           Pot Cap-1 Maneuver         -         1381         -         696         853           Stage 1         -         -         -         -         844         -           Stage 2         -         -         -         -         -         -           Mov Cap-1 Maneuver         -         1381         -         695         853           Mov Cap-2 Maneuver         -         -         -         -         844         -           Stage 1         -
Conflicting Flow All         0         0         203         0         300         194           Stage 1         -         -         -         194         -           Stage 2         -         -         -         106         -           Critical Hdwy         -         -         4.1         -         6.4         6.2           Critical Hdwy Stg 1         -         -         -         5.4         -           Critical Hdwy Stg 2         -         -         -         5.4         -           Follow-up Hdwy         -         -         2.2         -         3.5         3.3           Pot Cap-1 Maneuver         -         1381         -         696         853           Stage 1         -         -         -         844         -           Stage 2         -         -         -         -         695         853           Mov Cap-2 Maneuver         -         -         -         695         -         -           Stage 1         -         -         -         -         -         -         -         -         -         -         -         -         -         -
Conflicting Flow All         0         0         203         0         300         194           Stage 1         -         -         -         194         -           Stage 2         -         -         -         106         -           Critical Hdwy         -         -         4.1         -         6.4         6.2           Critical Hdwy Stg 1         -         -         -         5.4         -           Critical Hdwy Stg 2         -         -         -         5.4         -           Follow-up Hdwy         -         -         2.2         -         3.5         3.3           Pot Cap-1 Maneuver         -         1381         -         696         853           Stage 1         -         -         -         844         -           Stage 2         -         -         -         -         695         853           Mov Cap-2 Maneuver         -         -         -         695         -         -           Stage 1         -         -         -         -         844         -         -         -         -         -         -         -         -         -
Conflicting Flow All         0         0         203         0         300         194           Stage 1         -         -         -         194         -           Stage 2         -         -         -         106         -           Critical Hdwy         -         -         4.1         -         6.4         6.2           Critical Hdwy Stg 1         -         -         -         5.4         -           Critical Hdwy Stg 2         -         -         -         5.4         -           Follow-up Hdwy         -         -         2.2         -         3.5         3.3           Pot Cap-1 Maneuver         -         1381         -         696         853           Stage 1         -         -         -         844         -           Stage 2         -         -         -         -         695         853           Mov Cap-2 Maneuver         -         -         -         695         -         -           Stage 1         -         -         -         -         -         -         -         -         -         -         -         -         -         -
Stage 1       -       -       -       194       -         Stage 2       -       -       -       106       -         Critical Hdwy       -       4.1       -       6.4       6.2         Critical Hdwy Stg 1       -       -       -       5.4       -         Critical Hdwy Stg 2       -       -       -       5.4       -         Follow-up Hdwy       -       -       2.2       -       3.5       3.3         Pot Cap-1 Maneuver       -       1381       -       696       853         Stage 1       -       -       -       844       -         Stage 2       -       -       -       -       923       -         Mov Cap-1 Maneuver       -       -       1381       -       695       853         Mov Cap-2 Maneuver       -       -       -       695       -       -         Stage 1       -       -       -       844       -
Stage 2       -       -       -       106       -         Critical Hdwy       -       4.1       -       6.4       6.2         Critical Hdwy Stg 1       -       -       -       5.4       -         Critical Hdwy Stg 2       -       -       -       5.4       -         Follow-up Hdwy       -       -       2.2       -       3.5       3.3         Pot Cap-1 Maneuver       -       1381       -       696       853         Stage 1       -       -       -       844       -         Stage 2       -       -       -       -       923       -         Platoon blocked, %       -       -       -       -       -       923       -         Mov Cap-1 Maneuver       -       -       1381       -       695       853         Mov Cap-2 Maneuver       -       -       -       695       -       -         Stage 1       -       -       -       -       844       -         Stage 2       -       -       -       -       922       -         Amount Lane Major Mvmt       NBLn1 NBLn2       EBT       EBR
Critical Hdwy         -         -         4.1         -         6.4         6.2           Critical Hdwy Stg 1         -         -         -         5.4         -           Critical Hdwy Stg 2         -         -         -         5.4         -           Follow-up Hdwy         -         -         2.2         -         3.5         3.3           Pot Cap-1 Maneuver         -         1381         -         696         853           Stage 1         -         -         -         844         -           Stage 2         -         -         -         923         -           Platoon blocked, %         -         -         -         -         923         -           Mov Cap-1 Maneuver         -         -         1381         -         695         853           Mov Cap-2 Maneuver         -         -         -         695         -         -         844         -           Stage 1         -         -         -         -         844         -         -         -         922         -           Amount Lane Major Mvmt         NBLn1 NBLn2         EBT         EBR         WBL
Critical Hdwy Stg 1       -       -       -       5.4       -         Critical Hdwy Stg 2       -       -       -       5.4       -         Follow-up Hdwy       -       -       2.2       -       3.5       3.3         Pot Cap-1 Maneuver       -       -       1381       -       696       853         Stage 1       -       -       -       -       844       -         Stage 2       -
Critical Hdwy Stg 2         -         -         -         5.4         -           Follow-up Hdwy         -         -         2.2         -         3.5         3.3           Pot Cap-1 Maneuver         -         -         1381         -         696         853           Stage 1         -         -         -         -         844         -           Stage 2         -         -         -         -         -         -           Mov Cap-1 Maneuver         -         -         -         -         695         853           Mov Cap-2 Maneuver         -         -         -         695         -         -           Stage 1         -         -         -         -         844         -         -           Stage 2         -         -         -         -         922         -           Approach         EB         WB         NB         NB           HCM LOS         A         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -
Follow-up Hdwy         -         -         2.2         -         3.5         3.3           Pot Cap-1 Maneuver         -         -         1381         -         696         853           Stage 1         -         -         -         844         -           Stage 2         -         -         -         923         -           Platoon blocked, %         -         -         -         -           Mov Cap-1 Maneuver         -         -         1381         -         695         853           Mov Cap-2 Maneuver         -         -         -         695         -         -         844         -         -         -         844         -         -         -         844         -         -         -         922         -         -         -         922         -
Pot Cap-1 Maneuver         -         -         1381         -         696         853           Stage 1         -         -         -         -         844         -           Stage 2         -         -         -         923         -           Platoon blocked, %         -         -         -         -           Mov Cap-1 Maneuver         -         -         1381         -         695         853           Mov Cap-2 Maneuver         -         -         -         695         -         -         844         -         -         -         844         -         -         -         844         -         -         -         922         -           Approach         EB         WB         NB         NB         -         -         -         -         -         922         -           Approach         EB         WB         NB         NB         -
Stage 1       -       -       -       844       -         Stage 2       -       -       -       923       -         Platoon blocked, %       -       -       -       -         Mov Cap-1 Maneuver       -       -       1381       -       695       853         Mov Cap-2 Maneuver       -       -       -       695       -       -       695       -       -       844       -       -       -       695       -       -       -       844       -       -       -       922       -       -       -       -       922       - <t< td=""></t<>
Stage 2         -         -         923         -           Platoon blocked, %         -         -         -         -           Mov Cap-1 Maneuver         -         -         1381         -         695         853           Mov Cap-2 Maneuver         -         -         -         695         -           Stage 1         -         -         -         844         -           Stage 2         -         -         -         922         -           Approach         EB         WB         NB           HCM Control Delay, s         0         0.1         9.9           HCM LOS         A    Minor Lane/Major Mvmt  NBLn1 NBLn2  EBT  EBR  WBL  Capacity (veh/h)  695  853  - 1381  HCM Lane V/C Ratio  0.018  0.008  - 0.001  HCM Control Delay (s)  10.3  9.3  - 7.6  HCM Lane LOS  B  A  - A
Stage 2       -       -       -       923       -         Platoon blocked, %       -       -       -       -       -         Mov Cap-1 Maneuver       -       -       1381       -       695       853         Mov Cap-2 Maneuver       -       -       -       695       -         Stage 1       -       -       -       844       -         Stage 2       -       -       -       922       -         Approach       EB       WB       NB         HCM Control Delay, s       0       0.1       9.9         HCM LOS       A     Minor Lane/Major Mvmt  NBLn1 NBLn2  EBT  EBR  WBL  Capacity (veh/h)  695  853  1381  HCM Lane V/C Ratio  0.018  0.008  0.001  HCM Control Delay (s)  10.3  9.3  - 7.6  HCM Lane LOS  B  A  - A       HCM Lane LOS     B  A  A
Platoon blocked, %
Mov Cap-1 Maneuver         -         -         1381         -         695         853           Mov Cap-2 Maneuver         -         -         -         -         695         -           Stage 1         -         -         -         -         844         -           Stage 2         -         -         -         -         922         -           Approach         EB         WB         NB         NB           HCM Control Delay, s         0         0.1         9.9         -           HCM LOS         A         A         -         -         1381           Minor Lane/Major Mvmt         NBLn1 NBLn2         EBT         EBR         WBL           Capacity (veh/h)         695         853         -         -         1381           HCM Lane V/C Ratio         0.018         0.008         -         -         0.001           HCM Lane LOS         B         A         -         -         A
Mov Cap-2 Maneuver         -         -         -         695         -           Stage 1         -         -         -         844         -           Stage 2         -         -         -         922         -           Approach         EB         WB         NB         NB           HCM Control Delay, s         0         0.1         9.9         O.00         A         A           Minor Lane/Major Mvmt         NBLn1 NBLn2         EBT         EBR         WBL         Capacity (veh/h)         695         853         -         -         1381         HCM Lane V/C Ratio         0.018         0.008         -         -         0.001         HCM Control Delay (s)         10.3         9.3         -         -         7.6         HCM Lane LOS         B         A         -         -         A
Stage 1         -         -         -         844         -           Stage 2         -         -         -         922         -           Approach         EB         WB         NB           HCM Control Delay, s         0         0.1         9.9           HCM LOS         A           Minor Lane/Major Mvmt         NBLn1 NBLn2         EBT         EBR         WBL           Capacity (veh/h)         695         853         -         -         1381           HCM Lane V/C Ratio         0.018         0.008         -         -         0.001           HCM Control Delay (s)         10.3         9.3         -         -         7.6           HCM Lane LOS         B         A         -         -         A
Stage 2         -         -         -         922         -           Approach         EB         WB         NB           HCM Control Delay, s         0         0.1         9.9           HCM LOS         A             Minor Lane/Major Mvmt         NBLn1 NBLn2         EBT         EBR         WBL           Capacity (veh/h)         695         853         -         -         1381           HCM Lane V/C Ratio         0.018         0.008         -         -         0.001           HCM Control Delay (s)         10.3         9.3         -         -         7.6           HCM Lane LOS         B         A         -         -         A
Approach         EB         WB         NB           HCM Control Delay, s         0         0.1         9.9           HCM LOS         A           Minor Lane/Major Mvmt         NBLn1 NBLn2         EBT         EBR         WBL           Capacity (veh/h)         695         853         -         -         1381           HCM Lane V/C Ratio         0.018         0.008         -         -         0.001           HCM Control Delay (s)         10.3         9.3         -         -         7.6           HCM Lane LOS         B         A         -         -         A
HCM Control Delay, s   0   0.1   9.9
HCM Control Delay, s   0   0.1   9.9
HCM Control Delay, s   0   0.1   9.9
Minor Lane/Major Mvmt         NBLn1 NBLn2         EBT         EBR         WBL           Capacity (veh/h)         695         853         -         -         1381           HCM Lane V/C Ratio         0.018         0.008         -         -         0.001           HCM Control Delay (s)         10.3         9.3         -         -         7.6           HCM Lane LOS         B         A         -         A
Minor Lane/Major Mvmt         NBLn1 NBLn2         EBT         EBR         WBL           Capacity (veh/h)         695         853         -         -         1381           HCM Lane V/C Ratio         0.018         0.008         -         -         0.001           HCM Control Delay (s)         10.3         9.3         -         -         7.6           HCM Lane LOS         B         A         -         -         A
Capacity (veh/h)         695         853         -         -         1381           HCM Lane V/C Ratio         0.018         0.008         -         -         0.001           HCM Control Delay (s)         10.3         9.3         -         -         7.6           HCM Lane LOS         B         A         -         -         A
Capacity (veh/h)         695         853         -         -         1381           HCM Lane V/C Ratio         0.018         0.008         -         -         0.001           HCM Control Delay (s)         10.3         9.3         -         -         7.6           HCM Lane LOS         B         A         -         A
Capacity (veh/h)         695         853         -         -         1381           HCM Lane V/C Ratio         0.018         0.008         -         -         0.001           HCM Control Delay (s)         10.3         9.3         -         -         7.6           HCM Lane LOS         B         A         -         -         A
HCM Lane V/C Ratio       0.018 0.008       -       - 0.001         HCM Control Delay (s)       10.3 9.3 -       -       - 7.6         HCM Lane LOS       B A -       -       A
HCM Control Delay (s) 10.3 9.3 - 7.6 HCM Lane LOS B A - A
HCM Lane LOS B A A
HUM YATA WITE CIVEN 117 11 - 1
110W 30W 70W Q(VOII) 0.1 0 0

Intersection						
Int Delay, s/veh	1.7					
		MES	NET	NES	051	057
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	ሻ	7	<b>↑</b>	7	*	<b>↑</b>
Traffic Vol, veh/h	18	108	313	37	140	485
Future Vol, veh/h	18	108	313	37	140	485
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	Free	-	Free	-	None
Storage Length	0	25	-	75	475	-
Veh in Median Storage	, # 0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	96	96	96	96	96	96
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	19	113	326	39	146	505
		_		_		
	/linor1	N	/lajor1	N	//ajor2	
Conflicting Flow All	1123	-	0	-	326	0
Stage 1	326	-	-	-	-	-
Stage 2	797	-	-	-	-	-
Critical Hdwy	6.4	-	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	-	-	-	2.2	-
Pot Cap-1 Maneuver	230	0	_	0	1245	-
Stage 1	736	0	-	0	-	_
Stage 2	447	0	_	0	_	_
Platoon blocked, %		•	_	· ·		_
Mov Cap-1 Maneuver	203	_	_	_	1245	_
Mov Cap-2 Maneuver	203	_	_	-	1243	_
	736	_	-	-		
Stage 1			-	-	-	-
Stage 2	395	-	-	-	-	-
Approach	WB		NB		SB	
HCM Control Delay, s	24.5		0		1.9	
HCM LOS	C		J		1.0	
1 JOINI LOO						
Minor Lane/Major Mvm	t	NBTV	/BLn1V	VBLn2	SBL	SBT
Capacity (veh/h)		-	203	-	1245	-
HCM Lane V/C Ratio		-	0.092	-	0.117	-
HCM Control Delay (s)		-	24.5	0	8.3	-
HCM Lane LOS		-	С	Α	Α	-
HCM 95th %tile Q(veh)		-	0.3	-	0.4	-
(1011)						

latana ati a						
Intersection	0.0					
Int Delay, s/veh	0.2					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		4	f.		M	
Traffic Vol, veh/h	9	168	121	5	0	0
Future Vol, veh/h	9	168	121	5	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage	.# -	0	0	-	0	_
Grade, %	, _	0	0	_	0	_
Peak Hour Factor	88	88	88	88	88	88
Heavy Vehicles, %	0	0	0	0	0	0
Mymt Flow	10	191	138	6	0	0
IVIVIII( I IOW	10	131	100	U	U	U
Major/Minor N	//ajor1	N	/lajor2	N	/linor2	
Conflicting Flow All	144	0	-	0	352	141
Stage 1	-	-	-	-	141	-
Stage 2	-	-	-	-	211	-
Critical Hdwy	4.1	-	_	-	6.4	6.2
Critical Hdwy Stg 1	_	_	_	_	5.4	-
Critical Hdwy Stg 2	_	_	_	_	5.4	_
Follow-up Hdwy	2.2	_	_	_	3.5	3.3
Pot Cap-1 Maneuver	1451	_	_	_	650	912
Stage 1	-	_	_	_	891	-
Stage 2	_	_	_	_	829	_
Platoon blocked, %		_	_	_	023	
-	1451	-	-		645	912
Mov Cap-1 Maneuver				-	645	
Mov Cap-2 Maneuver	-	-	-	-		-
Stage 1	-	-	-	-	884	-
Stage 2	-	-	-	-	829	-
Approach	EB		WB		SB	
HCM Control Delay, s	0.4		0		0	
HCM LOS	V. 1				A	
110M 200					,,	
Minor Lane/Major Mvm	t	EBL	EBT	WBT	WBR:	SBLn1
Capacity (veh/h)		1451	-	-	-	-
HCM Lane V/C Ratio		0.007	-	-	-	-
HCM Control Delay (s)		7.5	0	-	-	0
HCM Lane LOS		Α	Α	-	-	Α
HCM 95th %tile Q(veh)		0	-	-	-	-

Intersection						
Int Delay, s/veh	1.3					
Movement	EBL	EBT	WBT	WDD	SBL	SBR
				WBR		SDK
Lane Configurations	22	152	106	2	Y	20
Traffic Vol, veh/h	23 23	153	106 106	3	4	20
Future Vol, veh/h		153		3	4	20
Conflicting Peds, #/hr	0	0	0		0	0
Sign Control	Free	Free None	Free	Free	Stop	Stop
RT Channelized	200		-		-	None
Storage Length	300	-	-	-	0	-
Veh in Median Storage,		0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	81	81	81	81	81	81
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	28	189	131	4	5	25
Major/Minor M	lajor1	N	Major2	N	/linor2	
Conflicting Flow All	135	0	-	0	378	133
Stage 1	-	_	_	-	133	-
Stage 2	_	_	_	_	245	_
Critical Hdwy	4.1	_	_	_	6.4	6.2
Critical Hdwy Stg 1	-T. I	_	_	_	5.4	- 0.2
Critical Hdwy Stg 2	_			_	5.4	_
Follow-up Hdwy	2.2	_	_	<u>-</u>	3.5	3.3
	1462		_		628	922
Stage 1	1402	_		<u>-</u>	898	-
Stage 2	_		_		800	
Platoon blocked, %	-	-	_	_	000	-
	1462		-		616	922
		-	-	-	616	
Mov Cap-2 Maneuver	-	-	-	-	616	-
Stage 1	-	-	-	-	881	-
Stage 2	-	-	-	-	800	-
Approach	EB		WB		SB	
HCM Control Delay, s	1		0		9.4	
HCM LOS	•		· ·		A	
110111 200					,,	
						/
Minor Lane/Major Mvmt		EBL	EBT	WBT	WBR :	
Capacity (veh/h)		1462	-	-	-	
HCM Lane V/C Ratio		0.019	-	-	-	0.035
HCM Control Delay (s)		7.5	-	-	-	9.4
HCM Lane LOS		Α	-	-	-	Α
HCM 95th %tile Q(veh)		0.1	-	-	-	0.1

Intersection			
Intersection Delay, s/veh	8.5		
Intersection LOS	Α		

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4	7		र्स	7		4	7		4	7
Traffic Vol, veh/h	22	90	10	7	43	7	4	55	8	4	87	28
Future Vol, veh/h	22	90	10	7	43	7	4	55	8	4	87	28
Peak Hour Factor	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Heavy Vehicles, %	0	0	0	0	0	0	0	0	0	0	0	0
Mvmt Flow	23	95	11	7	45	7	4	58	8	4	92	29
Number of Lanes	0	1	1	0	1	1	0	1	1	0	1	1
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	2			2			2			2		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	2			2			2			2		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	2			2			2			2		
HCM Control Delay	8.8			8.2			8.3			8.3		
HCM LOS	Α			Α			Α			Α		

Lane	NBLn1	NBLn2	EBLn1	EBLn2	WBLn1	WBLn2	SBLn1	SBLn2	
Vol Left, %	7%	0%	20%	0%	14%	0%	4%	0%	
Vol Thru, %	93%	0%	80%	0%	86%	0%	96%	0%	
Vol Right, %	0%	100%	0%	100%	0%	100%	0%	100%	
Sign Control	Stop								
Traffic Vol by Lane	59	8	112	10	50	7	91	28	
LT Vol	4	0	22	0	7	0	4	0	
Through Vol	55	0	90	0	43	0	87	0	
RT Vol	0	8	0	10	0	7	0	28	
Lane Flow Rate	62	8	118	11	53	7	96	29	
Geometry Grp	7	7	7	7	7	7	7	7	
Degree of Util (X)	0.089	0.01	0.168	0.013	0.076	0.009	0.135	0.036	
Departure Headway (Hd)	5.134	4.397	5.141	4.34	5.179	4.406	5.072	4.347	
Convergence, Y/N	Yes								
Cap	699	814	699	825	693	812	708	824	
Service Time	2.859	2.122	2.864	2.062	2.905	2.132	2.794	2.069	
HCM Lane V/C Ratio	0.089	0.01	0.169	0.013	0.076	0.009	0.136	0.035	
HCM Control Delay	8.4	7.2	8.9	7.1	8.3	7.2	8.6	7.2	
HCM Lane LOS	Α	Α	Α	Α	Α	Α	Α	Α	
HCM 95th-tile Q	0.3	0	0.6	0	0.2	0	0.5	0.1	

Intersection							
Int Delay, s/veh	0.5						
Movement	EBT	EBR	WBL	WBT	NBL	NBR	
Lane Configurations		וטוע	1100	4	٦	7	
Traffic Vol, veh/h	104	13	5	190	10	2	
Future Vol, veh/h	104	13	5	190	10	2	
Conflicting Peds, #/hr	0	0	0	0	0	0	
	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-	None	Slop -		
Storage Length	-	NOHE -	_	-	0	50	
Veh in Median Storage, #			_	0	0	-	
Grade, %	0	_	_	0	0	-	
Peak Hour Factor	81	81	81	81	81	81	
Heavy Vehicles, %	0	0	0	0	0	0	
Mymt Flow	128	16	6	235	12	2	
WWIIICHIOW	120	10	U	200	12		
Major/Minor Ma	ajor1	N	Major2	N	/linor1		
Conflicting Flow All	0	0	144	0	383	136	
Stage 1	-	-	-	-	136	-	
Stage 2	-	-	-	-	247	-	
Critical Hdwy	-	-	4.1	-	6.4	6.2	
Critical Hdwy Stg 1	-	-	-	-	5.4	-	
Critical Hdwy Stg 2	-	-	-	-	5.4	-	
Follow-up Hdwy	-	-	2.2	-	3.5	3.3	
Pot Cap-1 Maneuver	-	-	1451	-	624	918	
Stage 1	-	-	-	-	895	-	
Stage 2	-	-	-	-	799	-	
Platoon blocked, %	-	-		-			
Mov Cap-1 Maneuver	-	-	1451	-	621	918	
Mov Cap-2 Maneuver	-	-	-	-	621	-	
Stage 1	_	_	_	-	895	-	
Stage 2	-	_	_	_	795	_	
Olago Z					1 33		
Approach	EB		WB		NB		
HCM Control Delay, s	0		0.2		10.6		
HCM LOS					В		
Minor Lane/Major Mvmt	1	NBLn11	NBLn2	EBT	EBR	WBL	
Capacity (veh/h)		621	918	-		1451	
HCM Lane V/C Ratio			0.003	_		0.004	
HCM Control Delay (s)		10.9	8.9	_	_	7.5	
HCM Lane LOS		В	Α.5	_	_	Α.5	
HCM 95th %tile Q(veh)		0.1	0	_	_	0	
Sivi oo ai 70 aio Q(voii)		J. 1	- 0				

Intersection						
Int Delay, s/veh	1.5					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	VVDL	WDK	IND I	NDK	SDL N	<u>301</u>
Traffic Vol, veh/h	21	189	<b>T</b> 511	r 15	107	<b>T</b> 362
Future Vol, veh/h	21	189	511	15	107	362
Conflicting Peds, #/hr	0	109	0	0	0	302
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	Stop -	Free	riee -	Free	riee -	None
Storage Length	0	25	_	75	475	None -
Veh in Median Storage		-	0	-	475	0
Grade, %	,# 0	_	0	<u>-</u>	_	0
	95		95		95	95
Peak Hour Factor		95		95		
Heavy Vehicles, %	0	100	0	0	0	0
Mvmt Flow	22	199	538	16	113	381
Major/Minor N	Minor1	N	/lajor1	N	Major2	
Conflicting Flow All	1145	-	0	-	538	0
Stage 1	538	_	_	-	-	_
Stage 2	607	_	_	_	_	_
Critical Hdwy	6.4	_	_	_	4.1	_
Critical Hdwy Stg 1	5.4	_	_	_	-	_
Critical Hdwy Stg 2	5.4	_	_	_	_	_
Follow-up Hdwy	3.5	_	_	_	2.2	_
Pot Cap-1 Maneuver	223	0	_	0	1040	_
Stage 1	589	0	<u>-</u>	0	-	<u>-</u>
Stage 2	548	0	_	0	_	_
Platoon blocked, %	540	U	_	U	-	-
Mov Cap-1 Maneuver	199	_	-	_	1040	-
	199					
Mov Cap-2 Maneuver		-	-	-	-	-
Stage 1	589	-	-	-	-	-
Stage 2	488	-	-	-	-	-
Approach	WB		NB		SB	
HCM Control Delay, s	25.3		0		2	
HCM LOS	D					
Minardana (NA 11 NA		NDTA	/DL 41/	VDL 0	001	ODT
Minor Lane/Major Mvm	ι	MRIM	VBLn1V		SBL	SBT
0			7 (1(1	-	1040	-
Capacity (veh/h)		-	199			
HCM Lane V/C Ratio		-	0.111	-	0.108	-
HCM Lane V/C Ratio HCM Control Delay (s)		-	0.111 25.3	- 0	0.108 8.9	-
HCM Lane V/C Ratio		- - -	0.111	-	0.108	

Intersection						
Int Delay, s/veh	0					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
	EDL			WDK	SDL W	SDK
Lane Configurations	0	41	73	۸		٥
Traffic Vol, veh/h	0	121	212	0	0	0
Future Vol, veh/h	0	121	212	0	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-		-	None
Storage Length	- 	-	-	-	0	-
Veh in Median Storage,		0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	88	88	88	88	88	88
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	0	138	241	0	0	0
Major/Minor M	lajor1	N	/lajor2	N	/linor2	
Conflicting Flow All	241	0	-	0	379	241
Stage 1	-	-	_	-	241	-
Stage 2	_	_	_	<u>-</u>	138	<u>-</u>
Critical Hdwy	4.1	_	_	_	6.4	6.2
Critical Hdwy Stg 1	-	_	_	<u>-</u>	5.4	- 0.2
Critical Hdwy Stg 2	_	_		_	5.4	_
Follow-up Hdwy	2.2	_	_	_	3.5	3.3
	1337			_	627	803
Stage 1	1001	_	_	<u>-</u>	804	-
Stage 2	_			_	894	_
Platoon blocked, %	_	_	_		034	_
	1337	-	-	_	627	803
		-	-	-	627	- 003
Mov Cap-2 Maneuver	-	-	-	-		
Stage 1	-	-	-	-	804	-
Stage 2	-	-	-	-	894	-
Approach	EB		WB		SB	
	0		0		0	
HCM Control Delay, s	U				A	
HCM Control Delay, s HCM LOS	U					
HCM Control Delay, s HCM LOS	U					
HCM LOS		ED!	<b>CDT</b>	WDT	WDD	ODI 4
HCM LOS  Minor Lane/Major Mvmt		EBL	EBT	WBT	WBR	SBLn1
HCM LOS  Minor Lane/Major Mvmt Capacity (veh/h)		1337	-	-	-	-
Minor Lane/Major Mvmt Capacity (veh/h) HCM Lane V/C Ratio		1337	-	-	-	-
Minor Lane/Major Mvmt Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s)		1337 - 0	- - -	- -	- - -	- - 0
Minor Lane/Major Mvmt Capacity (veh/h) HCM Lane V/C Ratio		1337	-	-	-	-

Intersection						
Int Delay, s/veh	0.3					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	7	<b>^</b>	1		Y	
Traffic Vol, veh/h	3	115	206	2	1	6
Future Vol, veh/h	3	115	206	2	1	6
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	
Storage Length	300	-	-	-	0	-
Veh in Median Storage		0	0	_	0	_
Grade, %	- -	0	0	_	0	_
Peak Hour Factor	86	86	86	86	86	86
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	3	134	240	2	1	7
IVIVIIIL FIOW	3	134	240			I
Major/Minor	Major1	l N	Major2	N	/linor2	
Conflicting Flow All	242	0	-	0	381	241
Stage 1	-	-	_	-	241	Z <del>T</del> 1
Stage 2	-	_	_	_	140	_
	4.1	-			6.4	6.2
Critical Hdwy		-	-	-		
Critical Hdwy Stg 1	-	_	-	-	5.4	-
Critical Hdwy Stg 2	-	-	-	-	5.4	-
Follow-up Hdwy	2.2	_	-	-	3.5	3.3
Pot Cap-1 Maneuver	1336	-	-	-	625	803
Stage 1	-	_	-	-	804	-
Stage 2	-	-	-	-	892	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver	1336	-	-	-	624	803
Mov Cap-2 Maneuver	-	-	-	-	624	-
Stage 1	-	_	_	-	802	_
Stage 2	_	_	_	_	892	_
Clayo Z					552	
Approach	EB		WB		SB	
HCM Control Delay, s	0.2		0		9.7	
HCM LOS					Α	
NAII (NA NA		EDI	EDT	MOT	MDD	אום ב
Minor Lane/Major Mvm	IL	EBL	EBT	WBT	WBR S	
Capacity (veh/h)		1336	-	-	-	2 2 2
HCM Lane V/C Ratio		0.003	-	-	-	0.011
HCM Control Delay (s)		7.7	-	-	-	9.7
HCM Lane LOS		Α	-	-	-	Α
HCM 95th %tile Q(veh	)	0	-	-	-	0
,						

Intersection		
Intersection Delay, s/veh	8.7	
Intersection LOS	Α	

intorcootion Eco												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		ર્ન	7		र्स	7		ર્ન	7		4	7
Traffic Vol, veh/h	27	18	5	9	101	14	5	93	12	2	76	23
Future Vol, veh/h	27	18	5	9	101	14	5	93	12	2	76	23
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Heavy Vehicles, %	0	0	0	0	0	0	0	0	0	0	0	0
Mvmt Flow	31	20	6	10	115	16	6	106	14	2	86	26
Number of Lanes	0	1	1	0	1	1	0	1	1	0	1	1
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	2			2			2			2		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	2			2			2			2		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	2			2			2			2		
HCM Control Delay	8.7			8.9			8.7			8.3		
HCM LOS	Α			Α			Α			Α		

Lane	NBLn1	NBLn2	EBLn1	EBLn2	WBLn1	WBLn2	SBLn1	SBLn2	
Vol Left, %	5%	0%	60%	0%	8%	0%	3%	0%	
Vol Thru, %	95%	0%	40%	0%	92%	0%	97%	0%	
Vol Right, %	0%	100%	0%	100%	0%	100%	0%	100%	
Sign Control	Stop								
Traffic Vol by Lane	98	12	45	5	110	14	78	23	
LT Vol	5	0	27	0	9	0	2	0	
Through Vol	93	0	18	0	101	0	76	0	
RT Vol	0	12	0	5	0	14	0	23	
Lane Flow Rate	111	14	51	6	125	16	89	26	
Geometry Grp	5	5	5	5	5	5	5	5	
Degree of Util (X)	0.159	0.017	0.079	0.007	0.18	0.02	0.127	0.032	
Departure Headway (Hd)	5.151	4.423	5.543	4.537	5.198	4.453	5.15	4.434	
Convergence, Y/N	Yes								
Сар	697	809	646	787	690	803	697	807	
Service Time	2.88	2.151	3.278	2.272	2.928	2.184	2.879	2.163	
HCM Lane V/C Ratio	0.159	0.017	0.079	0.008	0.181	0.02	0.128	0.032	
HCM Control Delay	8.9	7.2	8.8	7.3	9.1	7.3	8.6	7.3	
HCM Lane LOS	Α	Α	Α	Α	Α	Α	Α	Α	
HCM 95th-tile Q	0.6	0.1	0.3	0	0.7	0.1	0.4	0.1	

Intersection						
Int Delay, s/veh	0.5					
	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	1			4	7	7
Traffic Vol, veh/h	184	18	0	131	11	5
Future Vol, veh/h	184	18	0	131	11	5
Conflicting Peds, #/hr	0	0	0	0	0	0
	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	50
Veh in Median Storage, #	<del>#</del> 0	-	_	0	0	-
Grade, %	0	_	_	0	0	_
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	204	20	0	146	12	6
IVIVIII I IOW	204	20	U	170	12	U
Major/Minor Ma	ajor1	N	Major2	<u> </u>	/linor1	
Conflicting Flow All	0	0	224	0	360	214
Stage 1	-	-	-	-	214	-
Stage 2	-	-	-	_	146	-
Critical Hdwy	-	-	4.1	_	6.4	6.2
Critical Hdwy Stg 1	-	_	-	_	5.4	-
Critical Hdwy Stg 2	_	_	_	_	5.4	_
Follow-up Hdwy	_	<u>-</u>	2.2	_	3.5	3.3
Pot Cap-1 Maneuver	_		1357	_	643	831
Stage 1		_	1001	_	826	- 001
Stage 2					886	
	-	-	-	-	000	-
Platoon blocked, %	-	-	1257	-	640	004
Mov Cap-1 Maneuver	-	-	1357	-	643	831
Mov Cap-2 Maneuver	-	-	-	-	643	-
Stage 1	-	-	-	-	826	-
Stage 2	-	-	-	-	886	-
Approach	EB		WB		NB	
HCM Control Delay, s	0		0		10.3	
HCM LOS	U		U		10.3 B	
HOW LOS					В	
Minor Lane/Major Mvmt	1	NBLn11	NBLn2	EBT	EBR	WBL
Capacity (veh/h)		643	831	-		1357
HCM Lane V/C Ratio		0.019		_	_	-
HCM Control Delay (s)		10.7	9.4	_	_	0
HCM Lane LOS		В	3. <del>4</del>	_	_	A
HCM 95th %tile Q(veh)		0.1	0	_	_	0
		0.1	U	-	-	U

Intersection						
Int Delay, s/veh	1.7					
-		WDD	NDT	NDD	001	OPT
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	<b>\</b>	7	<b>↑</b>	7	<b>1</b> 50	<b>†</b>
Traffic Vol, veh/h	19	110	357	35	158	569
Future Vol, veh/h	19	110	357	35	158	569
Conflicting Peds, #/hr	0	0	_ 0	0	_ 0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	Free	-	Free	-	None
Storage Length	0	25	-	75	475	-
Veh in Median Storage		-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	96	96	96	96	96	96
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	20	115	372	36	165	593
Majay/Mina	N 1: 1		1-1-1		1-10	
	Minor1		/lajor1	<u> </u>	Major2	
Conflicting Flow All	1295	-	0	-	372	0
Stage 1	372	-	-	-	-	-
Stage 2	923	-	-	-	-	-
Critical Hdwy	6.4	-	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	-	-	-	2.2	-
Pot Cap-1 Maneuver	181	0	-	0	1198	-
Stage 1	702	0	-	0	-	-
Stage 2	390	0	-	0	-	-
Platoon blocked, %			_			_
Mov Cap-1 Maneuver	156	_	_	_	1198	_
Mov Cap 1 Maneuver		_	_	_		_
Stage 1	702					
Stage 2	336	_	_			
Staye 2	330	-	_	-	_	<u>-</u>
Approach	WB		NB		SB	
HCM Control Delay, s	31.4		0		1.8	
HCM LOS	D					
J 200						
			/DI /	/DI		05-
Minor Lane/Major Mvr	nt	NBTV	VBLn1V		SBL	SBT
Capacity (veh/h)		-			1198	-
HCM Lane V/C Ratio		-	0.127	-	0.137	-
HCM Control Delay (s	)	-	31.4	0	8.5	-
HCM Lane LOS		-	D	Α	Α	-
HCM 95th %tile Q(veh	1)	-	0.4	-	0.5	-

Intersection						
Int Delay, s/veh	0					
		<b>FDT</b>	WDT	WDD	CDI	CDD
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	^	4	100	•	Y	0
Traffic Vol, veh/h	0	193	123	0	0	0
Future Vol, veh/h	0	193	123	0	0	0
Conflicting Peds, #/hr	_ 0	_ 0	0	_ 0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-		-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage	e, # -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	88	88	88	88	88	88
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	0	219	140	0	0	0
Majay/Minay	\		/a:a#0	N	Air and	
	Major1		Major2		Minor2	1.10
Conflicting Flow All	140	0	-	0	359	140
Stage 1	-	-	-	-	140	-
Stage 2	-	-	-	-	219	-
Critical Hdwy	4.1	-	-	-	6.4	6.2
Critical Hdwy Stg 1	-	-	-	-	5.4	-
Critical Hdwy Stg 2	-	-	-	-	5.4	-
Follow-up Hdwy	2.2	-	-	-	3.5	3.3
Pot Cap-1 Maneuver	1456	-	-	-	644	913
Stage 1	-	-	-	-	892	-
Stage 2	-	-	-	-	822	-
Platoon blocked, %		_	_	-		
Mov Cap-1 Maneuver	1456	-	-	_	644	913
Mov Cap-2 Maneuver	-	-	_	_	644	-
Stage 1	_	_	_	_	892	_
Stage 2	_	_	_	_	822	_
Olago Z					ULL	
Approach	EB		WB		SB	
HCM Control Delay, s	0		0		0	
HCM LOS					Α	
Minor Long/Major M.	.1	ED!	EDT	WDT	WDD	CDL = 4
Minor Lane/Major Mvm	IL	EBL	EBT	WBT	WBR	ORFU!
Capacity (veh/h)		1456	-	-	-	-
HCM Lane V/C Ratio		-	-	-	-	-
HCM Control Delay (s)		0	-	-	-	0
		٨		-		٨
HCM Lane LOS HCM 95th %tile Q(veh)		A 0	-	_	-	Α

Intersection						
Int Delay, s/veh	0.1					
		FOT	MOT	14/55	051	055
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	ሻ	<b>†</b>	7		Y	
Traffic Vol, veh/h	6	195	123	0	0	0
Future Vol, veh/h	6	195	123	0	0	0
Conflicting Peds, #/hr	_ 0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	300	-	-	-	0	-
Veh in Median Storage	e, # -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	81	81	81	81	81	81
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	7	241	152	0	0	0
Majay/Mina	NA=1==4		Ania TO		Aim c = O	
	Major1		Major2		/linor2	
Conflicting Flow All	152	0	-	0	407	152
Stage 1	-	-	-	-	152	-
Stage 2	-	-	-	-	255	-
Critical Hdwy	4.1	-	-	-	6.4	6.2
Critical Hdwy Stg 1	-	-	-	-	5.4	-
Critical Hdwy Stg 2	-	-	-	-	5.4	-
Follow-up Hdwy	2.2	-	-	-	3.5	3.3
Pot Cap-1 Maneuver	1441	-	-	-	604	900
Stage 1	-	-	-	-	881	-
Stage 2	-	-	-	-	792	-
Platoon blocked, %		_	_	-		
Mov Cap-1 Maneuver	1441	-	_	-	601	900
Mov Cap-2 Maneuver	-	_	_	_	601	-
Stage 1	_	_	_	_	877	_
Stage 2					792	_
Olaye Z	_	_		-	132	_
Approach	EB		WB		SB	
HCM Control Delay, s	0.2		0		0	
HCM LOS					A	
NA: 1 /NA -: 14		EDI	- CDT	MDT	MDD	0DL 4
Minor Lane/Major Mvn	π	EBL	EBT	WBT	WBR :	SBLN1
Capacity (veh/h)		1441	-	-	-	-
HCM Lane V/C Ratio		0.005	-	-	-	-
HCM Control Delay (s)		7.5	-	-	-	0
HCM Lane LOS		Α	-	-	-	Α
HCM 95th %tile Q(veh	)	0	-	-	-	-

Intersection		
Intersection Delay, s/veh	8.6	
Intersection LOS	Α	

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		ર્ન	7		4	7		ર્લ	7		र्स	7
Traffic Vol, veh/h	28	94	10	7	45	9	4	61	8	12	103	41
Future Vol, veh/h	28	94	10	7	45	9	4	61	8	12	103	41
Peak Hour Factor	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Heavy Vehicles, %	0	0	0	0	0	0	0	0	0	0	0	0
Mvmt Flow	29	99	11	7	47	9	4	64	8	13	108	43
Number of Lanes	0	1	1	0	1	1	0	1	1	0	1	1
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	2			2			2			2		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	2			2			2			2		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	2			2			2			2		
HCM Control Delay	9			8.3			8.4			8.6		
HCM LOS	Α			Α			Α			Α		

Lane	NBLn1	NBLn2	EBLn1	EBLn2	WBLn1	WBLn2	SBLn1	SBLn2	
Vol Left, %	6%	0%	23%	0%	13%	0%	10%	0%	
Vol Thru, %	94%	0%	77%	0%	87%	0%	90%	0%	
Vol Right, %	0%	100%	0%	100%	0%	100%	0%	100%	
Sign Control	Stop								
Traffic Vol by Lane	65	8	122	10	52	9	115	41	
LT Vol	4	0	28	0	7	0	12	0	
Through Vol	61	0	94	0	45	0	103	0	
RT Vol	0	8	0	10	0	9	0	41	
Lane Flow Rate	68	8	128	11	55	9	121	43	
Geometry Grp	5	5	5	5	5	5	5	5	
Degree of Util (X)	0.099	0.01	0.188	0.013	0.081	0.012	0.173	0.053	
Departure Headway (Hd)	5.217	4.483	5.275	4.456	5.306	4.535	5.155	4.399	
Convergence, Y/N	Yes								
Сар	686	797	681	803	675	788	696	813	
Service Time	2.953	2.218	3.006	2.187	3.042	2.27	2.885	2.13	
HCM Lane V/C Ratio	0.099	0.01	0.188	0.014	0.081	0.011	0.174	0.053	
HCM Control Delay	8.5	7.3	9.2	7.2	8.5	7.3	9	7.4	
HCM Lane LOS	А	Α	Α	Α	Α	Α	Α	Α	
HCM 95th-tile Q	0.3	0	0.7	0	0.3	0	0.6	0.2	

Intersection							
Int Delay, s/veh	0.4						
		===	14/	14/5-			
	EBT	EBR	WBL	WBT	NBL	NBR	
Lane Configurations	₽			4	7	7	
Traffic Vol, veh/h	140	14	4	216	10	2	
Future Vol, veh/h	140	14	4	216	10	2	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-	None	-	None	
Storage Length	-	-	-	-	0	50	
Veh in Median Storage, #	# 0	-	-	0	0	-	
Grade, %	0	-	-	0	0	_	
Peak Hour Factor	81	81	81	81	81	81	
Heavy Vehicles, %	0	0	0	0	0	0	
Mvmt Flow	173	17	5	267	12	2	
IVIVIIIL I IOW	173	17	J	201	12		
Major/Minor Ma	ajor1	N	Major2	N	/linor1		ı
Conflicting Flow All	0	0	190	0	459	182	
Stage 1	-	-	-	-	182	-	
Stage 2	_	-	_	-	277	-	
Critical Hdwy	_	_	4.1	-	6.4	6.2	
Critical Hdwy Stg 1	-	-		_	5.4	-	
Critical Hdwy Stg 2	_	_	_	_	5.4	_	
Follow-up Hdwy	_	_	2.2	_	3.5	3.3	
Pot Cap-1 Maneuver	_	_	1396	_	564	866	
Stage 1		_	1330	_	854	- 000	
					774		
Stage 2	-	-	-	-	114	-	
Platoon blocked, %	-	-	4000	-	F00	000	
Mov Cap-1 Maneuver	-	-	1396	-	562	866	
Mov Cap-2 Maneuver	-	-	-	-	562	-	
Stage 1	-	-	-	-	854	-	
Stage 2	-	-	-	-	771	-	
Approach	EB		WB		NB		
	0		0.1		11.2		
HCM LOS	U		U. I				
HCM LOS					В		
Minor Lane/Major Mvmt	1	NBLn1N	NBLn2	EBT	EBR	WBL	
Capacity (veh/h)		562	866	-		1396	
HCM Lane V/C Ratio		0.022		_		0.004	
HCM Control Delay (s)		11.6	9.2	_	_	7.6	
HCM Lane LOS		В				Α.	
			A 0	-	-	0	
HCM 95th %tile Q(veh)		0.1	U	-	-	U	

1.9					
\/\/RI	W/RR	NRT	NRR	SRI	SBT
					262
					362
					362
					_ 0
Stop		Free		Free	Free
-		-		-	None
0	25	-	75	475	-
ge,# 0	-	0	-	-	0
0	-	0	-	-	0
95	95	95	95	95	95
0					0
					381
23	220	550	Z 1	170	JU 1
Minor1	N	Major1	ı	Major2	
	-		_		0
				-	-
					-
					-
	-	-			-
	-	-	-	-	-
	-	-	-		-
	0	-		1040	-
589	0	-	0		-
511	0	-	0	-	-
		-			-
r 175	-	_	_	1040	-
	_	_	_	-	_
	_		_	_	_
439	-	-	-	-	-
WB		NB		SB	
		U		2.0	
D					
	NRTW	VBLn1V	VBLn2	SBL	SBT
/mt	11011				
/mt	-			1040	
	-	175	-	1040 0 141	-
)	-	175 0.144	-	0.141	-
	-	175 0.144 29	- 0	0.141 9	-
)	-	175 0.144	-	0.141	-
	0 ge, # 0 0 95 0 25 Minor1 1211 538 673 6.4 5.4 5.4 5.4 3.5 203	24 212 24 212 27 0 0 Stop Stop - Free 0 25 ge, # 0 - 95 95 0 0 25 223  Minor1 N 1211 - 538 - 673 - 6.4 - 5.4 - 3.5 - 7 203 0 589 0 511 0 er 175 - er 175 - 589 - 439 - WB s 29	24 212 511 24 212 511 r 0 0 0 Stop Stop Free - Free - 0 25 - ge, # 0 - 0 95 95 95 0 0 0 0 25 223 538  Minor1 Major1 1211 - 0 538 633 64 54 54 54 554 554 554 554 554 554 555 67 3 68 69 51 0 - 69 51 0 - 69 51 0 - 69 51 0 - 69 51 0 - 69 51 0 - 69 51 0 - 69 51 0 - 69 51 0 - 69 51 0 - 69 51 0 - 69 51 0 - 69 51 0 - 69 51 0 - 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 0 60 0 0 60 0 0 0 60	24 212 511 20 24 212 511 20 r 0 0 0 0 0 Stop Stop Free Free - Free - Free 0 25 - 75 ge, # 0 - 0 - 0 - 0 - 95 95 95 95 0 0 0 0 0 25 223 538 21  Minor1 Major1 1 1211 - 0 - 538 6.4 5.4 -	24 212 511 20 139 24 212 511 20 139 If 0 0 0 0 0 0 Stop Stop Free Free Free - Free - Free - Free - Free - Free - Free 0 25 - 75 475 ge, # 0 - 0 0 - 0 95 95 95 95 95 95 0 0 0 0 0 0 0 25 223 538 21 146  Minor1 Major1 Major2  1211 - 0 - 538 538 6.4 4.1 5.4 4.1 5.4 4.1 5.4 2.2 f 203 0 - 0 1040 589 0 - 0 - 538 er 175 2.2 f 203 0 - 0 1040 589 0 - 0 - 538 er 175 1040 er 175 1040 er 175 1040 er 175

Interception						
Intersection Int Delay, s/veh	0.6					
•						
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		4	1		N.	
Traffic Vol, veh/h	16	142	230	9	5	8
Future Vol, veh/h	16	142	230	9	5	8
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage	, # -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	88	88	88	88	88	88
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	18	161	261	10	6	9
	Major1		/lajor2		/linor2	
Conflicting Flow All	271	0	-	0	463	266
Stage 1	-	-	-	-	266	-
Stage 2	-	-	-	-	197	-
Critical Hdwy	4.1		-	-	6.4	6.2
Critical Hdwy Stg 1	-	-	-	-	5.4	-
Critical Hdwy Stg 2	-		-	_	5.4	-
Follow-up Hdwy	2.2	-	-	_	3.5	3.3
Pot Cap-1 Maneuver	1304	_	_	_	561	778
Stage 1	-	_	_	_	783	-
Stage 2	_	_	_	_	841	_
Platoon blocked, %		_	_	_	O-T 1	
Mov Cap-1 Maneuver	1304	_		_	553	778
Mov Cap-1 Maneuver	1304	_	_	_	553	- 110
·		-				
Stage 1	-	-	-	-	771	-
Stage 2	-	-	-	-	841	-
Approach	EB		WB		SB	
HCM Control Delay, s	0.8		0		10.5	
HCM LOS	0.0		U		В	
TIOWI LOG					ט	
Minor Lane/Major Mvm	nt	EBL	EBT	WBT	WBR:	SBL <sub>n1</sub>
Capacity (veh/h)		1304	-	-	-	673
HCM Lane V/C Ratio		0.014	-	-	-	0.022
HCM Control Delay (s)		7.8	0	-	-	10.5
HCM Lane LOS		Α	A	-	_	В
HCM 95th %tile Q(veh)		0	-	_	_	0.1
Sivi oo ar 70 allo Q(VOII)		U				J. 1

Intersection						
Int Delay, s/veh	1.2					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	7	<b>^</b>	13		A.	
Traffic Vol, veh/h	24	120	215	6	4	24
Future Vol, veh/h	24	120	215	6	4	24
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	
Storage Length	300	-	-	-	0	-
Veh in Median Storage,		0	0	-	0	_
Grade, %	, <i>''</i> -	0	0	_	0	_
Peak Hour Factor	86	86	86	86	86	86
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	28	140	250	7	5	28
IVIVIIIL FIOW	20	140	200	I	J	20
Major/Minor N	//ajor1	N	/lajor2	N	/linor2	
Conflicting Flow All	257	0	-	0	450	254
Stage 1		-	_	_	254	-
Stage 2	_	_	_	_	196	_
Critical Hdwy	4.1	_	_	_	6.4	6.2
Critical Hdwy Stg 1	-			_	5.4	- 0.2
Critical Hdwy Stg 2	-	-	-		5.4	
	2.2	-	-	-		3.3
Follow-up Hdwy		-	-	-	3.5	
Pot Cap-1 Maneuver	1320	-	-	-	571	790
Stage 1	-	-	-	-	793	-
Stage 2	-	-	-	-	842	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver	1320	-	-	-	559	790
Mov Cap-2 Maneuver	-	-	-	-	559	-
Stage 1	-	-	-	-	776	-
Stage 2	_	_	-	_	842	-
			1675		0.5	
Approach	EB		WB		SB	
HCM Control Delay, s	1.3		0		10	
HCM LOS					В	
Minor Lane/Major Mvm	t	EBL	EBT	WBT	WBR :	SRI n1
			EDI	VVDI		
Capacity (veh/h)		1320	-	-	-	
HCM Lane V/C Ratio		0.021	-	-		0.044
HCM Control Delay (s)		7.8	-	-	-	10
HCM Lane LOS		Α	-	-	-	В
HCM 95th %tile Q(veh)		0.1	-	-	-	0.1

-												
Intersection												
Intersection Delay, s/veh	8.7											
Intersection LOS	Α											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		र्स	7		र्स	7		ર્ન	7		र्स	7
Traffic Vol, veh/h	30	18	5	9	101	19	5	97	12	6	78	24
Future Vol, veh/h	30	18	5	9	101	19	5	97	12	6	78	24
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Heavy Vehicles, %	0	0	0	0	0	0	0	0	0	0	0	0
Mvmt Flow	34	20	6	10	115	22	6	110	14	7	89	27
Number of Lanes	0	1	1	0	1	1	0	1	1	0	1	1
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	2			2			2			2		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	2			2			2			2		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	2			2			2			2		
HCM Control Delay	8.8			8.8			8.8			8.5		
HCM LOS	Α			Α			Α			Α		
Lane		NBLn1	NBLn2	EBLn1	EBLn2	WBLn1	WBLn2	SBLn1	SBLn2			
Vol Left, %		5%	0%	62%	0%	8%	0%	7%	0%			
Vol Thru, %		95%	0%	38%	0%	92%	0%	93%	0%			
Vol Right, %		0%	100%	0%	100%	0%	100%	0%	100%			
Sign Control		Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop			
Traffic Vol by Lane		102	12	48	5	110	19	84	24			
LT Vol												
Through Vol		5	0	30	0	9	0	6	0			
		97	0	18	0	101	0	78	0			
RT Vol		97 0	0 12	18 0	0 5	101 0	0 19	78 0	0 24			
RT Vol Lane Flow Rate		97 0 116	0 12 14	18 0 55	0 5 6	101 0 125	0 19 22	78 0 95	0 24 27			
RT Vol Lane Flow Rate Geometry Grp		97 0 116 7	0 12 14 7	18 0 55 7	0 5 6 7	101 0 125 7	0 19 22 7	78 0 95 7	0 24 27 7			
RT Vol Lane Flow Rate Geometry Grp Degree of Util (X)		97 0 116 7 0.167	0 12 14 7 0.017	18 0 55 7 0.085	0 5 6 7 0.007	101 0 125 7 0.182	0 19 22 7 0.027	78 0 95 7 0.138	0 24 27 7 0.034			
RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd)		97 0 116 7 0.167 5.184	0 12 14 7 0.017 4.456	18 0 55 7 0.085 5.597	0 5 6 7 0.007 4.578	101 0 125 7 0.182 5.236	0 19 22 7 0.027 4.491	78 0 95 7 0.138 5.204	0 24 27 7 0.034 4.465			
RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N		97 0 116 7 0.167 5.184 Yes	0 12 14 7 0.017 4.456 Yes	18 0 55 7 0.085 5.597 Yes	0 5 6 7 0.007 4.578 Yes	101 0 125 7 0.182 5.236 Yes	0 19 22 7 0.027 4.491 Yes	78 0 95 7 0.138 5.204 Yes	0 24 27 7 0.034 4.465 Yes			
RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap		97 0 116 7 0.167 5.184 Yes 692	0 12 14 7 0.017 4.456 Yes 802	18 0 55 7 0.085 5.597 Yes 639	0 5 6 7 0.007 4.578 Yes 779	101 0 125 7 0.182 5.236 Yes 685	0 19 22 7 0.027 4.491 Yes 796	78 0 95 7 0.138 5.204 Yes 689	0 24 27 7 0.034 4.465 Yes 801			
RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time		97 0 116 7 0.167 5.184 Yes 692 2.916	0 12 14 7 0.017 4.456 Yes 802 2.188	18 0 55 7 0.085 5.597 Yes 639 3.338	0 5 6 7 0.007 4.578 Yes 779 2.319	101 0 125 7 0.182 5.236 Yes 685 2.972	0 19 22 7 0.027 4.491 Yes 796 2.227	78 0 95 7 0.138 5.204 Yes 689 2.936	0 24 27 7 0.034 4.465 Yes 801 2.197			
RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time HCM Lane V/C Ratio		97 0 116 7 0.167 5.184 Yes 692 2.916 0.168	0 12 14 7 0.017 4.456 Yes 802 2.188 0.017	18 0 55 7 0.085 5.597 Yes 639 3.338 0.086	0 5 6 7 0.007 4.578 Yes 779 2.319 0.008	101 0 125 7 0.182 5.236 Yes 685 2.972 0.182	0 19 22 7 0.027 4.491 Yes 796 2.227 0.028	78 0 95 7 0.138 5.204 Yes 689 2.936 0.138	0 24 27 7 0.034 4.465 Yes 801 2.197 0.034			
RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time HCM Lane V/C Ratio HCM Control Delay		97 0 116 7 0.167 5.184 Yes 692 2.916 0.168	0 12 14 7 0.017 4.456 Yes 802 2.188 0.017 7.3	18 0 55 7 0.085 5.597 Yes 639 3.338 0.086 8.9	0 5 6 7 0.007 4.578 Yes 779 2.319 0.008 7.4	101 0 125 7 0.182 5.236 Yes 685 2.972 0.182 9.1	0 19 22 7 0.027 4.491 Yes 796 2.227 0.028 7.4	78 0 95 7 0.138 5.204 Yes 689 2.936 0.138 8.8	0 24 27 7 0.034 4.465 Yes 801 2.197 0.034 7.4			
RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time HCM Lane V/C Ratio		97 0 116 7 0.167 5.184 Yes 692 2.916 0.168	0 12 14 7 0.017 4.456 Yes 802 2.188 0.017	18 0 55 7 0.085 5.597 Yes 639 3.338 0.086	0 5 6 7 0.007 4.578 Yes 779 2.319 0.008	101 0 125 7 0.182 5.236 Yes 685 2.972 0.182	0 19 22 7 0.027 4.491 Yes 796 2.227 0.028	78 0 95 7 0.138 5.204 Yes 689 2.936 0.138	0 24 27 7 0.034 4.465 Yes 801 2.197 0.034			

-							
Intersection							
Int Delay, s/veh	0.5						
		EDD	WDI	WDT	NDI	NDD	
Movement	EBT	EBR	WBL	WBT	NBL	NBR	
Lane Configurations	7			ન		7	
Traffic Vol, veh/h	189	18	1	137	11	6	
Future Vol, veh/h	189	18	1	137	11	6	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-	None	-	None	
Storage Length	-	-	-	-	0	50	
Veh in Median Storage,	# 0	-	-	0	0	-	
Grade, %	0	-	-	0	0	-	
Peak Hour Factor	90	90	90	90	90	90	
Heavy Vehicles, %	0	0	0	0	0	0	
Mvmt Flow	210	20	1	152	12	7	
						•	
Major/Minor M	lajor1	N	Major2	N	/linor1		
Conflicting Flow All	0	0	230	0	374	220	
Stage 1	-	-	-	-	220	-	
Stage 2	-	-	-	-	154	-	
Critical Hdwy	-	-	4.1	_	6.4	6.2	
Critical Hdwy Stg 1	-	-	-	-	5.4	-	
Critical Hdwy Stg 2	_	-	_	-	5.4	_	
Follow-up Hdwy	-	-	2.2	_	3.5	3.3	
Pot Cap-1 Maneuver	_	_	1350	_	631	825	
Stage 1	<u>-</u>		-	_	821	- 020	
Stage 2		_		_	879		
Platoon blocked, %	-	_	-		019	-	
			1250	-	620	825	
Mov Cap-1 Maneuver	-	-	1350	-	630		
Mov Cap-2 Maneuver	-	-	-	-	630	-	
Stage 1	-	-	-	-	821	-	
Stage 2	-	-	-	-	878	-	
Approach	EB		WB		NB		
HCM Control Delay, s	0		0.1		10.3		
HCM LOS	U		U. I		10.3 B		
I IOIVI LOS					D		
Minor Lane/Major Mvmt	1	NBLn1N	NBLn2	EBT	EBR	WBL	WBT
Capacity (veh/h)		630	825	-		1350	_
HCM Lane V/C Ratio		0.019		_		0.001	_
HCM Control Delay (s)		10.8	9.4	_	_	7.7	0
HCM Lane LOS		В	Α.4	_	_	Α.	A
HCM 95th %tile Q(veh)		0.1	0	_		0	-
Holvi sour wille Q(ven)		0.1	U	-	-	U	_

Intersection						
Int Delay, s/veh	2					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	ነ	100	<b>↑</b>	7	101	<b>†</b>
Traffic Vol, veh/h	19	130	357	38	181	568
Future Vol, veh/h	19	130	357	38	181	568
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	Free	-	Free	-	None
Storage Length	0	25	-	75	475	-
Veh in Median Storag	e,# 0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	96	96	96	96	96	96
Heavy Vehicles, %	0	0	0	0	0	0
Mymt Flow	20	135	372	40	189	592
IVIVIIIL I IOW	20	100	JIZ	40	103	JJZ
Major/Minor	Minor1	N	/lajor1	N	//ajor2	
Conflicting Flow All	1342	-	0	_	372	0
Stage 1	372	_	-	_	-	-
Stage 2	970	_	_	<u> </u>		-
	6.4				4.1	
Critical Hdwy		-	-	-		-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	-	-	-	2.2	-
Pot Cap-1 Maneuver	169	0	-	0	1198	-
Stage 1	702	0	-	0	-	-
Stage 2	371	0	-	0	-	-
Platoon blocked, %			-			-
Mov Cap-1 Maneuver	142	-	-	-	1198	-
Mov Cap-2 Maneuver		-	-	-	-	-
Stage 1	702	_	-	_	_	-
Stage 2	312	_	_	_	_	_
Olaye Z	012	-			_	_
Approach	WB		NB		SB	
HCM Control Delay, s			0		2.1	
HCM LOS	D					
TIOWI LOO	U					
Minor Lane/Major Mvr	nt	NBTW	VBLn1V	VBLn2	SBL	SBT
Capacity (veh/h)		-	142	-	1198	-
HCM Lane V/C Ratio		_	0.139		0.157	-
HCM Control Delay (s	(	-	34.4	0	8.6	-
HCM Lane LOS	,	_	D	A	A	_
HCM 95th %tile Q(veh	n)		0.5	-	0.6	
HOW SOUT MILE W(VEI	1)	_	0.5	_	0.0	_

Intersection						
Int Delay, s/veh	0.2					
		EDT	MOT	WDD	ODI	000
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		4	Þ	_	Y	
Traffic Vol, veh/h	9	210	143	5	0	0
Future Vol, veh/h	9	210	143	5	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage	e, # -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	88	88	88	88	88	88
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	10	239	163	6	0	0
Major/Minor I	Major1	N	/lajor2	N	/linor2	
						100
Conflicting Flow All	169	0	-	0	425	166
Stage 1	-	-	-	-	166	-
Stage 2	-	-	-	-	259	-
Critical Hdwy	4.1	-	-	-	6.4	6.2
Critical Hdwy Stg 1	-	-	-	-	5.4	-
Critical Hdwy Stg 2	-	-	-	-	5.4	-
Follow-up Hdwy	2.2	-	-	-	3.5	3.3
Pot Cap-1 Maneuver	1421	-	-	-	590	884
Stage 1	-	-	-	-	868	-
Stage 2	-	-	-	-	789	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver	1421	-	-	-	585	884
Mov Cap-2 Maneuver	-	-	-	-	585	-
Stage 1	-	-	-	-	861	-
Stage 2	-	-	-	-	789	-
ŭ						
Approach	EB		WB		SB	
HCM Control Delay, s	0.3		0		0	
HCM LOS					Α	
Minor Lane/Major Mvm	nt _	EBL	EBT	WBT	WBR :	SBL <sub>n1</sub>
Capacity (veh/h)		1421	-		_	_
HCM Lane V/C Ratio		0.007	-	-	-	-
HCM Control Delay (s)		7.6	0	-	-	0
110141						

Α

Α

0

Α

HCM Lane LOS

HCM 95th %tile Q(veh)

Intersection						
Int Delay, s/veh	1.1					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	7	<b>^</b>	1		N.	
Traffic Vol, veh/h	23	195	128	3	4	20
Future Vol, veh/h	23	195	128	3	4	20
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	300	-	-	-	0	-
Veh in Median Storage	,# -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	81	81	81	81	81	81
Heavy Vehicles, %	0	0	0	0	0	0
Mvmt Flow	28	241	158	4	5	25
IVIVIIIL I IOVV	20	Z71	100	7	- 0	20
	Major1	١	/lajor2	N	/linor2	
Conflicting Flow All	162	0	-	0	457	160
Stage 1	-	-	-	-	160	-
Stage 2	-	-	-	-	297	-
Critical Hdwy	4.1	-	-	-	6.4	6.2
Critical Hdwy Stg 1	_	-	_	-	5.4	-
Critical Hdwy Stg 2	-	-	-	-	5.4	-
Follow-up Hdwy	2.2	-	_	-	3.5	3.3
Pot Cap-1 Maneuver	1429		-	-	565	890
Stage 1	-	_	_	-	874	-
Stage 2	_	_	_	_	758	_
Platoon blocked, %		_	_	_	. 00	
Mov Cap-1 Maneuver	1429	_	_	_	554	890
Mov Cap-1 Maneuver	1423		_	-	554	- 030
Stage 1	_	-	_		857	-
•	-	-	-	-	758	
Stage 2	<del>-</del>	-	<del>-</del>	<del>-</del>	7 00	-
Approach	EB		WB		SB	
HCM Control Delay, s	0.8		0		9.6	
HCM LOS					A	
Minor Lane/Major Mvm	t	EBL	EBT	WBT	WBR S	
Capacity (veh/h)		1429	-	-	-	808
HCM Lane V/C Ratio		0.02	-	-	-	0.037
HCM Control Delay (s)		7.6	-	-	-	9.6
HCM Lane LOS		Α	-	-	-	Α
HCM 95th %tile Q(veh)		0.1	-	-	-	0.1

Intersection												
Intersection Delay, s/veh	8.7											
Intersection LOS	Α											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4	7		र्स	7		र्भ	7		र्स	7
Traffic Vol, veh/h	29	94	10	7	45	13	4	63	8	16	102	41
Future Vol, veh/h	29	94	10	7	45	13	4	63	8	16	102	41
Peak Hour Factor	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Heavy Vehicles, %	0	0	0	0	0	0	0	0	0	0	0	0
Mvmt Flow	31	99	11	7	47	14	4	66	8	17	107	43
Number of Lanes	0	1	1	0	1	1	0	1	1	0	1	1
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	2			2			2			2		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	2			2			2			2		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	2			2			2			2		
HCM Control Delay	9.1			8.3			8.5			8.7		
HCM LOS	Α			Α			Α			Α		
Laura												
Lane		NBLn1	NBLn2	EBLn1	EBLn2	WBLn1	WBLn2	SBLn1	SBLn2			
Vol Left, %		NBLn1 6%	NBLn2 0%	EBLn1 24%	EBLn2 0%	WBLn1 13%	WBLn2 0%	SBLn1 14%	SBLn2 0%			
				24% 76%		13% 87%		14% 86%				
Vol Left, % Vol Thru, % Vol Right, %		6%	0%	24%	0% 0% 100%	13%	0%	14%	0% 0% 100%			
Vol Left, % Vol Thru, % Vol Right, % Sign Control		6% 94% 0% Stop	0% 0%	24% 76% 0% Stop	0% 0% 100% Stop	13% 87% 0% Stop	0% 0% 100% Stop	14% 86% 0% Stop	0% 0% 100% Stop			
Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane		6% 94% 0% Stop 67	0% 0% 100%	24% 76% 0% Stop 123	0% 0% 100% Stop 10	13% 87% 0%	0% 0% 100%	14% 86% 0% Stop 118	0% 0% 100% Stop 41			
Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol		6% 94% 0% Stop 67 4	0% 0% 100% Stop 8 0	24% 76% 0% Stop 123 29	0% 0% 100% Stop 10	13% 87% 0% Stop 52	0% 0% 100% Stop 13	14% 86% 0% Stop 118	0% 0% 100% Stop 41			
Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol		6% 94% 0% Stop 67 4 63	0% 0% 100% Stop 8 0	24% 76% 0% Stop 123 29 94	0% 0% 100% Stop 10 0	13% 87% 0% Stop 52 7 45	0% 0% 100% Stop 13 0	14% 86% 0% Stop 118 16	0% 0% 100% Stop 41 0			
Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol		6% 94% 0% Stop 67 4 63	0% 0% 100% Stop 8 0 0	24% 76% 0% Stop 123 29 94	0% 0% 100% Stop 10 0	13% 87% 0% Stop 52 7 45	0% 0% 100% Stop 13 0 0	14% 86% 0% Stop 118 16 102	0% 0% 100% Stop 41 0 0			
Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate		6% 94% 0% Stop 67 4 63 0	0% 0% 100% Stop 8 0 0	24% 76% 0% Stop 123 29 94 0 129	0% 0% 100% Stop 10 0 0	13% 87% 0% Stop 52 7 45 0 55	0% 0% 100% Stop 13 0 0	14% 86% 0% Stop 118 16 102 0	0% 0% 100% Stop 41 0 0 41 43			
Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp		6% 94% 0% Stop 67 4 63 0 71	0% 0% 100% Stop 8 0 0	24% 76% 0% Stop 123 29 94 0 129	0% 0% 100% Stop 10 0 10 11	13% 87% 0% Stop 52 7 45 0 55	0% 0% 100% Stop 13 0 0 13 14	14% 86% 0% Stop 118 16 102 0 124	0% 0% 100% Stop 41 0 0 41 43 7			
Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X)		6% 94% 0% Stop 67 4 63 0 71 7	0% 0% 100% Stop 8 0 0 8 8 7	24% 76% 0% Stop 123 29 94 0 129 7	0% 0% 100% Stop 10 0 0 11 7	13% 87% 0% Stop 52 7 45 0 55 7	0% 0% 100% Stop 13 0 0 13 14 7	14% 86% 0% Stop 118 16 102 0 124 7	0% 0% 100% Stop 41 0 0 41 43 7 0.053			
Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd)		6% 94% 0% Stop 67 4 63 0 71 7 0.103 5.234	0% 0% 100% Stop 8 0 0 8 8 7 0.011 4.5	24% 76% 0% Stop 123 29 94 0 129 7 0.191 5.298	0% 0% 100% Stop 10 0 0 11 7 0.013 4.477	13% 87% 0% Stop 52 7 45 0 55 7 0.081 5.325	0% 0% 100% Stop 13 0 0 13 14 7 0.017 4.553	14% 86% 0% Stop 118 16 102 0 124 7 0.179 5.186	0% 0% 100% Stop 41 0 0 41 43 7 0.053 4.415			
Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N		6% 94% 0% Stop 67 4 63 0 71 7 0.103 5.234 Yes	0% 0% 100% Stop 8 0 0 8 8 7 0.011 4.5 Yes	24% 76% 0% Stop 123 29 94 0 129 7 0.191 5.298 Yes	0% 0% 100% Stop 10 0 0 11 7 0.013 4.477 Yes	13% 87% 0% Stop 52 7 45 0 55 7 0.081 5.325 Yes	0% 0% 100% Stop 13 0 0 13 14 7 0.017 4.553 Yes	14% 86% 0% Stop 118 16 102 0 124 7 0.179 5.186 Yes	0% 0% 100% Stop 41 0 0 41 43 7 0.053 4.415 Yes			
Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap		6% 94% 0% Stop 67 4 63 0 71 7 0.103 5.234 Yes 684	0% 0% 100% Stop 8 0 0 8 8 7 0.011 4.5 Yes 794	24% 76% 0% Stop 123 29 94 0 129 7 0.191 5.298 Yes 677	0% 0% 100% Stop 10 0 0 11 7 0.013 4.477 Yes 798	13% 87% 0% Stop 52 7 45 0 55 7 0.081 5.325 Yes 672	0% 0% 100% Stop 13 0 0 13 14 7 0.017 4.553 Yes 784	14% 86% 0% Stop 118 16 102 0 124 7 0.179 5.186 Yes 692	0% 0% 100% Stop 41 0 0 41 43 7 0.053 4.415 Yes 810			
Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time		6% 94% 0% Stop 67 4 63 0 71 7 0.103 5.234 Yes 684 2.972	0% 0% 100% Stop 8 0 0 8 8 7 0.011 4.5 Yes 794 2.237	24% 76% 0% Stop 123 29 94 0 129 7 0.191 5.298 Yes 677 3.033	0% 0% 100% Stop 10 0 0 10 11 7 0.013 4.477 Yes 798 2.211	13% 87% 0% Stop 52 7 45 0 55 7 0.081 5.325 Yes 672 3.065	0% 0% 100% Stop 13 0 0 13 14 7 0.017 4.553 Yes 784 2.293	14% 86% 0% Stop 118 16 102 0 124 7 0.179 5.186 Yes 692 2.919	0% 0% 100% Stop 41 0 0 41 43 7 0.053 4.415 Yes 810 2.148			
Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time HCM Lane V/C Ratio		6% 94% 0% Stop 67 4 63 0 71 7 0.103 5.234 Yes 684 2.972 0.104	0% 0% 100% Stop 8 0 0 8 8 7 0.011 4.5 Yes 794 2.237 0.01	24% 76% 0% Stop 123 29 94 0 129 7 0.191 5.298 Yes 677 3.033 0.191	0% 0% 100% Stop 10 0 11 7 0.013 4.477 Yes 798 2.211 0.014	13% 87% 0% Stop 52 7 45 0 55 7 0.081 5.325 Yes 672 3.065 0.082	0% 0% 100% Stop 13 0 0 13 14 7 0.017 4.553 Yes 784 2.293 0.018	14% 86% 0% Stop 118 16 102 0 124 7 0.179 5.186 Yes 692 2.919 0.179	0% 0% 100% Stop 41 0 0 41 43 7 0.053 4.415 Yes 810 2.148 0.053			
Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time HCM Lane V/C Ratio HCM Control Delay		6% 94% 0% Stop 67 4 63 0 71 7 0.103 5.234 Yes 684 2.972 0.104 8.6	0% 0% 100% Stop 8 0 0 8 8 7 0.011 4.5 Yes 794 2.237 0.01 7.3	24% 76% 0% Stop 123 29 94 0 129 7 0.191 5.298 Yes 677 3.033 0.191 9.3	0% 0% 100% Stop 10 0 0 11 7 0.013 4.477 Yes 798 2.211 0.014 7.3	13% 87% 0% Stop 52 7 45 0 55 7 0.081 5.325 Yes 672 3.065 0.082 8.5	0% 0% 100% Stop 13 0 0 13 14 7 0.017 4.553 Yes 784 2.293 0.018 7.4	14% 86% 0% Stop 118 16 102 0 124 7 0.179 5.186 Yes 692 2.919 0.179 9.1	0% 0% 100% Stop 41 0 0 41 43 7 0.053 4.415 Yes 810 2.148 0.053 7.4			
Vol Left, % Vol Thru, % Vol Right, % Sign Control Traffic Vol by Lane LT Vol Through Vol RT Vol Lane Flow Rate Geometry Grp Degree of Util (X) Departure Headway (Hd) Convergence, Y/N Cap Service Time HCM Lane V/C Ratio		6% 94% 0% Stop 67 4 63 0 71 7 0.103 5.234 Yes 684 2.972 0.104	0% 0% 100% Stop 8 0 0 8 8 7 0.011 4.5 Yes 794 2.237 0.01	24% 76% 0% Stop 123 29 94 0 129 7 0.191 5.298 Yes 677 3.033 0.191	0% 0% 100% Stop 10 0 11 7 0.013 4.477 Yes 798 2.211 0.014	13% 87% 0% Stop 52 7 45 0 55 7 0.081 5.325 Yes 672 3.065 0.082	0% 0% 100% Stop 13 0 0 13 14 7 0.017 4.553 Yes 784 2.293 0.018	14% 86% 0% Stop 118 16 102 0 124 7 0.179 5.186 Yes 692 2.919 0.179	0% 0% 100% Stop 41 0 0 41 43 7 0.053 4.415 Yes 810 2.148 0.053			

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**Appendix C**Haul Routes and Levels of Service

#### Tuolumne Facility Haul Routes and Levels of Service

Haul Route	CA Postmile	Latitude	Longitude	Lanes at Postmile	FHWA FC#1	Type#2	LOS "D" Capacity at Postmile <sup>2</sup>	Data Year <sup>3</sup>	Back ADT A	Ahead ADT	ADT (Base Yr)	ADT (2023)	V/C (E) LOS	ADT (Project Logging/Haul Trucks)	ADT (E+P)	V/C (E+P) LOS	LOS D or better?	ADT (2025)	V/C (OY)	LOS (OY)	ADT (OY+P)	//C (OY+P)	LOS (OY+P)	OY+P LOS D or better?
SR-4	29.62	38.139059	-120.456141	2	4	210	20100	2021	7000	6800	7000		0.362 A	236				7577	0.377		7813	0.389	A	Yes
SR-4	18.556	38.067128	-120.59894	2	3	5	13260	2021	490	490	490	510	0.038 A	236	746	0.056 A	Yes	531	0.040	A	767	0.058	A	Yes
SR-41	17.91	37.12444	-119.736963	4	3	2	20485	2021	16000	13400	16000	16646	0.813 D	236	16882	0.824 D	Yes	17318	0.845	D	17554	0.857	D	Yes
SR-49	1.65	38.573869	-120.846136	2	3	5	13260	2021	2050	2050	2050	2133	0.161 A	236	2369	0.179 A	Yes	2219	0.167	A	2455	0.185	A	Yes
SR-49	9.42	38.087694	-120.57103	2	4	5	13260	2021	7700	7100	7700	8011	0.604 B	236	8247	0.622 B	Yes	8335	0.629	В	8571	0.646	В	Yes
SR-49		37.569309			3	210	20100	2021	860	510	860	895	0.045 A	236		0.056 A	Yes	931	0.046		1167	0.058		Yes
US 50		38.731226			3	201	74400	2021	24300	23900	24300	25282	0.340 A	236		0.343 A	Yes	26303	0.354		26539	0.357		Yes
US 50	65.619	38.824307	-120.044235	2	3	104	18190	2021	15500	9200	15500	16126	0.887 D	236	16362	0.900 D	Yes	16777	0.922	E	17013	0.935	E	No
SR-88	1.25	38.704996	-120.050932	2	2	105	12340	2021	1950	2450	2450	2549	0.207 A	236	2785	0.226 A	Yes	2652	0.215	A	2888	0.234	A	Yes
SR-88	22.69	38.412824	-120.667363	2	3	4	19550	2021	12000	12000	12000	12485	0.639 B	236	12721	0.651 B	Yes	12989	0.664	В	13225	0.676	В	Yes
SR-108	7.511	37.996508	-120.267276	4	4	1	26520	2021	10500	7900	10500	10924	0.412 A	236	11160	0.421 A	Yes	11365	0.429	A	11601	0.437	A	Yes
SR-108	9.6	38.350174	-119.536286	2	4	105	12340	2021	1300	1550	1550	1613	0.131 A	236	1849	0.150 A	Yes	1678	0.136	A	1914	0.155	A	Yes
SR-120		37.838293			3	5	13260	2021	8600	3850	8600		0.675 B	236			Yes	9308	0.702		9544	0.720		Yes
SR-120		37.84335			3	4	19550	2021	9500	12900	12900	13421	0.686 B	236		0.699 B	Yes	13963	0.714		14199	0.726		Yes
SR-132		37.706276			4	5	13260	2021	1450	1150	1450	1509	0.114 A	236	1745	0.132 A	Yes	1570	0.118		1806	0.136		Yes
SR-132		37.661141			4	5	13260	2021	1700	1400	1700	1769	0.133 A	236			Yes	1840	0.139		2076	0.157		Yes
SR-140			-119.939815		3	105	12340	2021	2550	1400	2550	2653	0.215 A	236		0.234 A	Yes	2760	0.224	A	2996	0.243		Yes
SR-167			-119.557381		4	5	13260	2021	7000	6500	7000	7283	0.549 A	236			Yes	7577	0.571	A	7813	0.589		Yes
SR-168	65.84		-119.161485		4	105	12340	2021	1100	1000	1100		0.093 A	236			Yes	1190	0.096		1426	0.116		Yes
Road CR J59		37.840655	-120.507755	2	4	8	11008	2023	3155		3155	3155	0.287 A	236	3391	0.308 A	Yes	3282	0.298	A	3518	0.320	A	Yes
1 Federal Highway Administration Fund	tional Classification Sy	stem for Calti	ans roadways.																					
2 Type number and capacity based on t	the LOS Look Up Table	provided as A	ppendix Table	2 of the Tuolumne Co	unty General	Plan and F	TP Update Traffic Study (September	er 2015).																
<sup>3</sup> Average daily traffic (ADT), including																								

Appendix Table 2 – Tuolumne County – LOS Look up Table

	Appendix rable z = ru	·	ocunty	- LOO LO	JOK UP TU	DIC		
FHWA FC#	Roadway Type	Type #	Area Type		num Two-wa carrying Ca <sub>l</sub>		•	` '
10#			Type	LOS "A"	LOS "B"	LOS "C"	LOS "D"	LOS "E"
4	Rural Arterial (4-lane) Divided	1		6,240	12,480	18,720	26,520	31,200
4	Rural Arterial (4-lane) Undivided	2		4,820	9,640	14,460	20,485	24,100
4	Rural Minor Arterial (4-lane)	3		6,080	12,160	18,240	25,840	30,400
4	Rural Minor Arterial (with left-turn Lane)	4		4,600	9,200	13,800	19,550	23,000
4	Rural Minor Arterial (2-lane)	5	ى ق	3,120	6,240	9,360	13,260	15,600
5	Major Collector (34 ft 36 ft.)	6	N N	3,420	6,840	10,260	14,535	17,100
5	Major/Minor Collector (23 ft 32 ft.)	7	ROLLING	2,900	5,800	8,700	12,325	14,500
5	Major/Minor Collector (20 ft 23 ft.)	8	~	2,590	5,180	7,770	11,008	12,950
5	Major/Minor Collector (18 ft 20 ft.)	9		2,300	4,600	6,900	9,775	11,500
5	Major/Minor Collector (Less than 18 ft.)	10		1,920	3,840	5,760	8,160	9,600
6	Local Road	11		1,920	3,840	5,760	8,160	9,600
4	Rural Minor Arterial (with Climbing Lane)	12		2,900	7,400	13,800	19,700	28,800
4	Rural Arterial (4-lane) Divided	101		5,810	11,610	17,410	24,670	29,020
4	Rural Arterial (4-lane) Undivided	102		4,490	8,970	13,450	19,060	22,420
4	Rural Minor Arterial (4-lane)	103		5,660	11,310	16,970	24,040	28,280
4	Rural Minor Arterial (with left-turn Lane)	104	SI	4,280	8,560	12,840	18,190	21,390
4	Rural Minor Arterial (2-lane)	105	ig ig	2,910	5,810	8,710	12,340	14,510
5	Major Collector (34 ft 36 ft.)	106	N.	3,190	6,370	9,550	13,520	15,910
5	Major/Minor Collector (23 ft 32 ft.)	107	È	2,700	5,400	8,100	11,470	13,490
5	Major/Minor Collector (20 ft 23 ft.)	108	MOUNTANEOUS	2,410	4,820	7,230	10,240	12,050
5	Major/Minor Collector (18 ft 20 ft.)	109	Ĭ	2,140	4,280	6,420	9,100	10,700
5	Major/Minor Collector (Less than 18 ft.)	110		1,790	3,580	5,360	7,590	8,930
6	Local Road	111		1,790	3,580	5,360	7,590	8,930
4	Rural Minor Arterial (with Climbing Lane)	112		2,700	6,890	12,840	18,330	26,790
2	4-Lane Freeway	201		28,000	43,200	61,600	74,400	80,000
2	3-Lane Freeway	202		10,100	20,200	30,300	42,925	50,500
2	2-Lane Freeway + Auxiliary Lanes	203		8,392	16,784	25,176	35,666	41,960
2	2-Lane Freeway	204		6,680	13,360	20,040	28,390	33,400
2	4-Lane Expressway	205		24,000	28,000	32,000	36,000	40,000
2	2-Lane Expressway	206		5,700	11,300	17,000	24,100	28,400
3	6-Lane Divided Arterial (with left-turn lane)	207	URBAN	32,000	38,000	43,000	49,000	54,000
3	4-Lane Divided Arterial (with left-turn lane)	208	JRE	22,000	25,000	29,000	32,500	36,000
3	4-Lane Undivided Arterial (no left-turn lane)	209		18,000	21,000	24,000	27,000	30,000
4	2-Lane Principal/Minor Arterial (with left-turn lane)	210		2,900	7,700	14,300	20,100	31,300
4	2-Lane Principal/Minor Arterial (no left-turn lane)	211		2,900	7,200	11,900	16,100	24,200
5	2-Lane Major/Minor Collector (with left-turn lane)	212		3,400	6,900	11,600	15,800	29,400
5	2-Lane Major/Minor Collector (no left-turn lane)	213		2,700	5,600	9,200	12,800	23,500
6	2-Lane Local Street	214		2,300	4,900	8,400	11,400	21,200

#### Notes:

- 1. Values shown corresponding to LOS A through E are roadway ADT traffic volumes
- 2. Collector width is measured from the edge of pavement to the edge of pavement
- 3. Roadways with continuous grade steeper than 6% or above 4,000 ft. elevation should use mountainous train LOS thresholds
- 4. Site Specific LOS maybe necessary
- Peak Hour LOS threshold is assumed to be 10% of the daily traffic volume unless site specific analysis shows a different peak hour to daily traffic ratio
- 6. Examples LOS A (0.20 of capacity), LOS B (0.21 to 0.40 of capacity), LOS C (0.41 to 0.60 of capacity), LOS D (0.61 to 0.85 of capacity), LOS E (0.86 to 0.92 of capacity)

All volumes thresholds are approximate and assumes average roadway characteristics. Actual threshold volume for each Level of Service listed above may vary depending on variety of factors including (but not limited to) roadway curvature and grade, intersection or interchange spacing, driveway spacing, percentage of trucks, RVs, and other heavy vehicles, travel lane widths, speed limits, signal timing characteristics, on-street parking, volume of cross traffic and pedestrians, etc.

WR# 8431.008 August 2016



# **Appendix D**

Cumulative Project Trip Generation

**Cumulative Projects Trip Generation Summary** 

	idiative Projects hip Generation Summary				Al	M Peak Hou	r	P	M Peak Hou	ır
	Land Use	ITE Code	Size/Units	Daily	In	Out	Total	In	Out	Total
TRIP	RATES <sup>1</sup>									
Hotel		310	per Room	7.99	0.26	0.20	0.46	0.30	0.29	0.59
Casin	o (Field Counts) <sup>2</sup>	-	per GP	8.01	0.11	0.12	0.23	0.20	0.19	0.39
Quali	y Restaurant	931	per TSF	10.99	0.37	0.37	0.73	5.23	2.57	7.80
Drink	ing Place <sup>3</sup>	975	per TSF	61.69	0.00	0.00	0.00	7.50	3.86	11.36
No.	TRIP GENERATION <sup>4</sup>									
T1	Casino	-	400 GP	3,204	54	38	92	96	73	169
			To Attached Hotel	-1,406	-19	-28	-47	-30	-32	-62
			To Steakhouse	-234	-1	-1	-2	-7	-14	-21
	Attached Hotel	310	200 Rooms	1,598	52	40	92	60	58	118
			To Casino	-828	-28	-19	-47	-32	-30	-62
	Sports Bar	975	2.4 TSF	148	0	0	0	18	9	27
			To Casino	-76	0	0	0	-9	-5	-14
	Steakhouse	931	5.4 TSF	59	2	2	4	28	14	42
			To Casino	-30	-1	-1	-2	-14	-7	-21
	Chicken Ranch Rancheria New Hotel a	nd Casino P	roject 2 Net New Total	2,436	58	31	90	110	66	176
T2	Tuolumne Bioenergy Woody Biomass Pellet		Passenger Vehicles	12	6	3	9	3	6	9
	Manufacturing Facility		Trucks	12	2	2	4	2	2	4
			Total	24	8	5	13	5	8	13
			Trucks (PCE-adjusted)	36	6	6	12	6	6	12
			Total (PCE-adjusted)	48	12	9	21	9	12	21
T3	Tuolumne Biomass LLC Biomass Utilization Project <sup>5</sup>		Passenger Vehicles	334	167	0	167	0	167	167
			Trucks	130	8	8	16	8	8	16
			Total	464	175	8	183	8	175	183
			Trucks (PCE-adjusted)	390	24	24	48	24	24	48
			Total (PCE-adjusted)	724	191	24	215	24	191	215
T4	Social and Ecological Resilience Across the Landscape		Passenger Vehicles	45	13	0	13	0	13	13
	(SERAL) Forest Health Project Phase 1 - Stanislaus		Trucks	108	8	7	15	7	7	14
	National Forest		Total	153	21	7	28	7	20	27
			Trucks (PCE-adjusted)	324	24	21	45	21	21	42
			Total (PCE-adjusted)	369	37	21	58	21	34	55
			Total Trip Generation	3,077	262	51	313	130	268	399
		Total	Trip Generation (PCE)	3,577	298	85	383	164	302	467

Notes: TSF = thousand square feet; GP = gaming position

 $<sup>^{1}</sup>$  Trip rates from *Trip Generation Manual, 11th Edition* , Institute of Transportation Engineers, 2021.

Trip generation from Appendix H of the Chicken Ranch Rancheria New Hotel and Casino Project Final TEIR, July 2021; updated where applicable with ITE 11th Edition rates. Daily internal trip capture (ITC) <sup>2</sup> estimated from average percentages between AM and PM ITC assumptions from the TEIR.

<sup>&</sup>lt;sup>3</sup> No daily rate provided for Drinking Place land use; daily rate from Brewery Tap Room (ITE Code 971) used.

<sup>&</sup>lt;sup>4</sup> Cumulative projects provided by the County of Tuolumne, 2023.

 $<sup>^{\</sup>rm 5}\,$  Trip generation approximated from Appendix A of the TBLLC Public IS-MND; January 26, 2023.

<sup>&</sup>lt;sup>6</sup> Trip generation approximated from Figure 2 - Site Plan of the TBI Biomass Initial Study/Mitigated Negative Declaration; site plan received by Community Development Dept. March 30, 2021.

**Appendix E**SimTraffic Queuing Worksheet

Movement	WB	WB	SB
Directions Served	L	R	L
Maximum Queue (ft)	66	48	61
Average Queue (ft)	17	37	26
95th Queue (ft)	47	43	52
Link Distance (ft)	510		
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)		25	475
Storage Blk Time (%)	7	2	
Queuing Penalty (veh)	11	0	

#### Intersection: 2: La Grange Road - CR J59 & SPI Employee Dwy

Movement
Directions Served
Maximum Queue (ft)
Average Queue (ft)
95th Queue (ft)
Link Distance (ft)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (ft)
Storage Blk Time (%)
Queuing Penalty (veh)

Movement	EB	SB
Directions Served	L	LR
Maximum Queue (ft)	10	29
Average Queue (ft)	0	4
95th Queue (ft)	5	21
Link Distance (ft)		867
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)	300	
Storage Blk Time (%)		
Queuing Penalty (veh)		

Movement	EB	WB	NB	NB	SB	SB
Directions Served	LT	LT	LT	R	LT	R
Maximum Queue (ft)	29	47	48	37	49	45
Average Queue (ft)	16	28	29	11	28	14
95th Queue (ft)	38	42	43	35	45	41
Link Distance (ft)	2630	2629	1416		2042	
Upstream Blk Time (%)						
Queuing Penalty (veh)						
Storage Bay Dist (ft)				25		25
Storage Blk Time (%)			5	1	5	1
Queuing Penalty (veh)			1	1	1	1

#### Intersection: 5: Red Hill Road & Montezuma/SR-49 - SR-120

Movement	NB	NB
Directions Served	L	R
Maximum Queue (ft)	21	25
Average Queue (ft)	5	5
95th Queue (ft)	18	21
Link Distance (ft)	1595	
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		50
Storage Blk Time (%)	0	
Queuing Penalty (veh)	0	

#### **Network Summary**

Movement	WB	WB	SB
Directions Served	L	R	L
Maximum Queue (ft)	44	44	53
Average Queue (ft)	12	33	22
95th Queue (ft)	36	47	49
Link Distance (ft)	510		
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)		25	475
Storage Blk Time (%)	7	1	
Queuing Penalty (veh)	6	0	

#### Intersection: 2: La Grange Road - CR J59 & SPI Employee Dwy

Movement
Directions Served
Maximum Queue (ft)
Average Queue (ft)
95th Queue (ft)
Link Distance (ft)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (ft)
Storage Blk Time (%)
Queuing Penalty (veh)

Movement	EB
Directions Served	L
Maximum Queue (ft)	17
Average Queue (ft)	1
95th Queue (ft)	8
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	300
Storage Blk Time (%)	
Queuing Penalty (veh)	

Movement	EB	WB	NB	NB	SB	SB
Directions Served	LT	LT	LT	R	LT	R
Maximum Queue (ft)	56	32	43	39	52	42
Average Queue (ft)	30	22	24	7	29	19
95th Queue (ft)	47	38	43	29	46	46
Link Distance (ft)	2630	2629	1416		2042	
Upstream Blk Time (%)						
Queuing Penalty (veh)						
Storage Bay Dist (ft)				25		25
Storage Blk Time (%)			3	1	6	2
Queuing Penalty (veh)			0	0	2	1

#### Intersection: 5: Red Hill Road & Montezuma/SR-49 - SR-120

Movement	WB	NB	NB
Directions Served	LT	L	R
Maximum Queue (ft)	12	24	25
Average Queue (ft)	0	6	3
95th Queue (ft)	6	20	17
Link Distance (ft)	1098	1595	
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)			50
Storage Blk Time (%)		0	
Queuing Penalty (veh)		0	

#### **Network Summary**

Movement	WB	WB	SB
Directions Served	L	R	L
Maximum Queue (ft)	75	48	77
Average Queue (ft)	16	38	30
95th Queue (ft)	50	45	62
Link Distance (ft)	510		
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)		25	475
Storage Blk Time (%)	6	2	
Queuing Penalty (veh)	10	1	

#### Intersection: 2: La Grange Road - CR J59 & SPI Employee Dwy

Movement	EB	SB	
Directions Served	LT	LR	
Maximum Queue (ft)	39	29	
Average Queue (ft)	2	10	
95th Queue (ft)	17	32	
Link Distance (ft)	510	582	
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Movement	EB	SB
Directions Served	L	LR
Maximum Queue (ft)	34	38
Average Queue (ft)	3	19
95th Queue (ft)	18	42
Link Distance (ft)		867
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)	300	
Storage Blk Time (%)		
Queuing Penalty (veh)		

Movement	EB	WB	NB	NB	SB	SB
Directions Served	LT	LT	LT	R	LT	R
Maximum Queue (ft)	42	50	51	37	53	45
Average Queue (ft)	18	29	29	12	30	14
95th Queue (ft)	40	43	43	36	44	40
Link Distance (ft)	2630	2629	1416		2042	
Upstream Blk Time (%)						
Queuing Penalty (veh)						
Storage Bay Dist (ft)				25		25
Storage Blk Time (%)			6	1	5	1
Queuing Penalty (veh)			1	1	1	1

#### Intersection: 5: Red Hill Road & Montezuma/SR-49 - SR-120

Directions Served L R
Directions derived L IX
Maximum Queue (ft) 20 25
Average Queue (ft) 5 5
95th Queue (ft) 17 21
Link Distance (ft) 1595
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (ft) 50
Storage Blk Time (%) 0
Queuing Penalty (veh) 0

#### **Network Summary**

Movement	WB	WB	NB	SB
Directions Served	L	R	R	L
Maximum Queue (ft)	64	44	33	67
Average Queue (ft)	14	35	2	26
95th Queue (ft)	42	43	18	56
Link Distance (ft)	510			
Upstream Blk Time (%)				
Queuing Penalty (veh)				
Storage Bay Dist (ft)		25	75	475
Storage Blk Time (%)	8	1	0	
Queuing Penalty (veh)	8	0	0	

#### Intersection: 2: La Grange Road - CR J59 & SPI Employee Dwy

Movement	EB
Directions Served	LT
Maximum Queue (ft)	33
Average Queue (ft)	2
95th Queue (ft)	15
Link Distance (ft)	510
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

Movement	EB	SB
Directions Served	L	LR
Maximum Queue (ft)	32	29
Average Queue (ft)	4	13
95th Queue (ft)	19	36
Link Distance (ft)		867
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)	300	
Storage Blk Time (%)		
Queuing Penalty (veh)		

Movement	EB	WB	NB	NB	SB	SB
Directions Served	LT	LT	LT	R	LT	R
Maximum Queue (ft)	54	45	44	33	54	47
Average Queue (ft)	31	21	24	8	30	19
95th Queue (ft)	47	41	44	29	45	46
Link Distance (ft)	2630	2629	1416		2042	
Upstream Blk Time (%)						
Queuing Penalty (veh)						
Storage Bay Dist (ft)				25		25
Storage Blk Time (%)			4	1	6	2
Queuing Penalty (veh)			0	0	2	1

#### Intersection: 5: Red Hill Road & Montezuma/SR-49 - SR-120

Movement	WB	NB	NB
Directions Served	LT	L	R
Maximum Queue (ft)	26	20	20
Average Queue (ft)	1	4	2
95th Queue (ft)	12	16	13
Link Distance (ft)	1098	1595	
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)			50
Storage Blk Time (%)		0	
Queuing Penalty (veh)		0	

#### **Network Summary**

Movement	WB	WB	SB
Directions Served	L	R	L
Maximum Queue (ft)	64	50	66
Average Queue (ft)	20	39	32
95th Queue (ft)	53	49	62
Link Distance (ft)	510		
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)		25	475
Storage Blk Time (%)	8	3	
Queuing Penalty (veh)	15	1	

#### Intersection: 2: La Grange Road - CR J59 & SPI Employee Dwy

Movement
Directions Served
Maximum Queue (ft)
Average Queue (ft)
95th Queue (ft)
Link Distance (ft)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (ft)
Storage Blk Time (%)
Queuing Penalty (veh)

Movement	EB	SB
Directions Served	L	LR
Maximum Queue (ft)	16	28
Average Queue (ft)	1	4
95th Queue (ft)	7	20
Link Distance (ft)		867
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)	300	
Storage Blk Time (%)		
Queuing Penalty (veh)		

Movement	EB	EB	WB	NB	NB	SB	SB
Directions Served	LT	R	LT	LT	R	LT	R
Maximum Queue (ft)	34	11	55	57	37	53	45
Average Queue (ft)	21	0	29	31	10	30	16
95th Queue (ft)	39	8	45	45	34	48	43
Link Distance (ft)	2630		2629	1416		2042	
Upstream Blk Time (%)							
Queuing Penalty (veh)							
Storage Bay Dist (ft)		100			25		25
Storage Blk Time (%)				7	1	5	1
Queuing Penalty (veh)				1	1	1	1

#### Intersection: 5: Red Hill Road & Montezuma/SR-49 - SR-120

Movement	NB	NB
Directions Served	L	R
Maximum Queue (ft)	21	31
Average Queue (ft)	5	5
95th Queue (ft)	18	22
Link Distance (ft)	1595	
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		50
Storage Blk Time (%)	0	0
Queuing Penalty (veh)	0	0

#### **Network Summary**

Movement	WB	WB	SB
Directions Served	L	R	L
Maximum Queue (ft)	80	47	78
Average Queue (ft)	17	35	33
95th Queue (ft)	56	45	64
Link Distance (ft)	510		
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)		25	475
Storage Blk Time (%)	12	1	
Queuing Penalty (veh)	13	0	

#### Intersection: 2: La Grange Road - CR J59 & SPI Employee Dwy

Movement
Directions Served
Maximum Queue (ft)
Average Queue (ft)
95th Queue (ft)
Link Distance (ft)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (ft)
Storage Blk Time (%)
Queuing Penalty (veh)

Movement	EB	
Directions Served	L	
Maximum Queue (ft)	21	
Average Queue (ft)	1	
95th Queue (ft)	10	
Link Distance (ft)		
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)	300	
Storage Blk Time (%)		
Queuing Penalty (veh)		

Movement	EB	EB	WB	NB	NB	SB	SB
Directions Served	LT	R	LT	LT	R	LT	R
Maximum Queue (ft)	53	11	46	40	38	59	47
Average Queue (ft)	32	0	22	26	6	33	26
95th Queue (ft)	48	8	42	42	27	53	52
Link Distance (ft)	2630		2629	1416		2042	
Upstream Blk Time (%)							
Queuing Penalty (veh)							
Storage Bay Dist (ft)		100			25		25
Storage Blk Time (%)				4	1	8	3
Queuing Penalty (veh)				0	0	3	3

#### Intersection: 5: Red Hill Road & Montezuma/SR-49 - SR-120

Movement	WB	NB	NB
Directions Served	LT	L	R
Maximum Queue (ft)	5	29	20
Average Queue (ft)	0	5	3
95th Queue (ft)	4	18	17
Link Distance (ft)	1098	1595	
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)			50
Storage Blk Time (%)		0	
Queuing Penalty (veh)		0	

#### **Network Summary**

Movement	WB	WB	SB
Directions Served	L	R	L
Maximum Queue (ft)	164	50	76
Average Queue (ft)	31	40	37
95th Queue (ft)	99	50	65
Link Distance (ft)	510		
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)		25	475
Storage Blk Time (%)	11	4	
Queuing Penalty (veh)	23	1	

#### Intersection: 2: La Grange Road - CR J59 & SPI Employee Dwy

Movement	EB	SB
Directions Served	LT	LR
Maximum Queue (ft)	39	38
Average Queue (ft)	4	12
95th Queue (ft)	22	35
Link Distance (ft)	510	582
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Movement	EB	SB	
Directions Served	L	LR	
Maximum Queue (ft)	28	46	
Average Queue (ft)	6	17	
95th Queue (ft)	24	42	
Link Distance (ft)		867	
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)	300		
Storage Blk Time (%)			
Queuing Penalty (veh)			

Movement	EB	WB	NB	NB	SB	SB
Directions Served	LT	LT	LT	R	LT	R
Maximum Queue (ft)	37	55	48	38	58	47
Average Queue (ft)	22	30	30	11	31	16
95th Queue (ft)	40	48	41	36	46	44
Link Distance (ft)	2630	2629	1416		2042	
Upstream Blk Time (%)						
Queuing Penalty (veh)						
Storage Bay Dist (ft)				25		25
Storage Blk Time (%)			7	1	7	1
Queuing Penalty (veh)			1	1	2	1

#### Intersection: 5: Red Hill Road & Montezuma/SR-49 - SR-120

Movement	NB	NB	
Directions Served	L	R	
Maximum Queue (ft)	30	25	
Average Queue (ft)	7	5	
95th Queue (ft)	21	21	
Link Distance (ft)	1595		
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)		50	
Storage Blk Time (%)	0		
Queuing Penalty (veh)	0		

#### **Network Summary**

Movement	WB	WB	NB	SB
Directions Served	L	R	R	L
Maximum Queue (ft)	65	46	11	98
Average Queue (ft)	16	36	1	37
95th Queue (ft)	46	45	11	71
Link Distance (ft)	510			
Upstream Blk Time (%)				
Queuing Penalty (veh)				
Storage Bay Dist (ft)		25	75	475
Storage Blk Time (%)	12	1	0	
Queuing Penalty (veh)	16	0	0	

#### Intersection: 2: La Grange Road - CR J59 & SPI Employee Dwy

Movement	EB
Directions Served	LT
Maximum Queue (ft)	21
Average Queue (ft)	1
95th Queue (ft)	13
Link Distance (ft)	510
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

Movement	EB	SB	
Directions Served	L	LR	
Maximum Queue (ft)	30	37	
Average Queue (ft)	4	16	
95th Queue (ft)	19	39	
Link Distance (ft)		867	
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)	300		
Storage Blk Time (%)			
Queuing Penalty (veh)			

Movement	EB	WB	NB	NB	SB	SB
Directions Served	LT	LT	LT	R	LT	R
Maximum Queue (ft)	65	40	39	37	63	47
Average Queue (ft)	32	23	25	8	34	26
95th Queue (ft)	50	40	42	31	54	51
Link Distance (ft)	2630	2629	1416		2042	
Upstream Blk Time (%)						
Queuing Penalty (veh)						
Storage Bay Dist (ft)				25		25
Storage Blk Time (%)			4	1	8	3
Queuing Penalty (veh)			0	0	3	3

#### Intersection: 5: Red Hill Road & Montezuma/SR-49 - SR-120

Movement	WB	NB	NB
Directions Served	LT	L	R
Maximum Queue (ft)	27	16	20
Average Queue (ft)	1	4	2
95th Queue (ft)	12	14	15
Link Distance (ft)	1098	1595	
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)			50
Storage Blk Time (%)			
Queuing Penalty (veh)			

#### **Network Summary**